

Missouri Department of Transportation
Bridge Division

Bridge Design Manual
Section 3.31

Revised 05/28/2004

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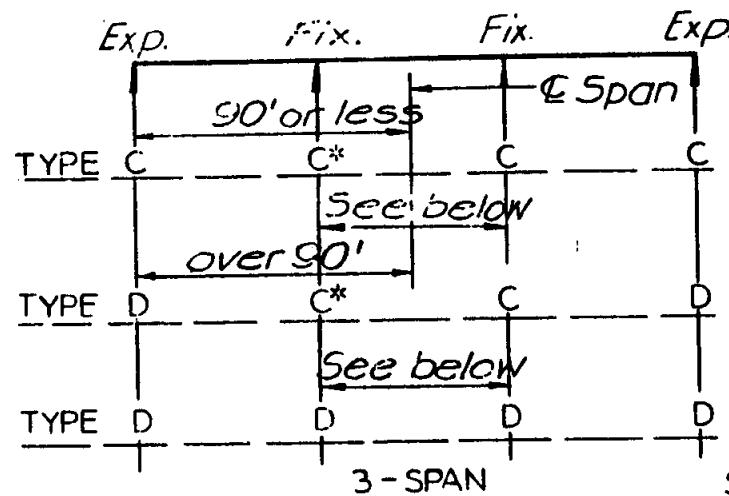
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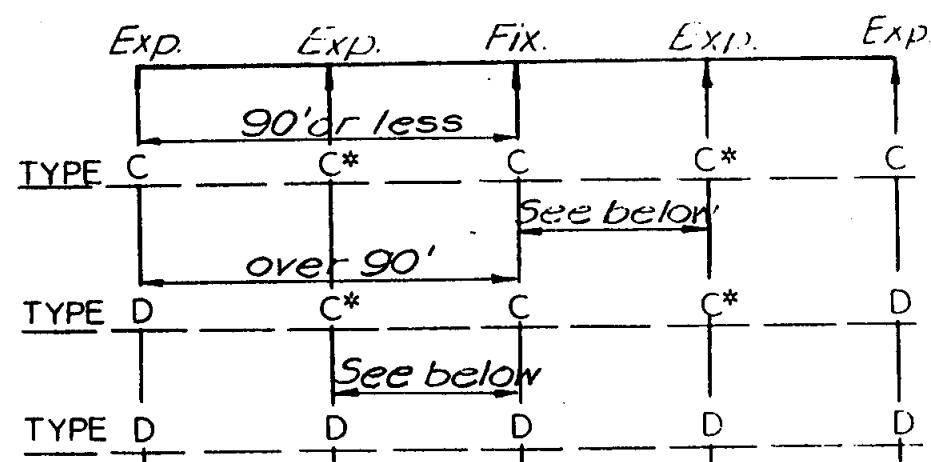
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EXPANDING LENGTH OF SUPERSTRUCTURE LIMITATIONS			ALLOWABLE MASONRY PRESSURE	ANCHOR BOLTS
TYPE BRG.	SIMPLE	CONTINUOUS		
Flat Plate	thru 33'	---	700 psi	1"φ
Type "C"	35' thru 80'	see diagram		1"φ
Type "D"	---	see diagram	1000 psi	Exp Brg..... - 1½"φ Fix Brg - thru 150' spans - 1½"φ Fix Brg - over 150' spans - 1¾"φ

See the Structural Design Engineer for final choice of bearings.



SPAN LIMITATION DIAGRAMS



Use same size bearing for all stringers at each location. Design for maximum stringer reaction.

* Intermediate bents having Type C Bearings, other than the normal fixed bent, shall be designed as if they were fixed bents.

The use of Type C Bearings at intermediate bents is dependent on the column stiffness of the bent and the length of span producing the horizontal deflection due to temperature changes being such that excessive moments are not induced in the columns. Steel or C.I.P. Pile may in general, be considered to be limber enough not to produce resistance to longitudinal forces.

BEARING - DESIGN
(CONTINUED)

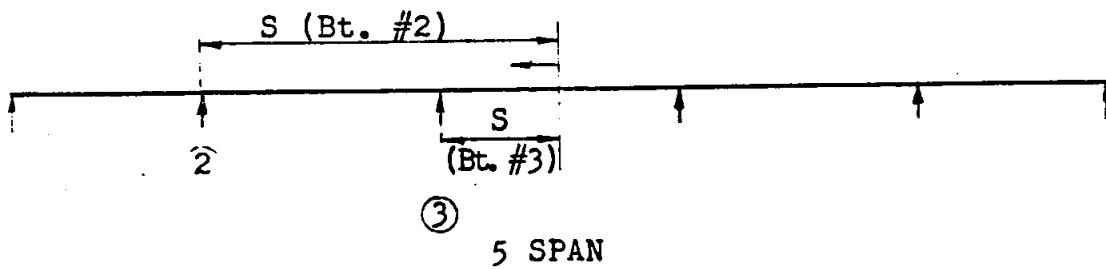
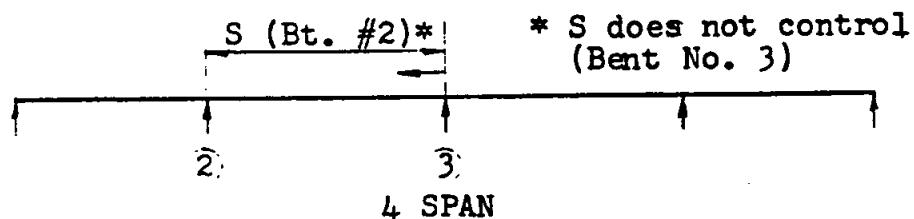
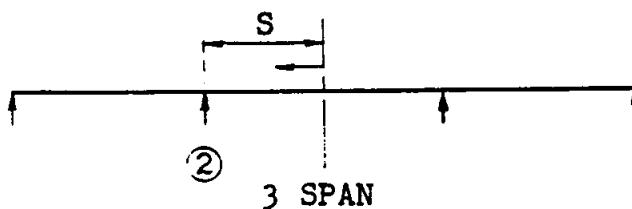
In general, a span/(bent height)² ratio of .05 and over may produce excessive column stresses.

Span = Length of superstructure producing deflection.

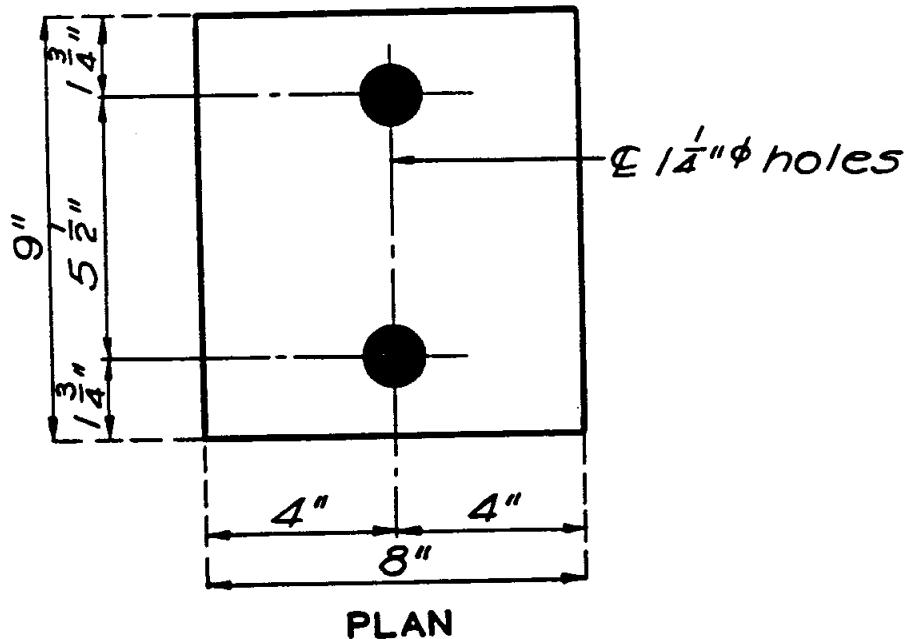
Bent height = Profile Grade to bottom of footing.

$$\frac{S}{h^2} = .05 \quad \text{or} \quad S = .05h^2$$

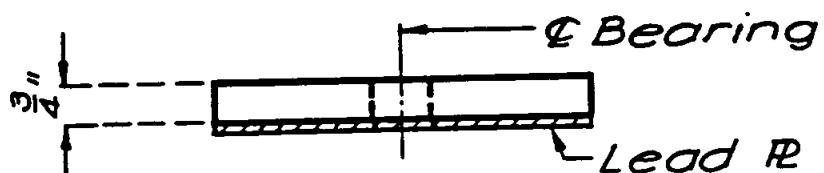
Bent Height (h)	S	RESTRICTING SPAN LENGTHS			
		3 SPAN BRIDGE		5 SPAN BRIDGE	
		(Span #2) BENT #2	(Span #2) BENT #2	(Span #2) BENT #2	(Span #3) BENT #3
15'	11.25'	22.5'	11.25'	11.25' - $\frac{1}{2}$ Span #3	22.5'
20'	20'	40'	20'	20' -	40'
25'	31.25'	62.5'	31.25'	31.25' -	62.5'
30'	45'	90'	45'	45' -	90'
40'	80'	160'	80'	80' -	160'
50'	125'	250'	125'	125' -	250'
60'	180'	360'	180'	180' -	360'
65'	211'	422'	211'	211' -	422'



DETAILS OF FLAT PLATE BEARING



PLAN

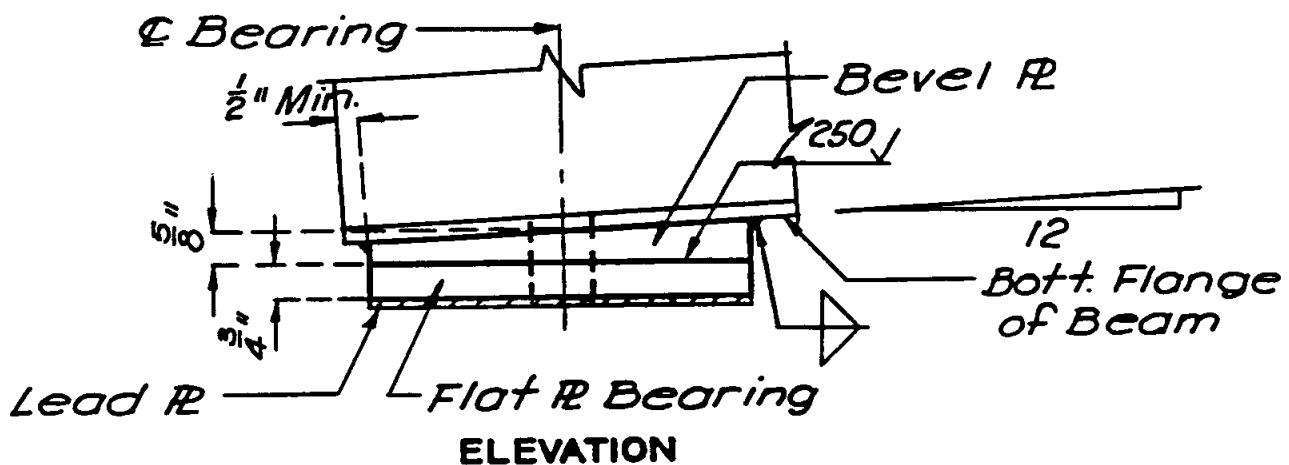
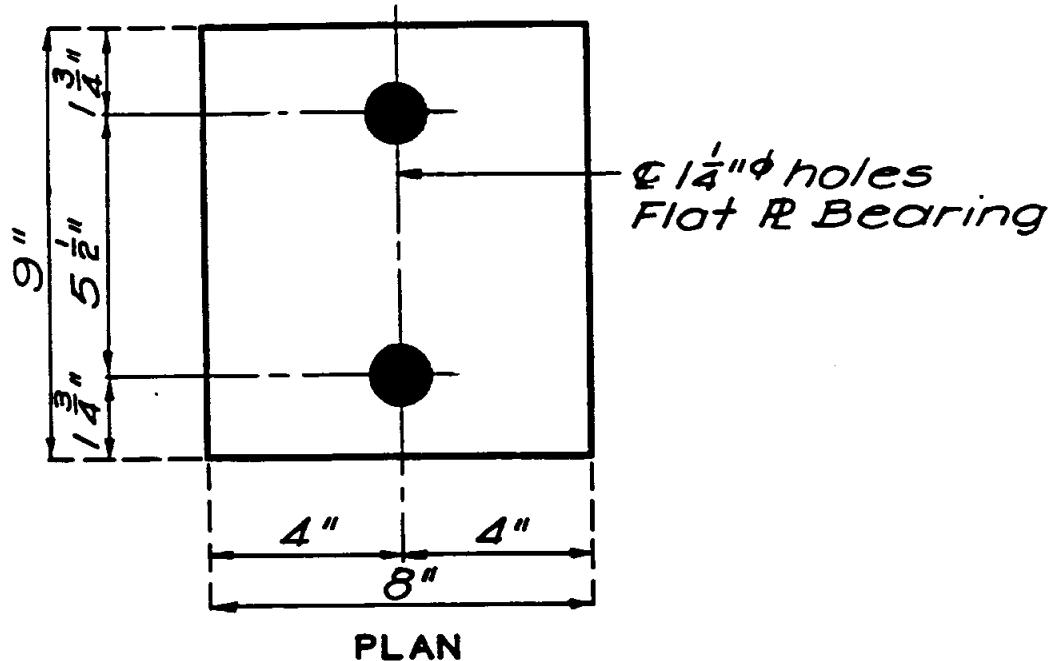


ELEVATION

Estimated Weight = 14.78 lbs. per bearing

Flat plate bearings shall be used on span lengths through 33 feet.

DETAILS OF FLAT PLATE BEARING
WITH BEVEL



Bevel plates are required when roadway grade is
2% or greater.

TYPE "C" BEARINGS

DESIGN DATA:

Steel = A36

$f_s = 20,000 \text{ psi}$

Maximum allowable masonry pressure = 1,000 psi

"P" = capacity of bearing in kips

"e" = eccentricity

(For the design of expansion or contraction for Type "C" Bearings, use 1/16" per 10.0' of span from fixed bearing + 3/8".)

Value of "P" controlled by masonry pressure =

$$P = \frac{Lb - 2.45}{(1 + 6e/b)}$$

Value of "P" controlled by " f_s " =

$$P = 1.333 f_s d^2 (L - 2.5)/b$$

Type "C" Bearings are applicable to Bridges with no more than 80 ft. of expansion.

Type "C" Bearings are only to be used for the cases as specified by the Design Layout or the Chief Designer.

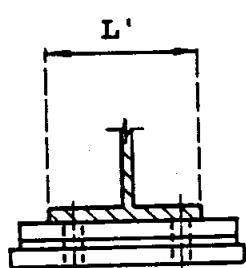
INSTRUCTIONS FOR USE OF THE STANDARD

Enter the table No. 1 with the minimum (L) and determine the proper bearing for the required capacity.

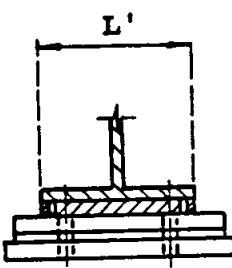
Use greater (L) if the larger capacity is required or the bearing produced will adapt itself better to the skew, sub-structure beam width, etc.

Overhang of the top plate of the bearing beyond the flange (L') or the flange plate width (L') (see sketches "A", "B", "C" or "D") controls the thickness of the top plate.

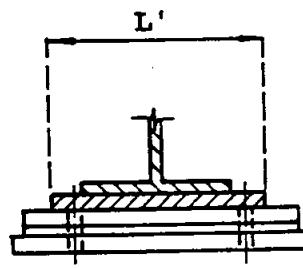
Determine the thickness of the top plate by consulting chart No. 1 of this Manual Section.



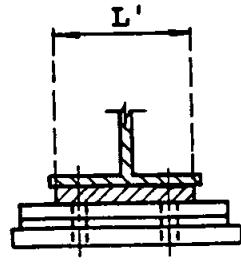
SKETCH "A"



SKETCH "B"



SKETCH "C"



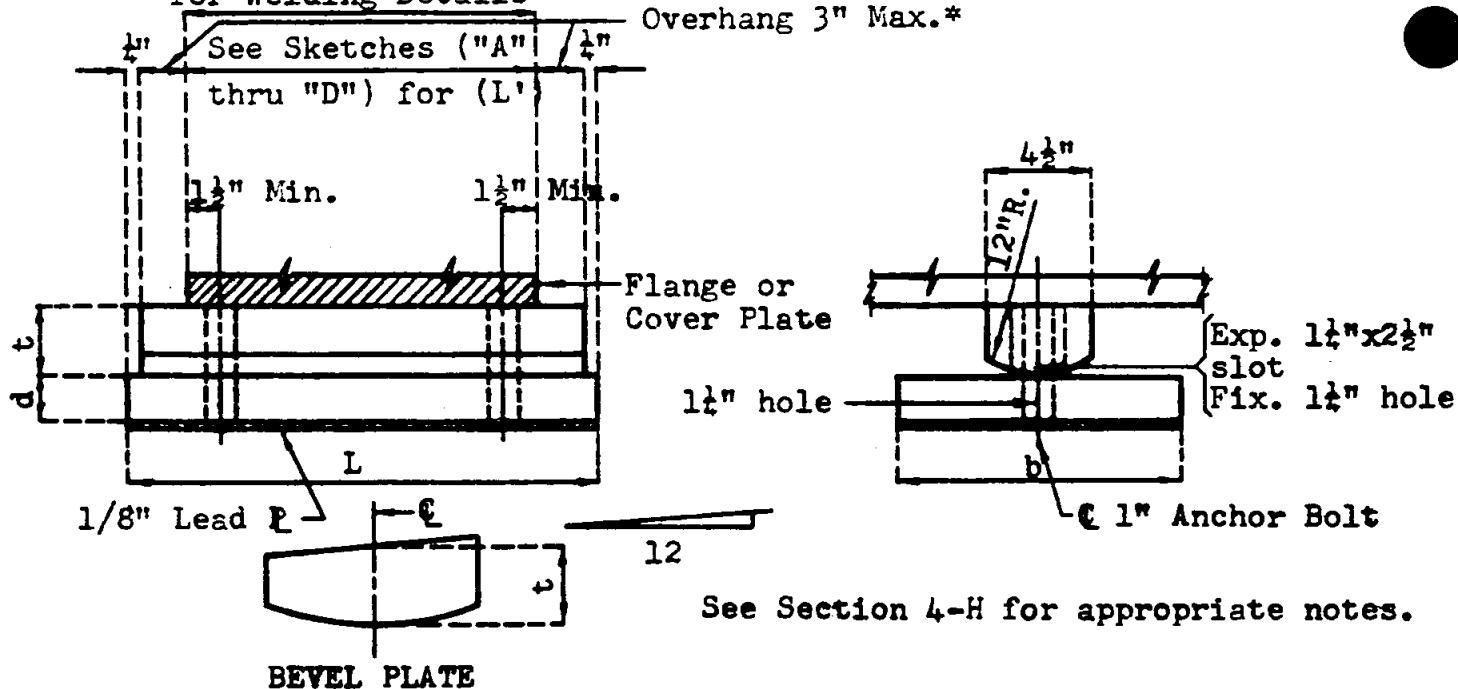
SKETCH "D"

NO FLANGE PLATES

FLANGE PLATES

TYPE "C" BEARING

See following sheet
for Welding Details



BEVEL PLATES: Bevel Rocker Plate when roadway grade is 4% or greater.

* Rocker Plate length shall not be less than Bottom Flange or Cover Plate width.

TYPICAL DETAILS OF TYPE "C" BEARINGS

TABLE NO. 1 - CAPACITY IN KIPS

L	b x d (inches)						
	8 x 1	8 x 1 1/8	8 x 1 1/4	9 x 1 1/2	10 x 1 3/4	11 x 2	12 x 2 1/4
10 1/2"	26.6K	33.7K	41.6K	53.4K	65.4K	77.6K	90.0K
11"	28.3	35.8	44.2	56.7	69.5	82.4	95.6
11 1/2"	29.9	37.9	46.8	60.0	73.5	87.3	101.2
12"	31.6	40.0	49.4	63.4	77.6	92.1	106.8
12 1/2"	33.2	42.1	52.0	66.7	81.7	97.0	112.5
13"	34.9	44.2	54.6	70.0	85.8	101.8	118.1
13 1/2"	36.6	46.4	57.2	73.4	89.9	106.6	123.7
14"	38.2	48.5	59.8	76.7	94.0	111.5	129.3
14 1/2"	39.9	50.6	62.4	80.0	98.0	116.3	135.0
15"	41.5	52.7	65.0	83.4	102.1	121.2	140.6
15 1/2"	43.2	54.8	67.6	86.7	106.2	126.0	146.2
16"	44.9	56.9	70.2	90.0	110.3	130.9	151.6
16 1/2"	46.5	59.0	72.8	93.4	114.4	135.7	156.4
17"	48.2	61.1	75.4	96.7	118.4	140.6	161.2
17 1/2"	49.8	63.2	78.0	100.0	122.5	145.4	166.0
18"	51.5	65.4	80.6	103.4	126.6	150.3	170.8
18 1/2"	53.2	67.5	83.2	106.7	130.7	155.1	175.6
19"	55.0	69.6	85.9	110.0	134.7	160.0	180.4
19 1/2"	56.7	71.7	88.5	113.3	138.8	164.8	185.2
20"	58.3	73.8	91.1	116.4	142.9	169.7	190.0
20 1/2"	60.0	75.9	93.7	120.0	147.0	174.5	194.8

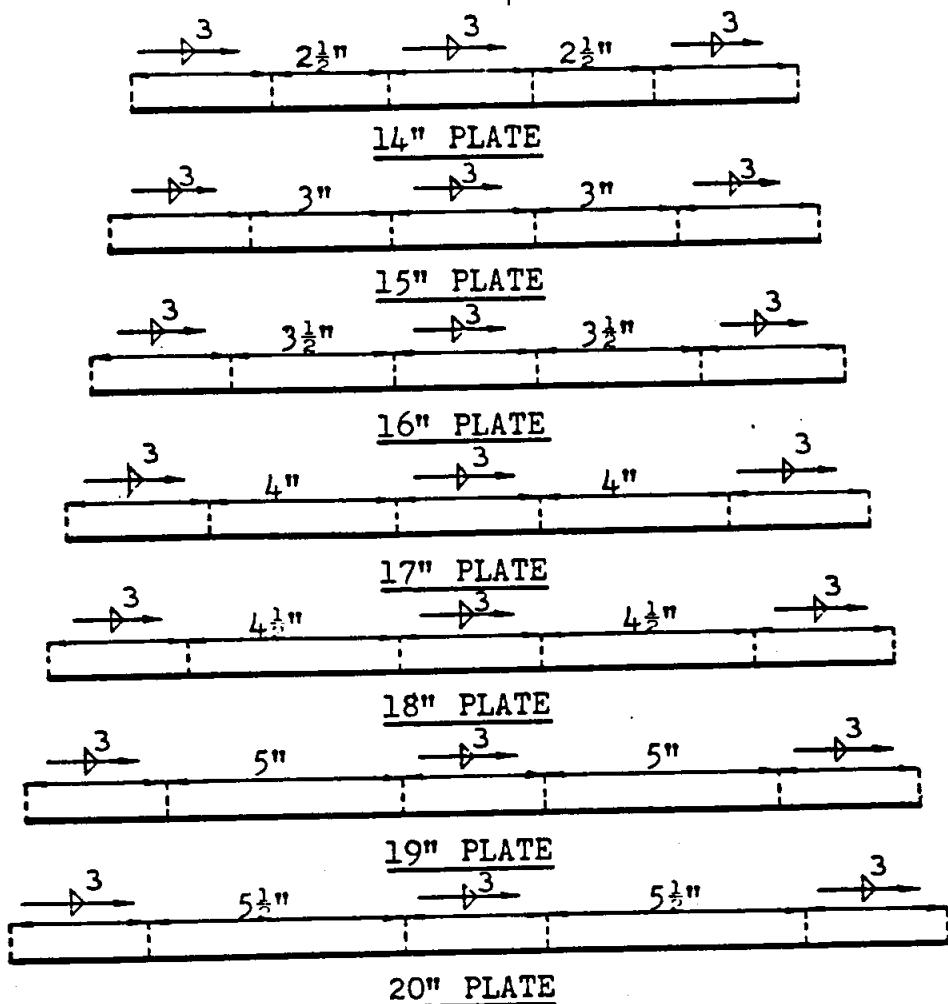
ROCKER PLATE WELDING DETAILS

TYPE "C" BEARINGS

(Rocker Plate to Flange or Cover Plate)

Flange or Cover plates 13" or less in length shall be welded to the rocker plate with a 3" long weld at each corner, transverse to flange.

Flange or Cover plates larger than 13" in length shall be welded to the rocker plate with a series of 3" long welds as shown below.



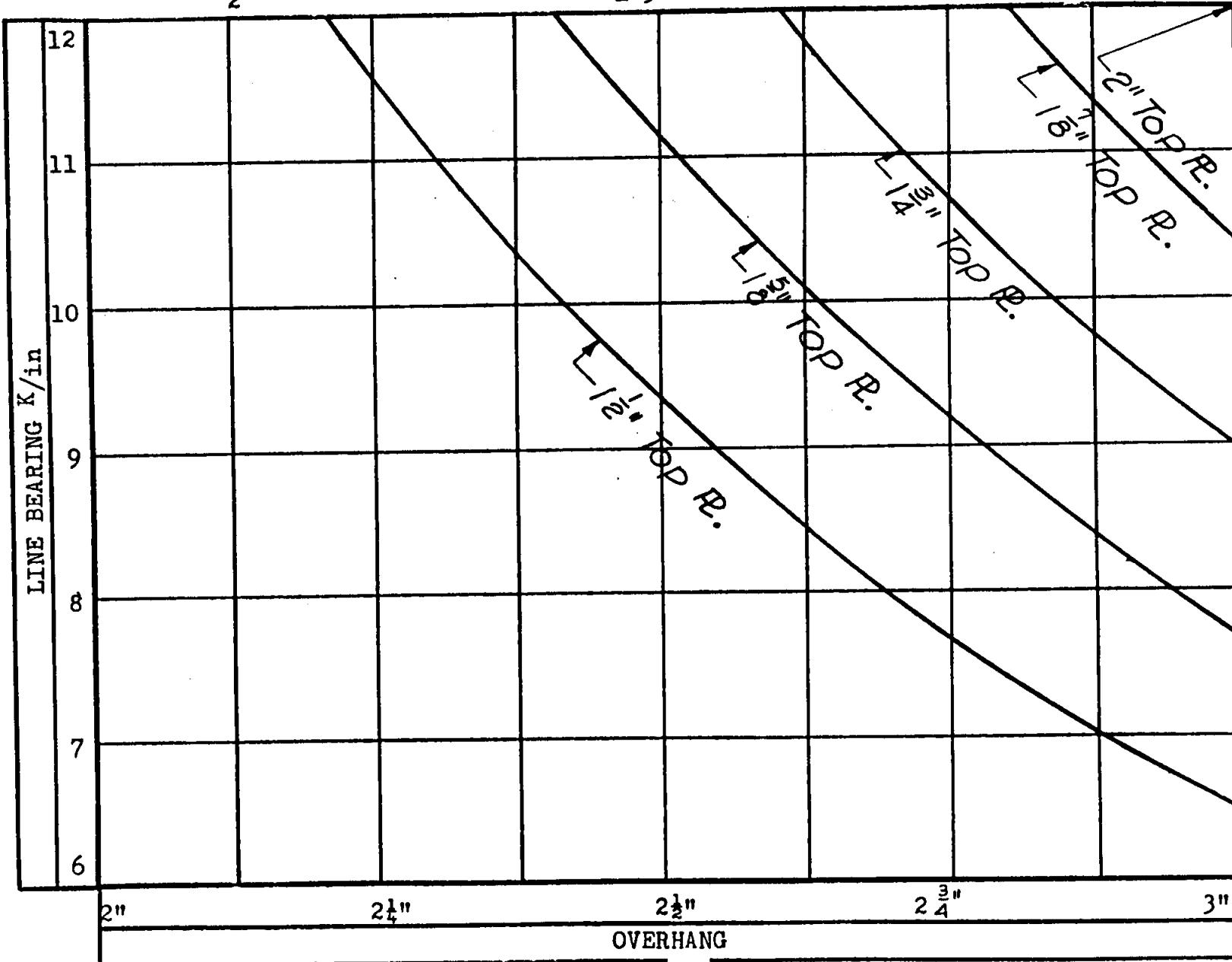
To use chart first calculate Overhang and Line Bearing from formulae shown below. Enter chart with these values and if intersection falls between lines indicating plate thickness use the thicker plate. If the intersection falls on or to the left and below the $1\frac{1}{2}$ " Top Plate line the use of the minimum $1\frac{1}{2}$ " Top Plate thickness is indicated.

$$\text{Over hang} = \frac{L-L!-\frac{1}{2}}{2}$$

$$\text{Line Bearing} = \frac{\text{Reaction}}{L-3''}$$

Top Plate thickness (t)

Min. = $1\frac{1}{2}"$
Max. = $2"$



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1.3.4

1 1/2" 2" 2 1/2"
TOP PLATE
THICKNESS

TYPE "C" BEARING

Weight of anchor bolts is included in weight of bottom plate.
Do not include weight of anchor bolts in the "Estimated Weight" given
on bearing sheet. Deduct 4.5# per bearing for anchor bolts.

TABLE NO. 2 - WEIGHT OF BOTTOM PLATES

Bottom Plate-L	b x d (inches)						
	8x1	8x1 ¹ /8	8x1 ¹ /4	9x1 ¹ /2	10x1 ³ /4	11x2	12x2 ¹ /4
10 ¹ / ₂ "	27.6#	30.5#	33.3#	43.6#	55.3#	68.5#	83.2#
11"	28.7	31.7	34.8	45.5	57.8	71.6	87.0
11 ¹ / ₂ "	29.8	33.0	36.2	47.4	60.3	74.7	90.9
12"	30.9	34.3	37.6	49.3	62.7	77.9	94.7
12 ¹ / ₂ "	32.1	35.6	39.0	51.2	65.2	81.0	98.5
13"	33.2	36.9	40.4	53.1	67.7	84.1	102.4
13 ¹ / ₂ "	34.3	38.1	41.9	55.0	70.2	87.2	106.2
14"	35.5	39.4	43.3	56.9	72.7	90.3	110.0
14 ¹ / ₂ "	36.6	40.7	44.7	58.9	75.1	93.5	113.9
15"	37.7	42.0	46.1	60.8	77.6	96.6	117.7
15 ¹ / ₂ "	38.9	43.3	47.5	62.7	80.1	99.7	121.5
16"	40.0	44.5	49.0	64.6	82.6	102.8	125.3
16 ¹ / ₂ "	41.1	45.8	50.4	66.5	85.1	105.9	129.2
17"	42.2	47.1	51.8	68.4	87.5	109.1	133.0
17 ¹ / ₂ "	43.4	48.4	53.2	70.3	90.0	112.2	136.8
18"	44.5	49.7	54.6	72.2	92.5	115.3	140.7
18 ¹ / ₂ "	45.6	50.9	56.1	74.1	95.0	118.4	144.5
19"	46.8	52.2	57.5	76.0	97.5	121.5	148.3
19 ¹ / ₂ "	47.9	53.5	58.9	78.0	99.9	124.7	152.2
20"	49.0	54.8	60.3	79.9	102.4	127.8	156.0
20 ¹ / ₂ "	50.2	56.1	61.7	81.8	104.9	130.9	159.8

TABLE NO. 3 - WEIGHT OF TOP PLATE EXP. BRG.

Bottom Plate-L	t (PL thickness - inches)				
	1 ¹ / ₂	1 ⁵ / ₈	1 ³ / ₄	1 ⁷ / ₈	2
10 ¹ / ₂ "	16.1#	17.5#	19.0#	20.4#	21.8#
11"	17.0	18.5	20.1	21.6	23.1
11 ¹ / ₂ "	17.9	19.5	21.1	22.7	24.3
12"	18.9	20.5	22.2	23.9	25.5
12 ¹ / ₂ "	19.8	21.5	23.3	25.0	26.8
13"	20.7	22.5	24.3	26.2	28.0
13 ¹ / ₂ "	21.6	23.5	25.4	27.3	29.2
14"	22.5	24.5	26.5	28.5	30.5
14 ¹ / ₂ "	23.4	25.5	27.6	29.6	31.7
15"	24.3	26.5	28.6	30.8	32.9
15 ¹ / ₂ "	25.2	27.5	29.7	31.9	34.2
16"	26.1	28.5	30.8	33.1	35.4
16 ¹ / ₂ "	27.1	29.5	31.8	34.2	36.6
17"	28.0	30.4	32.9	35.4	37.9
17 ¹ / ₂ "	28.9	31.4	34.0	36.5	39.1
18"	29.8	32.4	35.1	37.7	40.3
18 ¹ / ₂ "	30.7	33.4	36.1	38.8	41.5
19"	31.6	34.4	37.2	40.0	42.8
19 ¹ / ₂ "	32.5	35.4	38.3	41.2	44.0
20"	33.4	36.4	39.4	42.3	45.3
20 ¹ / ₂ "	34.3	37.4	40.4	43.5	46.5

TABLE NO. 4
FIXED BRG.

t	Added Weight
1-1/2"	1.1#
1-5/8"	1.1#
1-3/4"	1.2#
1-7/8"	1.3#
2"	1.4#

For weight of top plate for fixed bearing combine the weight in TABLES NO. 3 and NO. 4

TYPE "D" BEARINGS

EXPANSION

DESIGN DATA: Steel A-36, $f_s = 20,000$ psi
 Maximum allowable Masonry Pressure = 1,000 psi

ANCHOR BOLT SPACING: Use same anchor bolt spacing for all interior bents when difference in spacing would be 1" or less. If necessary, increase appropriate masonry plate size to accomodate larger spacing. (Use 1 $\frac{1}{4}$ " A.B. except for 2 Girder Design in which case use 1 $\frac{1}{2}$ " A.B.)

EXPANSION BEARINGS: Value of "P" controlled by Masonry Pressure.

$$\begin{array}{ll} \text{"e" IN MIDDLE } 1/3 & \text{"e" OUT OF MIDDLE } 1/3 \\ "P_c" = \frac{Lb - (3.53)*}{1 + 6e/b} & "P_c" = \frac{3(b/2 - e)L - (3.53)*}{2} \end{array}$$

Value of "P" controlled by Steel Stress.

$$"P_s" = \frac{1.333 \text{ fsl}^2 [L - (3**)]}{b}$$

* Use 4.81 for 1-3/4" holes (1 $\frac{1}{4}$ " A.B.)

** Use 3.5 for 1-3/4" holes (1 $\frac{1}{4}$ " A.B.)

BEVEL PLATES: Not required

P = Capacity of Bearing in Kips

b = Width of bottom plate

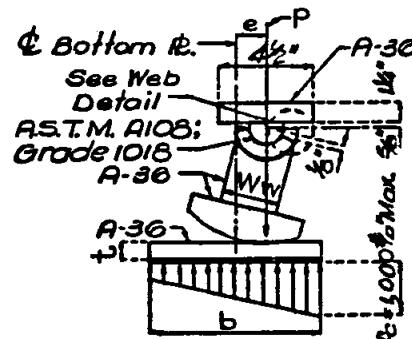
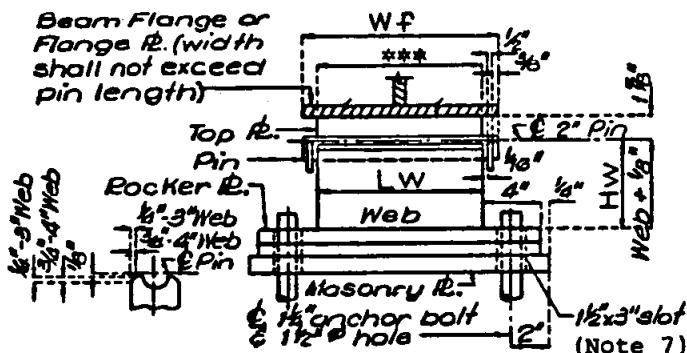
L = Length of bottom plate

e = Eccentricity ****

t = Bottom plate thickness

Length of span or spans	60'	80'	100'	180'	260'	340'	420'
Eccentricity to use	3/4"	7/8"	1"	1 $\frac{1}{2}$ "	2"	2 $\frac{1}{2}$ "	3"

**** Design of expansion or contraction for Type "D" Bearings.
 (Use 1/16" per 10' of span from fixed bearing + 3/8".)



*** Length of top plate shall not be less than out to out dimensions of stiff. plates. (Normal to web.)

NOTES TO DESIGNER:

1. Strive to obtain as much duplication as possible in machined bearing parts (rocker assemblies) within bridges and projects.
2. $L_w \leq W_f + 3"$.
3. $H_w \leq 2W_w$.
4. W_w exceeds 4" use 3" Pin.
5. A vertical line from Pin shall not fall outside web at maximum eccentricity.
6. Masonry Plate thickness and Rocker Plate thickness shall be in increments of $\frac{1}{4}$ ".
7. For $2" < e \leq 2.5"$ use 1 $\frac{1}{4}$ " x 1-3/4" and 1 $\frac{1}{4}$ " x 3 $\frac{1}{2}$ " slot Bottom and Top of Rocker plate respectively.
- For $2.5" < e \leq 3"$ use 1 $\frac{1}{4}$ " x 2" and 1 $\frac{1}{4}$ " x 4" slot Bottom and Top of Rocker plate respectively.

NOTE: For Bridges having roadway widths of 68' and greater without Longitudinal Expansion Joints in the slab and for curved Bridges, bearings under exterior and interior girder lines shall accomodate lateral movements of superstructure due to temperature changes. See Structural Design Engineer for type of Bearings to be used for each Bridge in the above catagories.

TYPE "D" BEARINGS
EXPANSION (CONT)

(MASONRY STRAIGHTS ONLY)

Beam Depth	Capacity in Kips e=3/4" e=7/8" e=1" e=1-1/8" e=2"					Masonry Plate	Top Plate	Web	Rocker Plate	Radius	Height (No Lead Plate)	*Weight
W21	82	78	73	58	46	8x1x16 $\frac{1}{2}$	8x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	3x4-5/8x8	6x1-3/4x16	6 $\frac{1}{2}$	9-3/8	124
				67	64	8x1 $\frac{1}{2}$ x16 $\frac{1}{2}$	8x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	3x4-5/8x8	6x1-3/4x16	6 $\frac{1}{2}$	9-7/8	142
	103	97	93	77	64	9x1 $\frac{1}{2}$ x17 $\frac{1}{2}$	9x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	3x4-5/8x9	6x1-3/4x17	6 $\frac{1}{2}$	9-5/8	150
	125	119	113	96	80	10x1-3/4x18 $\frac{1}{2}$	10x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	3x4-3/8x10	6x2x17	6 $\frac{1}{2}$	10-1/8	177
	150	143	137	116	99	11x2x19 $\frac{1}{2}$	11x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	3x4-7/8x11	6x2x18	6 $\frac{1}{2}$	10-1/8	200
									6x2x19	7	10-7/8	243
W24	87	82	78	62	49	8x1x17 $\frac{1}{2}$	9x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	3x4-5/8x9	6x1-3/4x17	6 $\frac{1}{2}$	9-3/8	135
				72	66	8x1 $\frac{1}{2}$ x17 $\frac{1}{2}$	9x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	3x4-5/8x9	6x1-3/4x17	6 $\frac{1}{2}$	9-7/8	154
	109	103	98	82	67	9x1-3/4x18 $\frac{1}{2}$	10x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	3x4-5/8x10	6x1-3/4x18	6 $\frac{1}{2}$	9-5/8	162
	125	119	114	96	81	10x1-3/4x18 $\frac{1}{2}$	10x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	3x4-3/8x10	6x2x18	6 $\frac{1}{2}$	10-1/8	200
	150	143	137	116	100	11x2x19 $\frac{1}{2}$	11x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	3x5-3/8x11	6x2x19	7 $\frac{1}{2}$	11-3/8	248
	176	169	162	139	121	12x2 $\frac{1}{4}$ x20 $\frac{1}{2}$	12x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	3x5-3/8x12	6x2x20	7 $\frac{1}{2}$	11-5/8	293
W27	92	87	83	66	52	8x1x18 $\frac{1}{2}$	10x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	3x4-5/8x10	6x1-3/4x18	6 $\frac{1}{2}$	9-3/8	146
				72	66	8x1 $\frac{1}{2}$ x18 $\frac{1}{2}$	10x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	3x4-5/8x10	6x1-3/4x18	6 $\frac{1}{2}$	9-7/8	166
	108	103	98	81	66	9x1-3/4x18 $\frac{1}{2}$	10x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	3x4-5/8x10	6x1-3/4x18	6 $\frac{1}{2}$	9-5/8	162
				93	80	10x1 $\frac{1}{2}$ x18 $\frac{1}{2}$	10x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	3x4-5/8x10	6x1-3/4x18	6 $\frac{1}{2}$	10-1/8	185
	125	119	113	96	80	10x1-3/4x18 $\frac{1}{2}$	10x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	3x4-3/8x10	6x2x18	6 $\frac{1}{2}$	10-1/8	200
	144	143	136	116	99	11x1-3/4x19 $\frac{1}{2}$	11x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	3x4-3/8x11	6x2x19	6 $\frac{1}{2}$	10-3/8	238
W30	176	169	162	139	121	12x2 $\frac{1}{4}$ x20 $\frac{1}{2}$	12x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	4x6-3/8x12	7x2x20	8 $\frac{1}{2}$	12-5/8	333
	205	197	189	163	144	13x2 $\frac{1}{4}$ x21 $\frac{1}{2}$	13x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	4x6-3/8x13	7x2x21	8 $\frac{1}{2}$	12-7/8	387
	95	90	85	68	53	8x1x19	10 $\frac{1}{2}$ x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	3x4-5/8x10 $\frac{1}{2}$	6x1-3/4x18 $\frac{1}{2}$	6 $\frac{1}{2}$	9-3/8	151
				74	69	8x1 $\frac{1}{2}$ x19	10 $\frac{1}{2}$ x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	3x4-5/8x10 $\frac{1}{2}$	6x1-3/4x18 $\frac{1}{2}$	6 $\frac{1}{2}$	9-7/8	172
	111	105	100	84	68	9x1-3/4x19	10 $\frac{1}{2}$ x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	3x4-5/8x10 $\frac{1}{2}$	6x1-3/4x18 $\frac{1}{2}$	6 $\frac{1}{2}$	9-5/8	168
				102	86	10x1 $\frac{1}{2}$ x20	11 $\frac{1}{2}$ x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	3x4-5/8x11 $\frac{1}{2}$	6x1-3/4x19 $\frac{1}{2}$	6 $\frac{1}{2}$	10-1/8	192
135	129	122	103	86	10x1-3/4x20	11 $\frac{1}{2}$ x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	3x4-3/8x11 $\frac{1}{2}$	6x2x19 $\frac{1}{2}$	6 $\frac{1}{2}$	10-1/8	220	
			126	119	101	11x1-3/4x20	11 $\frac{1}{2}$ x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	3x4-3/8x11 $\frac{1}{2}$	6x2x19 $\frac{1}{2}$	6 $\frac{1}{2}$	10-1/8	230
	147	140	119	101	11x2x20	11 $\frac{1}{2}$ x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	3x4-3/8x11 $\frac{1}{2}$	6x2x19 $\frac{1}{2}$	6 $\frac{1}{2}$	10-3/8	246	
			148	135	118	12x2x20	11 $\frac{1}{2}$ x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	3x4-3/8x11 $\frac{1}{2}$	6x2x19 $\frac{1}{2}$	6 $\frac{1}{2}$	10-3/8	252
	200	192	184	159	140	13x2 $\frac{1}{4}$ x21	12 $\frac{1}{2}$ x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	4x6-7/8x12 $\frac{1}{2}$	7x2x20 $\frac{1}{2}$	9	13-3/8	384
	230	221	213	185	164	14x2-3/4x22	13 $\frac{1}{2}$ x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	4x6-5/8x13 $\frac{1}{2}$	7x2 $\frac{1}{4}$ x21 $\frac{1}{2}$	9	13-5/8	450

*Weight does not include 2 anchor bolts @ 12#

NOTE: For required capacities larger than those provided by these tables, see following pages this section.

Beam Depth	Capacity in Kips e=3/4" e=7/8" e=1" e=1-1/4" e=2"				Masonry Plate	Top Plate	Web	Rocker Plate	Radius	Height (No Lead Plate)	*Weight		
W33	100	94	89	71	56	8x1x20	11 $\frac{1}{2}$ x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-5/8x11 $\frac{1}{2}$	6x1-3/4x19 $\frac{1}{2}$	6 $\frac{1}{4}$	9-3/8	162	
				79	56	8x1 $\frac{1}{4}$ x20	11 $\frac{1}{2}$ x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-5/8x11 $\frac{1}{2}$	6x1-3/4x19 $\frac{1}{2}$	6 $\frac{1}{4}$	9-7/8	184	
	118	111	106	88	71	9x1 $\frac{1}{4}$ x20	11 $\frac{1}{2}$ x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-5/8x11 $\frac{1}{2}$	6x1-3/4x19 $\frac{1}{2}$	6 $\frac{1}{4}$	9-5/8	180	
				108	91	10x1 $\frac{1}{4}$ x21	12 $\frac{1}{2}$ x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-5/8x12 $\frac{1}{2}$	6x1-3/4x20 $\frac{1}{2}$	6 $\frac{1}{4}$	9-7/8	214	
	142	135	129	109	91	10x1-3/4x21	12 $\frac{1}{2}$ x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-3/8x12 $\frac{1}{2}$	6x2x20 $\frac{1}{2}$	6 $\frac{1}{4}$	10-1/8	234	
			134	125	107	11x1-3/4x21	12 $\frac{1}{2}$ x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-3/8x12 $\frac{1}{2}$	6x2x20 $\frac{1}{2}$	6 $\frac{1}{4}$	10-1/8	242	
	157	154	147	125	107	11x2x21	12 $\frac{1}{2}$ x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-3/8x12 $\frac{1}{2}$	6x2x20 $\frac{1}{2}$	6 $\frac{1}{4}$	10-3/8	258	
			157	142	124	12x2x21	12 $\frac{1}{2}$ x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-3/8x12 $\frac{1}{2}$	6x2x20 $\frac{1}{2}$	6 $\frac{1}{4}$	10-3/8	270	
			187	184	159	140	13x2 $\frac{1}{4}$ x21	12 $\frac{1}{2}$ x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	4x7-7/8x12 $\frac{1}{2}$	7x2x20 $\frac{1}{2}$	10	14-1/8	380
	200	191	184	159	140	13x2 $\frac{1}{4}$ x21	12 $\frac{1}{2}$ x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	4x7-7/8x12 $\frac{1}{2}$	7x2x20 $\frac{1}{2}$	10	14-3/8	399	
W36	226	221	212	185	164	14x2 $\frac{1}{4}$ x22	13 $\frac{1}{2}$ x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	4x7-7/8x13 $\frac{1}{2}$	7x2x21 $\frac{1}{2}$	10	14-3/8	438	
	263	253	244	213	190	15x2-3/4x23	14 $\frac{1}{2}$ x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	4x7-5/8x14 $\frac{1}{2}$	7x2 $\frac{1}{4}$ x22 $\frac{1}{2}$	10	14-5/8	510	
W36	103	97	92	73	58	8x1x20 $\frac{1}{2}$	12x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-5/8x12	6x1-3/4x20	6 $\frac{1}{4}$	9-3/8	167	
				73	58	8x1 $\frac{1}{4}$ x20 $\frac{1}{2}$	12x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-5/8x12	6x1-3/4x20	6 $\frac{1}{4}$	9-7/8	190	
	121	114	109	90	73	9x1 $\frac{1}{4}$ x20 $\frac{1}{2}$	12x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-5/8x12	6x1-3/4x20	6 $\frac{1}{4}$	9-5/8	186	
				105	89	10x1 $\frac{1}{4}$ x20 $\frac{1}{2}$	12x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-5/8x12	6x1-3/4x20	6 $\frac{1}{4}$	10-1/8	211	
	139	132	126	106	89	10x1-3/4x20 $\frac{1}{2}$	12x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-3/8x12	6x2x20	6 $\frac{1}{4}$	9-7/8	207	
			137	128	109	11x1-3/4x21 $\frac{1}{2}$	13x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-3/8x13	6x2x21	6 $\frac{1}{4}$	10-1/8	227	
	165	158	151	128	109	11x2x21 $\frac{1}{2}$	13x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-3/8x13	6x2x21	6 $\frac{1}{4}$	10-3/8	249	
			161	145	127	12x2x21 $\frac{1}{2}$	13x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-3/8x13	6x2x21	6 $\frac{1}{4}$	10-3/8	266	
			192	189	163	143	13x2 $\frac{1}{4}$ x21 $\frac{1}{2}$	13x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	4x7-7/8x13	7x2 $\frac{1}{4}$ x21	10 $\frac{1}{4}$	14-5/8	412
	205	196	189	163	143	13x2 $\frac{1}{4}$ x21 $\frac{1}{2}$	13x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	4x7-7/8x13	7x2 $\frac{1}{4}$ x21	10 $\frac{1}{4}$	14-7/8	431	
W36	221	216	208	181	160	17x2 $\frac{1}{4}$ x21 $\frac{1}{2}$	13x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	4x7-7/8x13	7x2 $\frac{1}{4}$ x21	10 $\frac{1}{4}$	14-7/8	446	
	257	248	239	209	186	15x2-3/4x22 $\frac{1}{2}$	14x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	4x7-7/8x14	7x2 $\frac{1}{4}$ x22	10 $\frac{1}{4}$	15-1/8	511	
	290	280	271	238	213	16x3x23 $\frac{1}{2}$	15x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	4x7-7/8x15	7x2 $\frac{1}{4}$ x23	10 $\frac{1}{4}$	15-3/8	583	

*Weight does not include 2 anchor bolts @ 12#

NOTE: For required capacities larger than those provided by these tables, see following tables this section.

TYPE "D" BEARINGS
 EXPANSION (CONT.)
 (WIDE FLANGE STRINGERS ONLY)

REVISED FEB. 1980

SEC. 3.31

1.4.4

ALLOWABLE SPANNING = 2"

(Expansion Joint)

Bottom Flange width	Capacity in Kips					Masonry Plate	Top Plate	Web	Rocker Plate	Radius	Height (No Lead Plate)	*Weight
	e=3/4"	e=7/8"	e=1"	e=1 1/4"	e=2"							
8"	45	8x1 1/4x16 1/2	8x1 1/4x4 1/2	3x4-5/8x8	6x1-3/4x16	6 1/2	9-3/8	124				
	82	78	73	58	46	8x1 1/4x16 1/2	8x1 1/4x4 1/2	3x4-5/8x8	6x1-3/4x16	6 1/2	9-7/8	142
				67	64	9x1 1/4x17 1/2	9x1 1/4x4 1/2	3x4-5/8x9	6x1-3/4x17	6 1/2	9-5/8	150
	103	97	93	77	64	9x1-3/4x17 1/2	9x1 1/4x4 1/2	3x4-3/8x9	6x2x17	6 1/2	10-1/8	177
	125	119	113	96	80	10x1-3/4x18 1/2	10x1 1/4x4 1/2	3x4-3/8x10	6x2x18	6 1/2	10-1/8	200
	150	143	137	116	99	11x2x19 1/2	11x1 1/4x4 1/2	3x4-7/8x11	6x2x19	7	10-7/8	243
9"	48	8x1x17 1/2	9x1 1/4x4 1/2	3x4-5/8x9	6x1-3/4x17	6 1/2	9-3/8	135				
	87	82	78	62	49	8x1 1/4x17 1/2	9x1 1/4x4 1/2	3x4-5/8x9	6x1-3/4x17	6 1/2	9-7/8	154
				72	66	9x1 1/4x18 1/2	10x1 1/4x4 1/2	3x4-5/8x10	6x1-3/4x18	6 1/2	9-5/8	162
	109	103	98	82	67	9x1-3/4x18 1/2	10x1 1/4x4 1/2	3x4-5/8x10	6x1-3/4x18	6 1/2	10-1/8	185
	125	119	114	96	81	10x1-3/4x18 1/2	10x1 1/4x4 1/2	3x4-3/8x10	6x2x18	6 1/2	10-1/8	200
	150	143	137	116	100	11x2x19 1/2	11x1 1/4x4 1/2	3x5-3/8x11	6x2x19	7 1/2	11-3/8	248
10"	176	169	162	139	121	12x2 1/4x20 1/2	12x1 1/4x4 1/2	3x5-3/8x12	6x2x20	7 1/2	11-5/8	293
	92	87	83	66	52	8x1x18 1/2	10x1 1/4x4 1/2	3x4-5/8x10	6x1-3/4x18	6 1/2	9-3/8	146
				72	66	9x1 1/4x18 1/2	10x1 1/4x4 1/2	3x4-5/8x10	6x1-3/4x18	6 1/2	9-7/8	166
	108	103	98	81	66	9x1-3/4x18 1/2	10x1 1/4x4 1/2	3x4-5/8x10	6x1-3/4x18	6 1/2	9-5/8	162
				93	80	10x1 1/4x18 1/2	10x1 1/4x4 1/2	3x4-5/8x10	6x1-3/4x18	6 1/2	10-1/8	185
	125	119	113	96	80	10x1-3/4x18 1/2	10x1 1/4x4 1/2	3x4-3/8x10	6x2x18	6 1/2	9-7/8	182
12"			123	116	99	11x1-3/4x19 1/2	11x1 1/4x4 1/2	3x4-3/8x11	6x2x19	6 1/2	10-1/8	200
	144	143	136	116	99	11x2x19 1/2	11x1 1/4x4 1/2	3x4-3/8x11	6x2x19	6 1/2	10-3/8	223
	176	169	162	139	121	12x2 1/4x20 1/2	12x1 1/4x4 1/2	4x6-3/8x12	7x2x20	8 1/2	12-5/8	238
	205	197	189	163	144	13x2 1/4x21 1/2	13x1 1/4x4 1/2	4x6-3/8x13	7x2x21	8 1/2	12-7/8	387

*Weight does not include 2 anchor bolts @ 12#

<u>Bottom Flange Width</u>	<u>Capacity in Kips</u> <u>e=3/4"</u> <u>e=7/8"</u> <u>e=1"</u> <u>e=1 1/4"</u> <u>e=2"</u>					<u>Masonry Plate</u>	<u>Top Plate</u>	<u>Web</u>	<u>Rocker</u>	<u>Radius</u>	<u>Height (No Lead Plate)</u>	<u>*Weight</u>		
11"	98	92	87	70	55	8x1x19 $\frac{1}{2}$	11x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-5/8x11	6x1-3/4x19	6 $\frac{1}{4}$	9-3/8	156		
					55	8x1 $\frac{1}{4}$ x19 $\frac{1}{2}$	11x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-5/8x11	6x1-3/4x19	6 $\frac{1}{4}$	9-7/8	178		
					81	9x1 $\frac{1}{4}$ x20 $\frac{1}{2}$	12x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-5/8x12	6x1-3/4x20	6 $\frac{1}{4}$	9-5/8	186		
	121	114	109	90	73	9x1-3/4x20 $\frac{1}{2}$	12x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-5/8x12	6x1-3/4x20	6 $\frac{1}{4}$	10-1/8	211		
					111	10x1 $\frac{1}{4}$ x21 $\frac{1}{2}$	13x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-5/8x13	6x1-3/4x21	6 $\frac{1}{4}$	9-7/8	220		
	146	139	132	111	93	10x1-3/4x21 $\frac{1}{2}$	13x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-3/8x13	6x2x21	6 $\frac{1}{4}$	10-1/8	241		
					137	128	109	11x1-3/4x21 $\frac{1}{2}$	13x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-3/8x13	6x2x21	6 $\frac{1}{4}$	10-1/8	249
	165	158	151	128	109	11x2x21 $\frac{1}{2}$	13x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-3/8x13	6x2x21	6 $\frac{1}{4}$	10-3/8	266		
	194	185	178	152	133	12x2 $\frac{1}{4}$ x22 $\frac{1}{2}$	14x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x5-7/8x14	6x2x22	8	12-1/8	334		
	210	206	198	171	150	13x2 $\frac{1}{4}$ x22 $\frac{1}{2}$	14x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x5-7/8x14	6x2x22	8	12-3/8	369		
12"	103	97	92	75	59	8x1x20 $\frac{1}{2}$	12x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-5/8x12	6x1-3/4x20	6 $\frac{1}{4}$	9-3/8	167		
					60	8x1 $\frac{1}{4}$ x20 $\frac{1}{2}$	12x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-5/8x12	6x1-3/4x20	6 $\frac{1}{4}$	9-7/8	190		
					73	9x1 $\frac{1}{4}$ x20 $\frac{1}{2}$	12x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-5/8x12	6x1-3/4x20	6 $\frac{1}{4}$	9-5/8	186		
	120	114	108	90	75	9x1-3/4x20 $\frac{1}{2}$	12x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-5/8x12	6x1-3/4x20	6 $\frac{1}{4}$	10-1/8	211		
					111	93	10x1 $\frac{1}{4}$ x21 $\frac{1}{2}$	13x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-5/8x13	6x1-3/4x21	6 $\frac{1}{4}$	9-7/8	220	
	146	139	132	111	93	10x1-3/4x21 $\frac{1}{2}$	13x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-3/8x13	6x2x21	6 $\frac{1}{4}$	10-1/8	241		
					137	128	109	11x1-3/4x21 $\frac{1}{2}$	13x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-3/8x13	6x2x21	6 $\frac{1}{4}$	10-1/8	249
	165	158	151	128	109	11x2x21 $\frac{1}{2}$	13x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-3/8x13	6x2x21	6 $\frac{1}{4}$	10-3/8	266		
	224	215	207	178	157	12x2 $\frac{1}{4}$ x22 $\frac{1}{2}$	14x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-3/8x14	6x2x22	6 $\frac{1}{4}$	10-1/8	295		
	244	237	228	198	175	13x2 $\frac{1}{4}$ x23 $\frac{1}{2}$	15x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	4x6-7/8x15	7x2x23	9	13-3/8	434		
13"	108	102	96	77	61	8x1x21 $\frac{1}{2}$	13x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-5/8x13	6x1-3/4x21	6 $\frac{1}{4}$	9-3/8	178		
					61	8x1 $\frac{1}{4}$ x21 $\frac{1}{2}$	13x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-5/8x13	6x1-3/4x21	6 $\frac{1}{4}$	9-7/8	202		
					86	9x1 $\frac{1}{4}$ x21 $\frac{1}{2}$	13x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-5/8x13	6x1-3/4x21	6 $\frac{1}{4}$	9-5/8	197		
	127	120	114	95	77	9x1-3/4x21 $\frac{1}{2}$	13x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-5/8x13	6x1-3/4x21	6 $\frac{1}{4}$	10-1/8	224		
					117	98	10x1 $\frac{1}{4}$ x22 $\frac{1}{2}$	14x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-5/8x14	6x1-3/4x22	6 $\frac{1}{4}$	9-7/8	233	
	153	145	138	117	98	10x1-3/4x22 $\frac{1}{2}$	14x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-3/8x14	6x2x22	6 $\frac{1}{4}$	10-1/8	254		
					145	134	115	11x1-3/4x22 $\frac{1}{2}$	14x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-3/8x14	6x2x22	6 $\frac{1}{4}$	10-1/8	265
	170	165	158	134	115	11x2x22 $\frac{1}{2}$	14x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-3/8x14	6x2x22	6 $\frac{1}{4}$	10-3/8	283		
					179	159	139	12x2x23 $\frac{1}{2}$	15x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-3/8x15	6x2x23	6 $\frac{1}{4}$	10-3/8	311
	234	224	216	186	164	13x2 $\frac{1}{4}$ x24 $\frac{1}{2}$	16x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	4x6-7/8x16	7x2x24	9	13-3/8	456		
	256	247	238	207	183	14x2 $\frac{1}{4}$ x24 $\frac{1}{2}$	16x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	4x6-5/8x16	7x2 $\frac{1}{4}$ x24	9	13-3/8	480		

*Weight does not include 2 anchor bolts @ 12#

TYPE "D" BEARINGS
 (EXPANSION (CONT.))
 ALLOWABLE MOVEMENT = 2"

<u>Bottom Flange Width</u>	<u>Capacity in Kips</u> <u>e=3/4"</u> <u>e=7/8"</u> <u>e=1"</u> <u>e=1 1/4"</u> <u>e=2"</u>					<u>Masonry Plate</u>	<u>Top Plate</u>	<u>Web</u>	<u>Rocker</u>	<u>Radius</u>	<u>Height (No Lead Plate)</u>	<u>*Weight</u>		
14"	113	107	101	65	64	8x1x22 $\frac{1}{2}$	14x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-5/8x14	6x1-3/4x22	6 $\frac{1}{4}$	9-3/8	189		
				81	64	8x1 $\frac{1}{4}$ x22 $\frac{1}{2}$	14x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-5/8x14	6x1-3/4x22	6 $\frac{1}{4}$	9-7/8	214		
				90	81	9x1 $\frac{1}{4}$ x22 $\frac{1}{2}$	14x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-5/8x14	6x1-3/4x22	6 $\frac{1}{4}$	9-5/8	209		
	130	126	119	99	81	9x1 $\frac{1}{4}$ x22 $\frac{1}{2}$	14x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-5/8x14	6x1-3/4x22	6 $\frac{1}{4}$	9-7/8	223		
			123	122	102	10x1 $\frac{1}{4}$ x23 $\frac{1}{2}$	15x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-5/8x15	6x1-3/4x23	6 $\frac{1}{4}$	9-7/8	245		
	160	152	145	122	109	10x1-3/4x23 $\frac{1}{2}$	15x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-3/8x15	6x2x23	6 $\frac{1}{4}$	10-1/8	268		
			152	140	120	11x1-3/4x23 $\frac{1}{2}$	15x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-3/8x15	6x2x23	6 $\frac{1}{4}$	10-1/8	280		
	179	173	165	140	120	11x2x23 $\frac{1}{2}$	15x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-3/8x15	6x2x23	6 $\frac{1}{4}$	10-3/8	298		
			188	166	145	12x2x24 $\frac{1}{2}$	16x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-3/8x16	6x2x24	6 $\frac{1}{4}$	10-3/8	326		
	234	224	216	186	164	13x2 $\frac{1}{4}$ x24 $\frac{1}{2}$	16x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	4x7-3/8x16	7x2x24	9 $\frac{1}{4}$	13-7/8	466		
15"	267	257	247	215	190	14x2 $\frac{1}{4}$ x25 $\frac{1}{2}$	17x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	4x7-3/8x17	7x2x25	9 $\frac{1}{4}$	13-7/8	507		
			288	281	271	237	211	15x2-3/4x25 $\frac{1}{2}$	17x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	4x7-1/8x17	7x2 $\frac{1}{4}$ x25	9 $\frac{1}{4}$	14-1/8	558
	118	111	105	68	67	8x1x23 $\frac{1}{2}$	15x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-5/8x15	6x1-3/4x23	6 $\frac{1}{4}$	9-3/8	199		
				85	67	8x1 $\frac{1}{4}$ x23 $\frac{1}{2}$	15x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-5/8x15	6x1-3/4x23	6 $\frac{1}{4}$	9-7/8	225		
				95	85	9x1 $\frac{1}{4}$ x23 $\frac{1}{2}$	15x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-5/8x15	6x1-3/4x23	6 $\frac{1}{4}$	9-5/8	221		
	137	131	125	104	85	9x1 $\frac{1}{4}$ x23 $\frac{1}{2}$	15x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-5/8x15	6x1-3/4x23	6 $\frac{1}{4}$	9-7/8	235		
			129	127	107	10x1 $\frac{1}{4}$ x24 $\frac{1}{2}$	16x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-5/8x16	6x1-3/4x24	6 $\frac{1}{4}$	9-7/8	258		
	167	158	151	127	107	10x1-3/4x24 $\frac{1}{2}$	16x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-3/8x16	6x2x24	6 $\frac{1}{4}$	10-1/8	282		
			160	146	125	11x1-3/4x24 $\frac{1}{2}$	16x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-3/8x16	6x2x24	6 $\frac{1}{4}$	10-1/8	294		
	189	180	172	146	125	11x2x24 $\frac{1}{2}$	16x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-3/8x16	6x2x24	6 $\frac{1}{4}$	10-3/8	313		
16"			200	173	151	12x2x25 $\frac{1}{2}$	17x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-3/8x17	6x2x25	6 $\frac{1}{4}$	10-3/8	342		
	244	234	224	194	171	13x2 $\frac{1}{4}$ x25 $\frac{1}{2}$	17x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	4x7-3/8x17	7x2x25	9 $\frac{1}{4}$	13-7/8	489		
	278	267	257	224	198	14x2 $\frac{1}{4}$ x26 $\frac{1}{2}$	18x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	4x7-3/8x18	7x2x26	9 $\frac{1}{4}$	13-7/8	530		
			302	292	281	246	219	15x2-3/4x26 $\frac{1}{2}$	18x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	4x7-1/8x18	7x2 $\frac{1}{4}$ x26	9 $\frac{1}{4}$	14-1/8	584
	123	116	110	72	70	8x1x24 $\frac{1}{2}$	16x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-5/8x16	6x1-3/4x24	6 $\frac{1}{4}$	9-3/8	210		
				88	70	8x1 $\frac{1}{4}$ x24 $\frac{1}{2}$	16x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-5/8x16	6x1-3/4x24	6 $\frac{1}{4}$	9-7/8	237		
				100	88	9x1 $\frac{1}{4}$ x24 $\frac{1}{2}$	16x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-5/8x16	6x1-3/4x24	6 $\frac{1}{4}$	9-5/8	232		
	143	137	130	108	88	9x1 $\frac{1}{4}$ x24 $\frac{1}{2}$	16x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-5/8x16	6x1-3/4x24	6 $\frac{1}{4}$	9-7/8	248		
			129	127	107	10x1 $\frac{1}{4}$ x24 $\frac{1}{2}$	16x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-5/8x16	6x1-3/4x24	6 $\frac{1}{4}$	9-7/8	258		
	167	158	151	127	107	10x1-3/4x24 $\frac{1}{2}$	16x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-3/8x16	6x2x24	6 $\frac{1}{4}$	10-1/8	282		
			167	152	130	11x1-3/4x25 $\frac{1}{2}$	17x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-3/8x17	6x2x25	6 $\frac{1}{4}$	10-1/8	308		
	197	188	179	152	130	11x2x25 $\frac{1}{2}$	17x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-3/8x17	6x2x25	6 $\frac{1}{4}$	10-3/8	327		
			200	173	151	12x2x25 $\frac{1}{2}$	17x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x4-3/8x17	6x2x25	6 $\frac{1}{4}$	10-3/8	342		
	253	243	233	201	177	13x2 $\frac{1}{4}$ x26 $\frac{1}{2}$	18x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	4x7-7/8x18	7x2 $\frac{1}{4}$ x26	10 $\frac{1}{4}$	14-7/8	547		
.5	278	267	257	224	198	14x2 $\frac{1}{4}$ x26 $\frac{1}{2}$	18x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	4x7-7/8x18	7x2 $\frac{1}{4}$ x26	10 $\frac{1}{4}$	14-7/8	566		
	303	292	256	227	15x2-3/4x27 $\frac{1}{2}$	19x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	4x7-7/8x19	7x2 $\frac{1}{4}$ x27	10 $\frac{1}{4}$	15-1/8	639			
	341	329	317	279	249	16x3x27 $\frac{1}{2}$	19x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	4x7-7/8x19	7x2 $\frac{1}{4}$ x27	10 $\frac{1}{4}$	15-3/8	692		

*Weight does not include 2 anchor bolts @ 12#

SUSPENDED SYSTEMS
SECTION C-2
ALLOWABLE MOMENT = 24

(Expansion Cont.)

<u>Bottom Flange Width</u>	<u>Capacity in Kips</u> <u>e=3/4"</u> <u>e=7/8"</u> <u>e=1"</u> <u>e=1 1/4"</u> <u>e=2"</u>					<u>Masonry Plate</u>	<u>Top Plate</u>	<u>Web</u>	<u>Rocker</u>	<u>Radius</u>	<u>Height (No Lead Plate)</u>	<u>*Weight</u>	
17"													
	128	121	115	75	73	8x1x25 $\frac{1}{4}$	17x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	3x4-5/8x17	6x1-3/4x25	6 $\frac{1}{4}$	9-3/8	221	
				92	73	8x1 $\frac{1}{4}$ x25 $\frac{1}{4}$	17x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	3x4-5/8x17	6x1-3/4x25	6 $\frac{1}{4}$	9-7/8	249	
	151	143	136	113	92	9x1 $\frac{1}{4}$ x25 $\frac{1}{4}$	17x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	3x4-5/8x17	6x1-3/4x25	6 $\frac{1}{4}$	9-5/8	244	
				135	132	111	10x1 $\frac{1}{4}$ x25 $\frac{1}{4}$	17x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	3x4-5/8x17	6x1-3/4x25	6 $\frac{1}{4}$	9-7/8	260
	173	165	157	132	111	10x1-3/4x25 $\frac{1}{4}$	17x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	3x4-3/8x17	6x2x25	6 $\frac{1}{4}$	10-1/8	295	
				174	158	136	11x1-3/4x26 $\frac{1}{4}$	18x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	3x4-3/8x18	6x2x26	6 $\frac{1}{4}$	10-1/8	322
	204	195	186	158	136	11x2x26 $\frac{1}{4}$	18x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	3x4-3/8x18	6x2x26	6 $\frac{1}{4}$	10-3/8	342	
				206	180	157	12x2x26 $\frac{1}{4}$	18x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	3x4-3/8x18	6x2x26	6 $\frac{1}{4}$	10-3/8	357
	263	252	242	209	184	13x2 $\frac{1}{4}$ x27 $\frac{1}{4}$	19x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	4x7-7/8x19	7x2 $\frac{1}{4}$ x27	10 $\frac{1}{4}$	14-7/8	571	
	289	277	267	232	209	14x2 $\frac{1}{4}$ x27 $\frac{1}{4}$	19x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	4x7-7/8x19	7x2 $\frac{1}{4}$ x27	10 $\frac{1}{4}$	14-7/8	591	
	326	314	303	265	236	15x2-3/4x28 $\frac{1}{4}$	20x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	4x7-7/8x20	7x2 $\frac{1}{4}$ x28	10 $\frac{1}{4}$	15-1/8	666	
	353	341	329	290	259	16x3x28 $\frac{1}{4}$	20x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	4x7-7/8x20	7x2 $\frac{1}{4}$ x28	10 $\frac{1}{4}$	15-3/8	720	
18"													
	133	126	119	78	76	8x1x26 $\frac{1}{4}$	18x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	3x4-5/8x18	6x1-3/4x26	6 $\frac{1}{4}$	9-3/8	231	
				96	76	8x1 $\frac{1}{4}$ x26 $\frac{1}{4}$	18x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	3x4-5/8x18	6x1-3/4x26	6 $\frac{1}{4}$	9-7/8	261	
	157	148	141	117	96	9x1 $\frac{1}{4}$ x26 $\frac{1}{4}$	18x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	3x4-5/8x18	6x1-3/4x26	6 $\frac{1}{4}$	9-5/8	256	
				141	138	116	10x1 $\frac{1}{4}$ x26 $\frac{1}{4}$	18x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	3x4-5/8x18	6x1-3/4x26	6 $\frac{1}{4}$	9-7/8	272
	180	171	163	138	116	10x1-3/4x26 $\frac{1}{4}$	18x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	3x4-3/8x18	6x2x26	6 $\frac{1}{4}$	10-1/8	309	
				182	164	141	11x1-3/4x27 $\frac{1}{4}$	19x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	3x4-3/8x19	6x2x27	6 $\frac{1}{4}$	10-1/8	336
	212	202	193	164	141	11x2x27 $\frac{1}{4}$	19x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	3x4-3/8x19	6x2x27	6 $\frac{1}{4}$	10-3/8	357	
				218	187	163	12x2x27 $\frac{1}{4}$	19x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	3x4-3/8x19	6x2x27	6 $\frac{1}{4}$	10-3/8	373
	273	261	251	217	191	13x2 $\frac{1}{4}$ x28 $\frac{1}{4}$	20x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	4x7-7/8x20	7x2 $\frac{1}{4}$ x28	10 $\frac{1}{4}$	14-7/8	596	
	299	288	277	241	213	14x2 $\frac{1}{4}$ x28 $\frac{1}{4}$	20x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	4x7-7/8x20	7x2 $\frac{1}{4}$ x28	10 $\frac{1}{4}$	14-7/8	616	
	338	325	314	274	244	15x2-3/4x29 $\frac{1}{4}$	21x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	4x7-7/8x21	7x2 $\frac{1}{4}$ x29	10 $\frac{1}{4}$	15-1/8	693	
	366	353	341	300	268	16x3x29 $\frac{1}{4}$	21x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	4x7-7/8x21	7x2 $\frac{1}{4}$ x29	10 $\frac{1}{4}$	15-3/8	749	
19"													
	139	131	124	82	79	8x1x27 $\frac{1}{4}$	19x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	3x4-5/8x19	6x1-3/4x27	6 $\frac{1}{4}$	9-3/8	242	
				100	79	8x1 $\frac{1}{4}$ x27 $\frac{1}{4}$	19x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	3x4-5/8x19	6x1-3/4x27	6 $\frac{1}{4}$	9-7/8	273	
	163	154	146	122	100	9x1 $\frac{1}{4}$ x27 $\frac{1}{4}$	19x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	3x4-5/8x19	6x1-3/4x27	6 $\frac{1}{4}$	9-5/8	267	
				147	143	120	10x1 $\frac{1}{4}$ x27 $\frac{1}{4}$	19x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	3x4-5/8x19	6x1-3/4x27	6 $\frac{1}{4}$	9-7/8	285
	187	178	170	143	120	10x1-3/4x27 $\frac{1}{4}$	19x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	3x4-5/8x19	6x1-3/4x27	6 $\frac{1}{4}$	9-7/8	296	
				180	170	146	11x1-3/4x28 $\frac{1}{4}$	20x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	3x4-3/8x19	6x2x27	6 $\frac{1}{4}$	10-1/8	323
	220	210	201	170	146	11x2x28 $\frac{1}{4}$	20x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	3x4-3/8x20	6x2x28	6 $\frac{1}{4}$	10-1/8	350	
				227	226	193	12x2x28 $\frac{1}{4}$	20x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	3x4-3/8x20	6x2x28	6 $\frac{1}{4}$	10-3/8	388
	282	271	260	225	198	13x2 $\frac{1}{4}$ x29 $\frac{1}{4}$	21x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	4x7-7/8x21	7x2 $\frac{1}{4}$ x29	10 $\frac{1}{4}$	14-7/8	621	
	310	298	287	249	220	14x2 $\frac{1}{4}$ x29 $\frac{1}{4}$	21x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	4x7-7/8x21	7x2 $\frac{1}{4}$ x29	10 $\frac{1}{4}$	14-7/8	641	
	349	336	324	284	252	15x2-3/4x30 $\frac{1}{4}$	22x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	4x7-7/8x22	7x2 $\frac{1}{4}$ x30	10 $\frac{1}{4}$	15-1/8	720	
	378	365	352	310	277	16x3x30 $\frac{1}{4}$	22x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	4x7-7/8x22	7x2 $\frac{1}{4}$ x30	10 $\frac{1}{4}$	15-3/8	778	

*Weight does not include 2 anchor bolts @ 12#

ALLOWABLE MOVEMENT = 2"

TYPE "C" BEARING
(Expansion Cont.)

TYPE "D" BEARINGS
(Expansion Joint.)

ALLOWABLE MOVEMENT = 2"

Bottom Flange Width	Capacity in Kips					Masonry	Top Plate	Web	Rocker	Radius	Height (No Lead Plate)	*Weight
	e=3/4"	e=7/8"	e=1"	e=1 1/4"	e=2" plate							
20"			85	82	8x1x28 $\frac{1}{4}$	20x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	3x4-5/8x20	6x1-3/4x28	6 $\frac{1}{4}$	9-3/8	253	
	144	136	128	103	82 8x1 $\frac{1}{4}$ x28 $\frac{1}{4}$	20x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	3x4-5/8x20	6x1-3/4x28	6 $\frac{1}{4}$	9-7/8	285	
	169	160	152	126	103 9x1 $\frac{1}{4}$ x28 $\frac{1}{4}$	20x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	3x4-5/8x20	6x1-3/4x28	6 $\frac{1}{4}$	9-5/8	279	
			153	148	125 10x1 $\frac{1}{4}$ x28 $\frac{1}{4}$	20x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	3x4-5/8x20	6x1-3/4x28	6 $\frac{1}{4}$	9-7/8	297	
	194	185	176	148	128 10x1-3/4x28 $\frac{1}{4}$	20x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	3x4-3/8x20	6x2x28	6 $\frac{1}{4}$	10-1/8	336	
			197	177	151 11x1-3/4x29 $\frac{1}{4}$	21x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	3x4-3/8x21	6x2x29	6 $\frac{1}{4}$	10-1/8	364	
	228	217	208	177	151 11x2x29 $\frac{1}{4}$	21x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	3x4-3/8x21	6x2x29	6 $\frac{1}{4}$	10-3/8	387	
			233	200	175 12x2x29 $\frac{1}{4}$	21x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	3x4-3/8x21	6x2x29	6 $\frac{1}{4}$	10-3/8	404	
	292	280	269	232	204 13x2 $\frac{1}{4}$ x30 $\frac{1}{4}$	22x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	4x7-7/8x22	7x2 $\frac{1}{4}$ x30	10 $\frac{1}{4}$	14-7/8	645	
	320	308	296	258	228 14x2 $\frac{1}{4}$ x30 $\frac{1}{4}$	22x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	4x7-7/8x22	7x2 $\frac{1}{4}$ x30	10 $\frac{1}{4}$	14-7/8	667	
361	347	335	293	261	15x2-3/4x31 $\frac{1}{4}$	23x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	4x7-7/8x23	7x2 $\frac{1}{4}$ x31	10 $\frac{1}{4}$	15-1/8	747	
	391	377	364	320	286 16x3x31 $\frac{1}{4}$	23x1 $\frac{1}{4}$ x4 $\frac{1}{4}$	4x7-7/8x23	7x2 $\frac{1}{4}$ x31	10 $\frac{1}{4}$	15-3/8	807	

*Weight does not include 2 anchor bolts @ 12#

TYPE "C" BEAMS
(Expansion Cont.)

ALLOWABLE MOVEMENT = 2"

<u>Bottom Flange Width</u>	<u>Capacity in Kips</u> <u>e=1"</u> <u>e=1½"</u> <u>e=2"</u>			<u>Masonry Plate</u>	<u>Top Plate</u>	<u>Web</u>	<u>Rocker</u>	<u>Radius</u>	<u>Height (No Lead Plate)</u>	<u>*Weight</u>
21"	123	107		9x1½x29½	21x1½x4½	3x4-5/8x21	6x1-3/4x29	6½	9-5/8	291
	157	129	107	9x1½x29½	21x1½x4½	3x4-5/8x21	6x1-3/4x29	6½	9-7/8	309
	159	153	129	10x1½x29½	21x1½x4½	3x4-5/8x21	6x1-3/4x29	6½	9-7/8	322
	182	153	129	10x1-3/4x29½	21x1½x4½	3x4-5/8x21	6x1-3/4x29	6½	10-1/8	342
	204	183	157	11x1-3/4x30½	22x1½x4½	3x4-3/8x22	6x2x30	6½	10-1/8	379
	215	183	157	11x2x30½	22x1½x4½	3x4-3/8x22	6x2x30	6½	10-3/8	402
		187	179	12x1-3/4x30½	22x1½x4½	3x4-3/8x22	6x2x30	6½	10-1/8	394
	242	207	179	12x2x30½	22x1½x4½	3x4-3/8x22	6x2x30	6½	10-3/8	419
		234	211	13x2x31½	23x1½x4½	4x7-7/8x23	7x2x31	10	13-7/8	583
	278	240	211	13x2½x31½	23x1½x4½	4x7-7/8x23	7x2x31	10	14-1/8	611
	275	266	236	14x2½x31½	23x1½x4½	4x7-7/8x23	7x2x31	10	14-1/8	631
	306	266	236	14x2½x31½	23x1½x4½	4x7-7/8x23	7x2x31	10	14-3/8	662
	328	302	269	15x2½x32½	24x1½x4½	4x7-7/8x24	7x2x32	10	14-3/8	709
	346	302	269	15x2-3/4x32½	24x1½x4½	4x7-7/8x24	7x2x32	10	14-5/8	744
	372	331	295	16x2-3/4x32½	24x1½x4½	4x7-5/8x24	7x2½x32	10	14-5/8	777
22"	165	159	134	10x1½x30½	22x1½x4½	3x4-5/8x22	6x1-3/4x30	6½	9-7/8	334
	188	159	134	10x1-3/4x30½	22x1½x4½	3x4-5/8x22	6x1-3/4x30	6½	10-1/8	356
	204	183	157	11x1-3/4x30½	22x1½x4½	3x4-3/8x22	6x2x30	6½	10-1/8	379
	215	183	157	11x2x30½	22x1½x4½	3x4-3/8x22	6x2x30	6½	10-3/8	402
		194	185	12x1-3/4x31½	23x1½x4½	3x4-3/8x23	6x2x31	6½	10-1/8	408
	250	214	185	12x2x31½	23x1½x4½	3x4-3/8x23	6x2x31	6½	10-3/8	435
		234	211	13x2x31½	23x1½x4½	4x7-7/8x23	7x2x31	10	13-7/8	583
	278	240	211	13x2½x31½	23x1½x4½	4x7-7/8x23	7x2x31	10	14-1/8	611
	284	275	243	14x2½x32½	24x1½x4½	4x7-7/8x24	7x2x32	10	14-1/8	655
	316	275	243	14x2½x32½	24x1½x4½	4x7-7/8x24	7x2x32	10	14-3/8	686
	328	302	269	15x2½x32½	24x1½x4½	4x7-7/8x24	7x2x32	10	14-3/8	709
	346	302	269	15x2-3/4x32½	24x1½x4½	4x7-7/8x24	7x2x32	10	14-5/8	744
		318	304	16x2½x33½	25x1½x4½	4x7-5/8x25	7x2½x33	10	14-3/8	767
	384	341	304	16x2-3/4x33½	25x1½x4½	4x7-5/8x25	7x2½x33	10	14-5/8	804
		362	332	17x2-3/4x33½	25x1½x4½	4x7-5/8x25	7x2½x33	10	14-5/8	830
	414	370	332	17x3x33½	25x1½x4½	4x7-5/8x25	7x2½x33	10	14-7/8	870

*Weight does not include 2 anchor bolts @ 12#

<u>Bottom Flange Width</u>	<u>Capacity in Kips e=1" e=1½" e=2"</u>	<u>Masonry Plate</u>	<u>Top Plate</u>	<u>Web</u>	<u>Rocker</u>	<u>Radius</u>	<u>Height (No Lead Plate)</u>	<u>*Weight</u>
23"	171 164 138	10x1½x31½	23x1½x4½	3x4-5/8x23	6x1-3/4x31	6½	9-7/8	347
	195 164 138	10x1-3/4x31½	23x1½x4½	3x4-5/8x23	6x1-3/4x31	6½	10-1/8	369
	212 189 162	11x1-3/4x31½	23x1½x4½	3x4-3/8x23	6x2x31	6½	10-1/8	393
	222 189 162	11x2x31½	23x1½x4½	3x4-3/8x23	6x2x31	6½	10-3/8	417
	201 191	12x1-3/4x32½	24x1½x4½	3x4-3/8x24	6x2x32	6½	10-1/8	423
	258 221 191	12x2x32½	24x1½x4½	3x4-3/8x24	6x2x32	6½	10-3/8	450
	242 218	13x2x32½	24x1½x4½	4x7-7/8x24	7x2x32	10	13-7/8	604
	287 248 218	13x2½x32½	24x1½x4½	4x7-7/8x24	7x2x32	10	14-1/8	634
	294 283 251	14x2½x33½	25x1½x4½	4x7-7/8x25	7x2x33	10	14-1/8	678
	326 283 251	14x2½x33½	25x1½x4½	4x7-7/8x25	7x2x33	10	14-3/8	711
	339 312 277	15x2½x33½	25x1½x4½	4x7-7/8x25	7x2x33	10	14-3/8	734
	356 312 277	15x2-3/4x33½	25x1½x4½	4x7-7/8x26	7x2x33	10	14-5/8	770
	328 313	16x2½x34½	26x1½x4½	4x7-5/8x26	7x2½x34	10	14-3/8	792
	397 351 313	16x2-3/4x34½	26x1½x4½	4x7-5/8x26	7x2½x34	10	14-5/8	831
	374 342	17x2-3/4x34½	26x1½x4½	4x7-5/8x26	7x2½x34	10	14-5/8	858
	428 381 342	17x3x34½	26x1½x4½	4x7-5/8x26	7x2½x34	10	14-7/8	899
24"	219 195 167	11x1-3/4x32½	24x1½x4½	3x4-3/8x24	6x2x32	6½	10-1/8	407
	229 195 167	11x2x32½	24x1½x4½	3x4-3/8x24	6x2x32	6½	10-3/8	432
	201 191	12x1-3/4x32½	24x1½x4½	3x4-3/8x24	6x2x32	6½	10-1/8	423
	258 221 191	12x2x32½	24x1½x4½	3x4-3/8x24	6x2x32	6½	10-3/8	450
	250 225	13x2x33½	25x1½x4½	4x7-7/8x25	7x3x33	11	14-7/8	689
	296 255 225	13x2½x33½	25x1½x4½	4x7-7/8x25	7x3x33	11	15-1/8	720
	294 283 251	14x2½x33½	25x1½x4½	4x7-7/8x25	7x3x33	11	15-1/8	741
	326 283 251	14x2½x33½	25x1½x4½	4x7-7/8x25	7x3x33	11	15-3/8	774
	350 321 286	15x2½x34½	26x1½x4½	4x7-7/8x26	7x3x34	11	15-3/8	825
	367 321 286	15x2-3/4x34½	26x1½x4½	4x7-7/8x26	7x3x34	11	15-5/8	861
	328 313	16x2½x34½	26x1½x4½	4x7-7/8x26	7x3x34	11	15-3/8	849
	397 351 313	16x2-3/4x34½	26x1½x4½	4x7-7/8x26	7x3x34	11	15-5/8	888
	385 352	17x2-3/4x35½	27x1½x4½	4x7-7/8x27	7x3x35	11	15-5/8	944
	443 392 352	17x3x35½	27x1½x4½	4x7-7/8x27	7x3x35	11	15-7/8	987
	443 424 381	18x3x35½	27x1½x4½	4x7-7/8x27	7x3x35	11	15-7/8	1017
	477 424 381	18x3½x35½	27x1½x4½	4x7-7/8x27	7x3x35	11	16-1/8	1062

*Weight does not include 2 anchor bolts @ 12#

1.4.10 SEC. 3.31
 REVISION CONC.
 DESIGN NUMBER = 2

TYPE "D" BEARINGS
 (Expansion Cont.)

ALLOWABLE MOVEMENT = 2"

<u>Bottom Flange Width</u>	<u>Capacity in Kips</u>			<u>Masonry Plate</u>	<u>Top Plate</u>	<u>Web</u>	<u>Rocker</u>	<u>Radius</u>	<u>Height (No Lead Plate)</u>	<u>*Weight</u>
25"	226	201	172	11x1-3/4x33 $\frac{1}{2}$	25x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	3x4-3/8x25	6x2x33	6 $\frac{1}{4}$	10-1/8	421
	236	201	172	11x2x33 $\frac{1}{2}$	25x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	3x4-3/8x25	6x2x33	6 $\frac{1}{4}$	10-3/8	447
		208	197	12x1-3/4x33 $\frac{1}{2}$	25x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	3x4-3/8x25	6x2x33	6 $\frac{1}{4}$	10-1/8	438
	266	228	197	12x2x33 $\frac{1}{2}$	25x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	3x4-3/8x25	6x2x33	6 $\frac{1}{4}$	10-3/8	466
		258	231	13x2x34 $\frac{1}{2}$	26x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	4x7-7/8x26	7x3x34	11	14-7/8	713
	304	263	231	13x2 $\frac{1}{2}$ x34 $\frac{1}{2}$	26x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	4x7-7/8x26	7x3x34	11	15-1/8	744
	304	292	258	14x2 $\frac{1}{2}$ x34 $\frac{1}{2}$	26x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	4x7-7/8x26	7x3x34	11	15-3/8	800
	336	292	258	14x2 $\frac{1}{2}$ x34 $\frac{1}{2}$	26x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	4x7-7/8x26	7x3x35	11	15-3/8	852
	361	331	294	15x2 $\frac{1}{2}$ x35 $\frac{1}{2}$	27x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	4x7-7/8x27	7x3x35	11	15-5/8	889
	378	331	294	15x2-3/4x35 $\frac{1}{2}$	27x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	4x7-7/8x27	7x3x35	11	15-3/8	877
		338	323	16x2 $\frac{1}{2}$ x35 $\frac{1}{2}$	27x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	4x7-7/8x27	7x3x35	11	15-5/8	917
	410	361	323	16x2-3/4x35 $\frac{1}{2}$	27x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	4x7-7/8x27	7x3x36	11	15-5/8	974
		397	362	17x2-3/4x36 $\frac{1}{2}$	28x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	4x7-7/8x28	7x3x36	11	15-7/8	1018
	456	403	362	17x3x36 $\frac{1}{2}$	28x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	4x7-7/8x28	7x3x36	11	15-7/8	1049
	447	436	392	18x3x36 $\frac{1}{2}$	28x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	4x7-7/8x28	7x3x36	11	16-1/8	1095
	490	436	392	18x3 $\frac{1}{2}$ x36 $\frac{1}{2}$	28x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	4x7-7/8x28				
26"		214	203	12x1-3/4x34 $\frac{1}{2}$	26x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	4x6-3/8x26	6x2x34	8 $\frac{1}{4}$	12-1/8	539
	274	235	203	12x2x34 $\frac{1}{2}$	26x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	4x6-3/8x26	6x2x34	8 $\frac{1}{4}$	12-3/8	568
		258	231	13x2x34 $\frac{1}{2}$	26x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	4x6-3/8x26	6x2x34	8 $\frac{1}{4}$	12-3/8	588
	304	263	231	13x2 $\frac{1}{2}$ x34 $\frac{1}{2}$	26x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	4x6-3/8x26	6x2x34	8 $\frac{1}{4}$	12-5/8	619
	313	300	266	14x2 $\frac{1}{2}$ x35 $\frac{1}{2}$	27x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	4x6-3/8x27	7x2x35	8 $\frac{1}{4}$	12-5/8	676
	345	300	266	14x2 $\frac{1}{2}$ x35 $\frac{1}{2}$	27x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	4x6-3/8x27	7x2x35	8 $\frac{1}{4}$	12-7/8	710
	361	331	294	15x2 $\frac{1}{2}$ x35 $\frac{1}{2}$	27x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	4x6-3/8x27	7x2x35	8 $\frac{1}{4}$	12-7/8	736
	375	331	294	15x2-3/4x35 $\frac{1}{2}$	27x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	4x6-3/8x27	7x2x35	8 $\frac{1}{4}$	13-1/8	773
		349	332	16x2 $\frac{1}{2}$ x36 $\frac{1}{2}$	28x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	4x7-7/8x28	7x3 $\frac{1}{2}$ x36	11 $\frac{1}{4}$	15-7/8	939
	422	372	332	16x2-3/4x36 $\frac{1}{2}$	28x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	4x7-7/8x28	7x3 $\frac{1}{2}$ x36	11 $\frac{1}{4}$	16-1/8	980
		397	362	17x2-3/4x36 $\frac{1}{2}$	28x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	4x7-7/8x28	7x3 $\frac{1}{2}$ x36	11 $\frac{1}{4}$	16-1/8	1009
	456	403	362	17x3x36 $\frac{1}{2}$	28x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	4x7-7/8x28	7x3 $\frac{1}{2}$ x36	11 $\frac{1}{4}$	16-3/8	1052
	460	448	403	18x3x37 $\frac{1}{2}$	29x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	4x7-7/8x29	7x3 $\frac{1}{2}$ x37	11 $\frac{1}{4}$	16-3/8	1116
	504	448	403	18x3 $\frac{1}{2}$ x37 $\frac{1}{2}$	29x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	4x7-7/8x29	7x3 $\frac{1}{2}$ x37	11 $\frac{1}{4}$	16-5/8	1163
	511	481	435	19x3 $\frac{1}{2}$ x37 $\frac{1}{2}$	29x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	4x7-7/8x29	7x3 $\frac{1}{2}$ x37	11 $\frac{1}{4}$	16-5/8	1198
	539	481	435	19x3 $\frac{1}{2}$ x37 $\frac{1}{2}$	29x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	4x7-7/8x29	7x3 $\frac{1}{2}$ x37	11 $\frac{1}{4}$	16-7/8	1248

*Weight does not include 2 anchor bolts @ 12#

<u>Bottom Flange Width</u>	<u>Capacity in Kips e=1" e=1½" e=2"</u>		<u>Masonry Plate</u>	<u>Top Plate</u>	<u>Web</u>	<u>Rocker</u>	<u>Radius</u>	<u>Height (No Lead Plate)</u>	<u>*Weight</u>	
27"	267	238	13x2x35½	27x1½x4½	4x6-3/8x27	6x2x35	8½	12-3/8	607	
	313	271	13x2½x35½	27x1½x4½	4x6-3/8x27	6x2x35	8½	12-5/8	640	
	313	300	14x2½x35½	27x1½x4½	4x6-3/8x27	6x2x35	8½	12-5/8	662	
	345	300	14x2½x35½	27x1½x4½	4x6-3/8x27	6x2x35	8½	12-7/8	697	
	372	340	15x2½x36½	28x1½x4½	4x6-1/8x28	7x2½x36	8½	12-7/8	768	
	387	340	15x2-3/4x36½	28x1½x4½	4x6-1/8x28	7x2½x36	8½	13-1/8	806	
	349	332	16x2½x36½	28x1½x4½	4x7-7/8x28	7x4½x36	12½	16-7/8	1008	
422	372	332	16x2-3/4x36½	28x1½x4½	4x7-7/8x28	7x4½x36	12½	17-1/8	1049	
	409	372	17x2-3/4x37½	29x1½x4½	4x7-7/8x29	7x4½x37	12½	17-1/8	1110	
	469	415	17x3x37½	29x1½x4½	4x7-7/8x29	7x4½x37	12½	17-3/8	1155	
	460	448	403	18x3x37½	29x1½x4½	4x7-7/8x29	7x4½x37	12½	17-3/8	1187
	504	448	403	18x3½x37½	29x1½x4½	4x7-7/8x29	7x4½x37	12½	17-5/8	1235
	526	494	446	19x3½x38½	30x1½x4½	4x7-7/8x30	7x4½x38	12½	17-5/8	1306
	553	494	446	19x3½x38½	30x1½x4½	4x7-7/8x30	7x4½x38	12½	17-7/8	1357
	580	529	479	20x3½x38½	30x1½x4½	4x7-7/8x30	7x4½x38	12½	17-7/8	1396
	590	529	479	20x3-3/4x38½	30x1½x4½	4x7-7/8x30	7x4½x38	12½	18-1/8	1450

*weight does not include 2 anchor bolts @ 12#

TYPE "D" BEARINGS
(Expansion Cont.)

ALLOWABLE MOVEMENT = $2\frac{1}{2}$ " and 3"

Bottom Flange Width	Capacity in Kips $e=2 \frac{1}{2}"$	Masonry Plate	Top Plate	Web	Rocker	Radius	Height (No Lead Plate)	*Weight
8"	34	8x1x16-1/2	8x1-1/4x4-1/2	4x4-1/8x8	7x2-1/4x16	6 $\frac{1}{2}$	9-3/8	144
	49	9x1-1/4x17-1/2	9x1-1/4x4-1/2	4x4-1/8x9	7x2-1/4x17	6 $\frac{1}{2}$	9-5/8	172
	65	10x1-1/4x18-1/2	10x1-1/4x4-1/2	4x4-1/8x10	7x2-1/4x18	6 $\frac{1}{2}$	9-5/8	192
	84	11x1-1/2x19-1/2	11x1-1/4x4-1/2	4x4-1/8x11	7x2-1/4x19	6 $\frac{1}{2}$	9-7/8	228
	99	12x1-3/4x19-1/2	11x1-1/4x4-1/2	4x4-1/8x11	7x2-1/4x19	6 $\frac{1}{2}$	10-1/8	252
9"	36	8x1x17-1/2	9x1-1/4x4-1/2	4x4-1/8x9	7x2-1/4x17	6 $\frac{1}{2}$	9-3/8	156
	52	9x1-1/4x18-1/2	10x1-1/4x4-1/2	4x4-1/8x10	7x2-1/4x18	6 $\frac{1}{2}$	9-5/8	186
	70	10x1-1/4x19-1/2	11x1-1/4x4-1/2	4x4-1/8x11	7x2-1/4x19	6 $\frac{1}{2}$	9-5/8	206
	84	11x1-1/2x19-1/2	11x1-1/4x4-1/2	4x4-1/8x11	7x2-1/4x19	6 $\frac{1}{2}$	9-7/8	228
	104	12x1-3/4x20-1/2	12x1-1/4x4-1/2	4x4-1/8x12	7x2-1/4x20	6 $\frac{1}{2}$	10-1/8	269
	119	13x2x20-1/2	12x1-1/4x4-1/2	4x4-1/8x12	7x2-1/4x20	6 $\frac{1}{2}$	10-3/8	297
10"	38	8x1x18-1/2	10x1-1/4x4-1/2	4x4-1/8x10	7x2-1/4x18	6 $\frac{1}{2}$	9-3/8	169
	55	9x1-1/4x19-1/2	11x1-1/4x4-1/2	4x4-1/8x11	7x2-1/4x19	6 $\frac{1}{2}$	9-5/8	199
	73	10x1-1/4x20-1/2	12x1-1/4x4-1/2	4x4-1/8x12	7x2-1/4x20	6 $\frac{1}{2}$	9-5/8	220
	89	11x1-1/2x20-1/2	12x1-1/4x4-1/2	4x4-1/8x12	7x2-1/4x20	6 $\frac{1}{2}$	9-7/8	243
	109	12x1-3/4x21-1/2	13x1-1/4x4-1/2	4x4-1/8x13	7x2-1/4x21	6 $\frac{1}{2}$	10-1/8	285
	126	13x2x21-1/2	13x1-1/4x4-1/2	4x4-1/8x13	7x2-1/4x21	6 $\frac{1}{2}$	10-3/8	315
	40	8x1x19-1/2	11x1-1/4x4-1/2	4x4-1/8x11	7x2-1/4x19	6 $\frac{1}{2}$	9-3/8	182
11"	58	9x1-1/4x20-1/2	12x1-1/4x4-1/2	4x4-1/8x12	7x2-1/4x20	6 $\frac{1}{2}$	9-5/8	213
	73	10x1-1/4x20-1/2	12x1-1/4x4-1/2	4x4-1/8x12	7x2-1/4x20	6 $\frac{1}{2}$	9-5/8	220
	93	11x1-1/2x21-1/2	13x1-1/4x4-1/2	4x4-1/8x13	7x2-1/4x21	6 $\frac{1}{2}$	9-7/8	258
	109	12x1-3/4x21-1/2	13x1-1/4x4-1/2	4x4-1/8x13	7x2-1/4x21	6 $\frac{1}{2}$	10-1/8	285
	131	13x2x22-1/2	14x1-1/4x4-1/2	4x4-1/8x14	7x2-1/4x22	6 $\frac{1}{2}$	10-3/8	333
	148	14x2x22-1/2	14x1-1/4x4-1/2	4x4-1/8x14	7x2-1/4x22	6 $\frac{1}{2}$	10-3/8	345
	43	8x1x20-1/2	12x1-1/4x4-1/2	4x4-1/8x12	7x2-1/4x20	6 $\frac{1}{2}$	9-3/8	193
12"	58	9x1-1/4x20-1/2	12x1-1/4x4-1/2	4x4-1/8x12	7x2-1/4x20	6 $\frac{1}{2}$	9-5/8	213
	77	10x1-1/4x21-1/2	13x1-1/4x4-1/2	4x4-1/8x13	7x2-1/4x21	6 $\frac{1}{2}$	9-5/8	234
	93	11x1-1/2x21-1/2	13x1-1/4x4-1/2	4x4-1/8x13	7x2-1/4x21	6 $\frac{1}{2}$	9-7/8	258
	115	12x1-3/4x22-1/2	14x1-1/4x4-1/2	4x4-1/8x14	7x2-1/4x22	6 $\frac{1}{2}$	10-1/8	301
	131	13x2x22-1/2	14x1-1/4x4-1/2	4x4-1/8x14	7x2-1/4x22	6 $\frac{1}{2}$	10-3/8	333
	155	14x2x23-1/2	15x1-1/4x4-1/2	4x4-1/8x15	7x2-1/4x23	6 $\frac{1}{2}$	10-3/8	364
	175	15x2-1/4x23-1/2	15x1-1/4x4-1/2	4x4-1/8x15	7x2-1/4x23	6 $\frac{1}{2}$	10-5/8	402

*Weight does not include 2 anchor bolts @ 12#

<u>Bottom Flange Width</u>	<u>Capacity in Kips e=2 1/2" e=3"</u>	<u>Masonry Plate</u>	<u>Top Plate</u>	<u>Web</u>	<u>Rocker</u>	<u>Radius</u>	<u>Height (No Lead Plate)</u>	<u>*Weight</u>
13"	45	29	8x1x21-1/2	13x1-1/4x4-1/2	4x4-1/8x13	7x2-1/4x21	6 $\frac{1}{2}$	9-3/8 207
	61	45	9x1-1/4x21-1/2	13x1-1/4x4-1/2	4x4-1/8x13	7x2-1/4x21	6 $\frac{1}{2}$	9-5/8 226
	81	64	10x1-1/4x22-1/2	14x1-1/4x4-1/2	4x4-1/8x14	7x2-1/4x22	6 $\frac{1}{2}$	9-5/8 248
	98	81	11x1-1/2x22-1/2	14x1-1/4x4-1/2	4x4-1/8x14	7x2-1/4x22	6 $\frac{1}{2}$	9-7/8 273
	120	102	12x1-3/4x23-1/2	15x1-1/4x4-1/2	4x4-1/8x15	7x2-1/4x23	6 $\frac{1}{2}$	10-1/8 317
	138	120	13x2x23-1/2	15x1-1/4x4-1/2	4x4-1/8x15	7x2-1/4x23	6 $\frac{1}{2}$	10-3/8 350
	162	144	14x2x24-1/2	16x1-1/4x4-1/2	4x4-1/8x16	7x2-1/4x24	6 $\frac{1}{2}$	10-3/8 382
	182	162	15x2-1/4x24-1/2	16x1-1/4x4-1/2	4x4-1/8x16	7x2-1/4x24	6 $\frac{1}{2}$	10-5/8 422
14"	64	47	9x1-1/4x22-1/2	14x1-1/4x4-1/2	4x4-1/8x14	7x2-1/4x22	6 $\frac{1}{2}$	9-5/8 240
	81	64	10x1-1/4x22-1/2	14x1-1/4x4-1/2	4x4-1/8x14	7x2-1/4x22	6 $\frac{1}{2}$	9-5/8 248
	102	85	11x1-1/2x23-1/2	15x1-1/4x4-1/2	4x4-1/8x15	7x2-1/4x23	6 $\frac{1}{2}$	9-7/8 288
	120	102	12x1-3/4x23-1/2	15x1-1/4x4-1/2	4x4-1/8x15	7x2-1/4x23	6 $\frac{1}{2}$	10-1/8 317
	144	125	13x2x24-1/2	16x1-1/4x4-1/2	4x4-1/8x16	7x2-1/4x24	6 $\frac{1}{2}$	10-3/8 368
	162	143	14x2x24-1/2	16x1-1/4x4-1/2	4x4-1/8x16	7x2-1/4x24	6 $\frac{1}{2}$	10-3/8 382
	190	169	15x2-1/4x25-1/2	17x1-1/4x4-1/2	4x4-1/8x17	7x2-1/4x25	6 $\frac{1}{2}$	10-5/8 441
	209	188	16x2-1/2x25-1/2	17x1-1/4x4-1/2	4x4-7/8x17	7x2-1/2x25	7 $\frac{1}{2}$	11-7/8 515
	67	49	9x1-1/4x23-1/2	15x1-1/4x4-1/2	4x4-1/8x15	7x2-1/4x23	6 $\frac{1}{2}$	9-5/8 253
15"	85	67	10x1-1/4x23-1/2	15x1-1/4x4-1/2	4x4-1/8x15	7x2-1/4x23	6 $\frac{1}{2}$	9-5/8 262
	107	88	11x1-1/2x24-1/2	16x1-1/4x4-1/2	4x4-1/8x16	7x2-1/4x24	6 $\frac{1}{2}$	9-7/8 284
	125	107	12x1-3/4x24-1/2	16x1-1/4x4-1/2	4x4-1/8x16	7x2-1/4x24	6 $\frac{1}{2}$	10-1/8 334
	149	130	13x2x25-1/2	17x1-1/4x4-1/2	4x4-1/8x17	7x2-1/4x25	6 $\frac{1}{2}$	10-3/8 386
	169	150	14x2x25-1/2	17x1-1/4x4-1/2	4x4-1/8x17	7x2-1/4x25	6 $\frac{1}{2}$	10-3/8 400
	197	175	15x2-1/4x26-1/2	18x1-1/4x4-1/2	4x4-1/8x18	7x2-1/4x26	6 $\frac{1}{2}$	10-5/8 461
	217	195	16x2-1/2x26-1/2	18x1-1/4x4-1/2	4x4-7/8x18	7x2-1/2x26	7 $\frac{1}{2}$	11-7/8 538
	88	70	10x1-1/4x24-1/2	16x1-1/4x4-1/2	4x4-1/8x16	7x2-1/4x24	6 $\frac{1}{2}$	9-5/8 275
16"	107	88	11x1-1/2x24-1/2	16x1-1/4x4-1/2	4x4-1/8x16	7x2-1/4x24	6 $\frac{1}{2}$	9-7/8 303
	130	111	12x1-3/4x25-1/2	17x1-1/4x4-1/2	4x4-1/8x17	7x2-1/4x25	6 $\frac{1}{2}$	10-1/8 350
	149	130	13x2x25-1/2	17x1-1/4x4-1/2	4x4-1/8x17	7x2-1/4x25	6 $\frac{1}{2}$	10-3/8 386
	175	156	14x2x26-1/2	18x1-1/4x4-1/2	4x4-1/8x18	7x2-1/4x26	6 $\frac{1}{2}$	10-3/8 418
	195	175	15x2-1/4x26-1/2	18x1-1/4x4-1/2	4x4-1/8x18	7x2-1/4x26	6 $\frac{1}{2}$	10-5/8 461
	225	203	16x2-1/2x27-1/2	19x1-1/4x4-1/2	4x4-7/8x19	7x2-1/2x27	7 $\frac{1}{2}$	11-7/8 561
	246	223	17x2-3/4x27-1/2	19x1-1/4x4-1/2	4x4-7/8x19	7x2-1/2x27	7 $\frac{1}{2}$	12-1/8 613

*Weight does not include 2 anchor bolts @ 12#

TYPE "C" BEARINGS
(Expansion Cont.)

MICROBE MOVEMENT = 2 1/4 INCHES

<u>Bottom Flange Width</u>	<u>Capacity in Kips</u>	<u>Masonry Plate</u>	<u>Top Plate</u>	<u>Web</u>	<u>Rocker</u>	<u>Radius</u>	<u>Height (No Lead Plate)</u>	<u>*Weight</u>
17"	92	73	10x1-1/4x25-1/2	17x1-1/4x4-1/2	4x4-1/8x17	7x2-1/4x25	6 1/2	9-5/8 289
	111	92	11x1-1/2x25-1/2	17x1-1/4x4-1/2	4x4-1/8x17	7x2-1/4x25	6 1/2	9-7/8 318
	136	116	12x1-3/4x26-1/2	18x1-1/4x4-1/2	4x4-1/8x18	7x2-1/4x26	6 1/2	10-1/8 366
	156	136	13x2x26-1/2	18x1-1/4x4-1/2	4x4-1/8x18	7x2-1/4x26	6 1/2	10-3/8 403
	182	162	14x2x27-1/2	19x1-1/4x4-1/2	4x4-1/8x19	7x2-1/4x27	6 1/2	10-3/8 437
	205	182	15x2-1/4x27-1/2	19x1-1/4x4-1/2	4x4-1/8x19	7x2-1/4x27	6 1/2	10-5/8 481
	234	210	16x2-1/2x28-1/2	20x1-1/4x4-1/2	4x4-7/8x20	7x2-1/2x28	7 1/2	11-7/8 584
	256	232	17x2-3/4x28-1/2	20x1-1/4x4-1/2	4x4-7/8x20	7x2-1/2x28	7 1/2	12-1/8 638
18"	96	76	10x1-1/4x26-1/2	18x1-1/4x4-1/2	4x4-1/8x18	7x2-1/4x26	6 1/2	9-5/8 299
	116	96	11x1-1/2x26-1/2	18x1-1/4x4-1/2	4x4-1/8x18	7x2-1/4x26	6 1/2	9-7/8 329
	141	120	12x1-3/4x27-1/2	19x1-1/4x4-1/2	4x4-1/8x19	7x2-1/4x27	6 1/2	10-1/8 379
	162	141	13x2x27-1/2	19x1-1/4x4-1/2	4x4-1/8x19	7x2-1/4x27	6 1/2	10-3/8 417
	189	168	14x2x28-1/2	20x1-1/4x4-1/2	4x4-1/8x20	7x2-1/4x28	6 1/2	10-3/8 451
	212	189	15x2-1/4x28-1/2	20x1-1/4x4-1/2	4x4-1/8x20	7x2-1/4x28	6 1/2	10-5/8 497
	242	218	16x2-1/2x29-1/2	21x1-1/4x4-1/2	4x4-7/8x21	7x2-1/2x29	7 1/2	11-7/8 603
	265	240	17x2-3/4x29-1/2	21x1-1/4x4-1/2	4x4-7/8x21	7x2-1/2x29	7 1/2	12-1/8 659
19"	100	79	10x1-1/4x27-1/2	19x1-1/4x4-1/2	4x4-1/8x19	7x2-1/4x27	6 1/2	9-5/8 317
	120	100	11x1-1/2x27-1/2	19x1-1/4x4-1/2	4x4-1/8x19	7x2-1/4x27	6 1/2	9-7/8 348
	146	125	12x1-3/4x28-1/2	20x1-1/4x4-1/2	4x4-1/8x20	7x2-1/4x28	6 1/2	10-1/8 399
	168	146	13x2x28-1/2	20x1-1/4x4-1/2	4x4-1/8x20	7x2-1/4x28	6 1/2	10-3/8 439
	196	174	14x2x29-1/2	21x1-1/4x4-1/2	4x4-1/8x21	7x2-1/4x29	6 1/2	10-3/8 473
	218	196	15x2-1/4x29-1/2	21x1-1/4x4-1/2	4x4-1/8x21	7x2-1/4x29	6 1/2	10-5/8 521
	250	225	16x2-1/2x30-1/2	22x1-1/4x4-1/2	4x4-7/8x22	7x2-1/2x30	7 1/2	11-7/8 630
	274	248	17x2-3/4x30-1/2	22x1-1/4x4-1/2	4x4-7/8x22	7x2-1/2x30	7 1/2	12-1/8 688
20"	103	82	10x1-1/4x28-1/2	20x1-1/4x4-1/2	4x4-1/8x20	7x2-1/4x28	6 1/2	9-5/8 331
	125	103	11x1-1/2x28-1/2	20x1-1/4x4-1/2	4x4-1/8x20	7x2-1/4x28	6 1/2	9-7/8 341
	151	129	12x1-3/4x29-1/2	21x1-1/4x4-1/2	4x4-1/8x21	7x2-1/4x29	6 1/2	10-1/8 415
	174	151	13x2x29-1/2	21x1-1/4x4-1/2	4x4-1/8x21	7x2-1/4x29	6 1/2	10-3/8 457
	202	180	14x2x30-1/2	22x1-1/4x4-1/2	4x4-1/8x22	7x2-1/4x30	6 1/2	10-3/8 491
	227	202	15x2-1/4x30-1/2	22x1-1/4x4-1/2	4x4-1/8x22	7x2-1/4x30	6 1/2	10-5/8 541
	258	233	16x2-1/2x31-1/2	23x1-1/4x4-1/2	4x4-7/8x23	7x2-1/2x31	7 1/2	11-7/8 653
	283	256	17x2-3/4x31-1/2	23x1-1/4x4-1/2	4x4-7/8x23	7x2-1/2x31	7 1/2	12-1/8 713

*Weight does not include 2 anchor bolts @ 12#

<u>Bottom Flange Width</u>	<u>Capacity in Kips e=2½" e=3"</u>	<u>Masonry Plate</u>	<u>Top Plate</u>	<u>Web</u>	<u>Rocker</u>	<u>Radius</u>	<u>Height (No Lead Plate)</u>	<u>*Weight</u>
21"	129	107	11x1-1/2x29½	21x1½x4½	4x4-1/8x21	7x2-1/4x29	6½	9-7/8 378
	151	129	12x1-3/4x29½	21x1½x4½	4x4-1/8x21	7x2-1/4x29	6½	10-1/8 415
	179	157	13x2x30½	22x1½x4½	4x4-1/8x22	7x2-1/4x30	6½	10-3/8 474
	202	180	14x2x30½	22x1½x4½	4x4-1/8x22	7x2-1/4x30	6½	10-3/8 491
	233	209	15x2-1/4x31½	23x1½x4½	4x4-1/8x23	7x2-1/4x31	6½	10-5/8 561
	258	233	16x2-1/2x31½	23x1½x4½	4x5-1/8x23	7x2-3/4x31	8	12-3/8 675
	292	265	17x2-3/4x32½	24x1½x4½	4x5-1/8x24	7x2-3/4x32	8	12-5/8 761
	317	289	18x2-3/4x32½	24x1½x4½	4x5-1/8x24	7x2-3/4x32	8	12-5/8 786
22"	134	111	11x1-1/2x30½	22x1½x4½	4x4-1/8x22	7x2-1/4x30	6½	9-7/8 393
	157	134	12x1-3/4x30½	22x1½x4½	4x4-1/8x22	7x2-1/4x30	6½	10-1/8 431
	185	162	13x2x31½	23x1½x4½	4x4-1/8x23	7x2-1/4x31	6½	10-3/8 492
	209	185	14x2x31½	23x1½x4½	4x4-1/8x23	7x2-1/4x31	6½	10-3/8 510
	240	216	15x2-1/4x32½	24x1½x4½	4x4-1/8x24	7x2-1/4x32	6½	10-5/8 581
	267	240	16x2-1/2x32½	24x1½x4½	4x5-1/8x24	7x2-3/4x32	8	12-3/8 699
	301	273	17x2-1/2x33½	25x1½x4½	4x5-1/8x25	7x2-3/4x33	8	12-3/8 747
	327	298	18x2-3/4x33½	25x1½x4½	4x5-1/8x25	7x2-3/4x33	8	12-5/8 813
23"	162	138	12x1-3/4x31½	23x1½x4½	4x4-1/8x23	7x2-1/4x31	6½	10-1/8 448
	185	162	13x2x31½	23x1½x4½	4x4-1/8x23	7x2-1/4x31	6½	10-3/8 492
	216	191	14x2x32½	24x1½x4½	4x4-1/8x24	7x2-1/4x32	6½	10-3/8 528
	240	216	15x2-1/4x32½	24x1½x4½	4x4-1/8x24	7x2-1/4x32	6½	10-5/8 581
	269	248	16x2-1/2x33½	25x1½x4½	4x4-1/8x25	7x2-1/4x33	6½	10-7/8 659
	301	273	17x2-1/2x33½	25x1½x4½	4x5-3/8x25	7x3x33	8½	12-7/8 771
	337	307	18x2-3/4x34½	26x1½x4½	4x5-3/8x26	7x3x34	8½	13-1/8 864
	364	335	19x3x34½	26x1½x4½	4x5-3/8x26	7x3x34	8½	13-3/8 937
24"	167	143	12x1-3/4x32½	24x1½x4½	4x4-1/8x24	7x2-1/4x32	6½	10-1/8 464
	191	167	13x2x32½	24x1½x4½	4x4-1/8x24	7x2-1/4x32	6½	10-3/8 510
	223	197	14x2x33½	25x1½x4½	4x4-1/8x25	7x2-1/4x33	6½	10-3/8 546
	248	223	15x2-1/4x33½	25x1½x4½	4x4-1/8x25	7x2-1/4x33	6½	10-5/8 600
	278	255	16x2-1/2x34½	26x1½x4½	4x4-1/8x26	7x2-1/4x34	6½	10-7/8 681
	309	281	17x2-1/2x34½	26x1½x4½	4x5-3/8x26	7x3x34	8½	12-7/8 796
	347	316	18x2-3/4x35½	27x1½x4½	4x5-3/8x27	7x3x35	8½	13-1/8 892
	375	345	19x3x35½	27x1½x4½	4x5-3/8x27	7x3x35	8½	13-3/8 967

*Weight does not include 2 anchor bolts @ 12#

TYPE "D" BEARINGS
(Expansion Cont.)

ALLOWABLE MOVEMENT = 2½" and 3"

<u>Bottom Flange Width</u>	<u>Capacity in Kips e=2½" e=3"</u>	<u>Masonry Plate</u>	<u>Top Plate</u>	<u>Web</u>	<u>Rocker</u>	<u>Radius</u>	<u>Height (No Lead Plate)</u>	<u>*Weight</u>
25"	197	13x2x33½	25x1½x4½	4x4-1/8x25	7x2-1/4x33	6½	10-3/8	527
	223	14x2x33½	25x1½x4½	4x4-1/8x25	7x2-1/4x33	6½	10-3/8	546
	229	15x2-1/4x34½	26x1½x4½	4x4-1/8x26	7x2-1/4x34	6½	10-5/8	620
	255	16x2-1/2x34½	26x1½x4½	4x4-1/8x26	7x2-1/4x34	6½	10-7/8	681
	278	255	17x2-1/2x35½	27x1½x4½	4x5-7/8x27	7x3x35	9	13-3/8
	319	289	18x2-3/4x35½	27x1½x4½	4x5-7/8x27	7x3x35	9	13-5/8
	347	316	19x3x36½	28x1½x4½	4x5-7/8x28	7x3x36	9	13-7/8
	386	354	20x3-1/4x36½	28x1½x4½	4x5-7/8x28	7x3x36	9	14-1/8
26"	197	13x2x34½	26x1½x4½	4x4-1/8x26	7x2-1/4x34	6½	10-3/8	545
	223	14x2x34½	26x1½x4½	4x4-1/8x26	7x2-1/4x34	6½	10-3/8	564
	229	15x2-1/4x35½	27x1½x4½	4x4-1/8x27	7x2-1/4x35	6½	10-5/8	640
	263	236	16x2-1/2x35½	27x1½x4½	4x4-1/8x27	7x2-1/4x35	6½	10-7/8
	287	263	17x2-1/2x36½	28x1½x4½	4x5-7/8x28	7x3x36	9	13-3/8
	328	298	18x2-3/4x36½	28x1½x4½	4x5-7/8x28	7x3x36	9	13-7/8
	356	325	19x3x37½	29x1½x4½	4x5-7/8x29	7x3x37	9	13-7/8
	396	364	20x3-1/4x37½	29x1½x4½	4x5-7/8x29	7x3x37	9	14-1/8
27"	197	14x2x35½	27x1½x4½	4x4-1/8x27	7x2-1/4x35	6½	10-3/8	583
	223	15x2-1/4x35½	27x1½x4½	4x4-1/8x27	7x2-1/4x35	6½	10-5/8	640
	263	270	16x2-1/2x36½	28x1½x4½	4x4-1/8x28	7x2-1/4x36	6½	10-7/8
	296	298	17x2-1/2x36½	28x1½x4½	4x6-3/8x28	7x3-1/2x36	10	14-3/8
	328	334	18x2-3/4x37½	29x1½x4½	4x6-3/8x29	7x3-1/2x37	10	14-5/8
	366	364	19x3x37½	29x1½x4½	4x6-3/8x29	7x3-1/2x37	10	14-7/8
	438	403	20x3-1/4x38½	30x1½x4½	4x6-3/8x30	7x3-1/2x38	10	15-1/8
	470	433	21x3-1/4x38½	30x1½x4½	4x6-3/8x30	7x3-1/2x38	10	15-1/8

*Weight does not include 2 anchor bolts @ 12#

ALLOWABLE MOVEMENT = 2½" and 3"

TYPE AND BEARINGS
(Expansion Cont.)

TYPE "D" BEARINGS
FIXED

FIXED BEARINGS

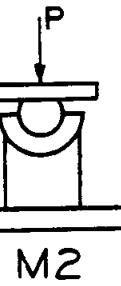
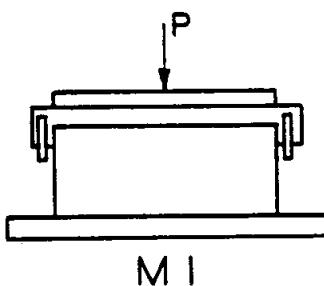
Value of "P" controlled by Masonry Pressure "P_c" = $\frac{bL-3.53}{1+3/b}$

Above formula based on an assumed eccentricity of load = $\frac{1}{2}$ ".

Value of "P" controlled by steel stress;

$$\text{MOMENT M1 } "Ps" = \frac{f_{st}^2(bL-3.53)}{36.75}$$

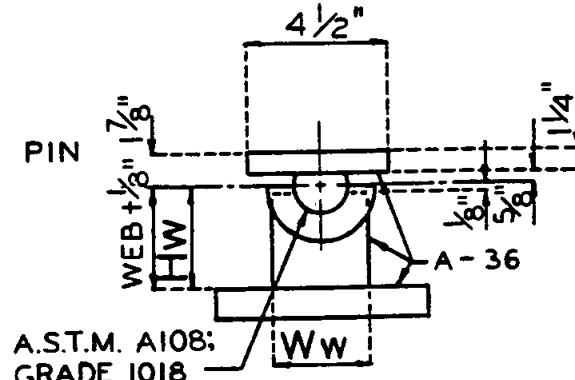
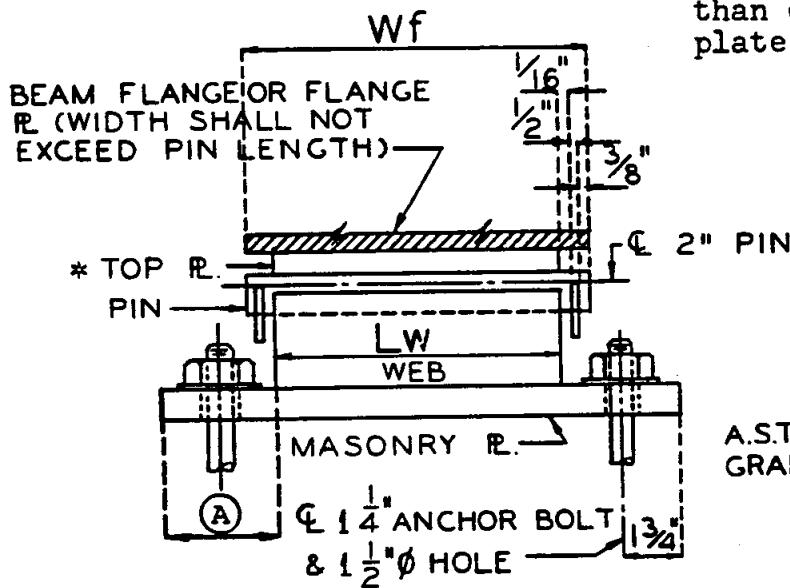
$$\text{MOMENT M2 } "Ps" = \frac{f_{st}^2(bL-3.53)}{3(b/2-1.5)^2}$$



M1

M2

* Length of top plate shall not be less than out to out dimensions of stiffener plates. (Normal to Web)



ANCHOR BOLTS:

Spans thru 150' 1 1/4" A.B.

Spans over 150' 1 1/2" A.B.

All 2 Girder Designs 1 1/2" A.B.

NOTES TO DESIGNER:

1. $L_w \leq W_f + 3"$
2. $H_w \approx W_w$
3. If W_w exceeds 4", use 3" Pin.
4. Masonry B thickness shall be in increments of $\frac{1}{4}"$.
5. $H_w = 2-3/4"$ minimum when 1-1/2" anchor bolts are used.

- (A) Tables for Type "D" Fixed bearings based on this dimension being equal to 4".

TYPE D BEARINGS
FIXED (CONT.)

BOTTOM FLANGE WIDTH OR BEAM DEPTH	TOP PLATE	WEB	MASONRY PLATE	P	HEIGHT (NO LEAD PLATE)	*WEIGHT
8"	9x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3x9	8x1x17	72	6	81
	9x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3x9	8x1 $\frac{1}{4}$ x17	96	6 $\frac{1}{4}$	90
	9x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3x9	9x1x17	81	6	85
	9x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3x9	9x1 $\frac{1}{4}$ x17	112	6 $\frac{1}{4}$	96
	9x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3x9	10x1 $\frac{1}{4}$ x17	128	6 $\frac{1}{4}$	102
	9x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3x9	11x1 $\frac{1}{2}$ x17	144	6 $\frac{1}{2}$	121
9"	10x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3x10	8x1x18	76	6	87
	10x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3x10	8x1 $\frac{1}{4}$ x18	102	6 $\frac{1}{4}$	97
	10x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3x10	9x1x18	86	6	93
	10x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3x10	9x1 $\frac{1}{4}$ x18	119	6 $\frac{1}{4}$	104
	10x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3x10	10x1 $\frac{1}{4}$ x18	136	6 $\frac{1}{4}$	110
	10x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3x10	11x1 $\frac{1}{2}$ x18	153	6 $\frac{1}{2}$	130
W24	10x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3x10	12x1 $\frac{1}{2}$ x18	157	6 $\frac{1}{2}$	138
	10x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3x10	12x1-3/4x18	170	6-3/4	153
	11x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3x11	8x1x19	81	6	94
	11x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3x11	8x1 $\frac{1}{4}$ x19	108	6 $\frac{1}{4}$	105
	11x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3x11	9x1x19	91	6	100
	11x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3x11	9x1 $\frac{1}{4}$ x19	126	6 $\frac{1}{4}$	111
10"	11x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3x11	10x1 $\frac{1}{4}$ x19	143	6 $\frac{1}{4}$	118
	11x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3x11	11x1 $\frac{1}{2}$ x19	161	6 $\frac{1}{2}$	139
	11x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3x11	12x1 $\frac{1}{2}$ x19	166	6 $\frac{1}{2}$	148
	11x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3x11	12x1-3/4x19	180	6-3/4	163
	11x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3x11				
	11x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3x11				
W27	12 $\frac{1}{2}$ x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-7/8x12 $\frac{1}{2}$	8x1x20 $\frac{1}{2}$	87	6-7/8	114
	12 $\frac{1}{2}$ x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-5/8x12 $\frac{1}{2}$	8x1 $\frac{1}{4}$ x20 $\frac{1}{2}$	117	6-7/8	122
	12 $\frac{1}{2}$ x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-7/8x12 $\frac{1}{2}$	9x1x20 $\frac{1}{2}$	98	6-7/8	119
	12 $\frac{1}{2}$ x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-5/8x12 $\frac{1}{2}$	9x1 $\frac{1}{4}$ x20 $\frac{1}{2}$	136	6-7/8	130
	12 $\frac{1}{2}$ x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-5/8x12 $\frac{1}{2}$	10x1 $\frac{1}{4}$ x20 $\frac{1}{2}$	155	6-7/8	137
	12 $\frac{1}{2}$ x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-3/8x12 $\frac{1}{2}$	11x1 $\frac{1}{2}$ x20 $\frac{1}{2}$	174	6-7/8	157
W30	12 $\frac{1}{2}$ x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-3/8x12 $\frac{1}{2}$	12x1 $\frac{1}{2}$ x20 $\frac{1}{2}$	180	6-7/8	166
	12 $\frac{1}{2}$ x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-1/8x12 $\frac{1}{2}$	12x1-3/4x20 $\frac{1}{2}$	194	6-7/8	180
	12 $\frac{1}{2}$ x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-1/8x12 $\frac{1}{2}$	13x1-3/4x20 $\frac{1}{2}$	214	6-7/8	190
	12 $\frac{1}{2}$ x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-1/8x12 $\frac{1}{2}$				
	12 $\frac{1}{2}$ x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-1/8x12 $\frac{1}{2}$				
	12 $\frac{1}{2}$ x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-1/8x12 $\frac{1}{2}$				
12"	13x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-7/8x13	8x1x21	90	6-7/8	118
	13x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-5/8x13	8x1 $\frac{1}{4}$ x21	120	6-7/8	126
	13x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-7/8x13	9x1x21	101	6-7/8	123
	13x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-5/8x13	9x1 $\frac{1}{4}$ x21	139	6-7/8	134
	13x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-5/8x13	10x1 $\frac{1}{4}$ x21	159	6-7/8	141
	13x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-3/8x13	11x1 $\frac{1}{2}$ x21	179	6-7/8	162
W33	13x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-3/8x13	12x1 $\frac{1}{2}$ x21	184	6-7/8	171
	13x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-1/8x13	12x1-3/4x21	199	6-7/8	186
	13x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-1/8x13	13x1-3/4x21	219	6-7/8	196
	13x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-7/8x13	14x2x21	239	6-7/8	224
	13x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-7/8x13				
	13x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-7/8x13				

*Weight does not include 2 anchor bolts @ 12#

TYPE D BEARINGS
FIXED (CONT.)

BOTTOM FLANGE	TOP PLATE	WEB	MASONRY PLATE	P	HEIGHT (NO LEAD PLATE)	*WEIGHT
13"	14x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-7/8x14	8x1x22	94	6-7/8	125
	14x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-5/8x14	8x1 $\frac{1}{2}$ x22	125	6-7/8	134
	14x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-7/8x14	9x1x22	106	6-7/8	131
	14x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-5/8x14	9x1 $\frac{1}{2}$ x22	146	6-7/8	142
	14x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-5/8x14	10x1 $\frac{1}{2}$ x22	167	6-7/8	150
	14x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-3/8x14	11x1 $\frac{1}{2}$ x22	187	6-7/8	172
	14x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-3/8x14	12x1 $\frac{1}{2}$ x22	193	6-7/8	181
	14x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-1/8x14	12x1-3/4x22	208	6-7/8	196
	14x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-1/8x14	13x1-3/4x22	230	6-7/8	207
	14x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-7/8x14	14x2x22	251	6-7/8	237
14"	15x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-7/8x15	8x1x23	98	6-7/8	133
	15x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-5/8x15	8x1 $\frac{1}{2}$ x23	131	6-7/8	142
	15x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-7/8x15	9x1x23	111	6-7/8	139
	15x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-5/8x15	9x1 $\frac{1}{2}$ x23	153	6-7/8	150
	15x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-5/8x15	10x1 $\frac{1}{2}$ x23	174	6-7/8	159
	15x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-3/8x15	11x1 $\frac{1}{2}$ x23	196	6-7/8	181
	15x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-3/8x15	12x1 $\frac{1}{2}$ x23	202	6-7/8	200
	15x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-1/8x15	12x1-3/4x23	218	6-7/8	207
	15x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-1/8x15	13x1-3/4x23	240	6-7/8	218
	15x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-7/8x15	14x2x23	262	6-7/8	249
15"	15x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-5/8x15	15x2-1/4x23	285	6-7/8	283
	16x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-7/8x16	8x1x24	103	6-7/8	140
	16x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-5/8x16	8x1 $\frac{1}{2}$ x24	137	6-7/8	150
	16x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-7/8x16	9x1x24	116	6-7/8	147
	16x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-5/8x16	9x1 $\frac{1}{2}$ x24	159	6-7/8	159
	16x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-5/8x16	10x1 $\frac{1}{2}$ x24	182	6-7/8	167
	16x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-3/8x16	11x1 $\frac{1}{2}$ x24	205	6-7/8	191
	16x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-3/8x16	12x1 $\frac{1}{2}$ x24	211	6-7/8	201
	16x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-1/8x16	12x1-3/4x24	228	6-7/8	218
	16x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-1/8x16	13x1-3/4x24	251	6-7/8	230
16"	16x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-7/8x16	14x2x24	274	6-7/8	262
	16x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-5/8x16	15x2 $\frac{1}{2}$ x24	297	6-7/8	297
	17x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-7/8x17	8x1x25	107	6-7/8	148
	17x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-5/8x17	8x1 $\frac{1}{2}$ x25	143	6-7/8	158
	17x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-7/8x17	9x1x25	121	6-7/8	155
17x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	17x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-5/8x17	9x1 $\frac{1}{2}$ x25	166	6-7/8	167
	17x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-5/8x17	10x1 $\frac{1}{2}$ x25	190	6-7/8	176
	17x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-3/8x17	11x1 $\frac{1}{2}$ x25	213	6-7/8	200
	17x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-3/8x17	12x1 $\frac{1}{2}$ x25	220	6-7/8	211
	17x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-1/8x17	12x1-3/4x25	237	6-7/8	228
	17x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-1/8x17	13x1-3/4x25	261	6-7/8	241
	17x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-7/8x17	14x2x25	285	6-7/8	274
	17x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-5/8x17	15x2-1/4x25	310	6-7/8	311

*Weight does not include 2 anchor bolts @ 12#

TYPE D BEARINGS
FIXED (CONT.)

BOTTOM FLANGE WIDTH	TOP PLATE	WEB	MASONRY PLATE	P	HEIGHT (NO LEAD PLATE)	*WEIGHT
17"	18x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-7/8x18	8x1x26	111	6-7/8	155
	18x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-5/8x18	8x1 $\frac{1}{4}$ x26	149	6-7/8	166
	18x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-7/8x18	9x1x26	125	6-7/8	163
	18x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-5/8x18	9x1 $\frac{1}{4}$ x26	173	6-7/8	175
	18x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-5/8x18	10x1 $\frac{1}{4}$ x26	197	6-7/8	184
	18x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-3/8x18	11x1 $\frac{1}{4}$ x26	222	6-7/8	210
	18x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-3/8x18	12x1 $\frac{1}{4}$ x26	229	6-7/8	221
	18x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-1/8x18	12x1-3/4x26	247	6-7/8	239
	18x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-1/8x18	13x1-3/4x26	272	6-7/8	252
	18x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-7/8x18	14x2x26	297	6-7/8	286
	18x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-5/8x18	15x2 $\frac{1}{4}$ x26	322	6-7/8	325
	18x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-5/8x18	16x2 $\frac{1}{4}$ x26	329	6-7/8	341
	18x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-3/8x18	16x2 $\frac{1}{2}$ x26	347	6-7/8	367
	19x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-7/8x19	8x1x27	116	6-7/8	163
18"	19x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-5/8x19	8x1 $\frac{1}{4}$ x27	155	6-7/8	174
	19x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-7/8x19	9x1x27	130	6-7/8	170
	19x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-5/8x19	9x1 $\frac{1}{4}$ x27	180	6-7/8	183
	19x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-5/8x19	10x1 $\frac{1}{4}$ x27	205	6-7/8	193
	19x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-3/8x19	11x1 $\frac{1}{4}$ x27	231	6-7/8	219
	19x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-3/8x19	12x1 $\frac{1}{4}$ x27	237	6-7/8	231
	19x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-1/8x19	12x1-3/4x27	256	6-7/8	249
	19x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-1/8x19	13x1-3/4x27	282	6-7/8	263
	19x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-7/8x19	14x2x27	308	6-7/8	299
	19x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-5/8x19	15x2 $\frac{1}{4}$ x27	335	6-7/8	338
	19x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-5/8x19	16x2-1/4x27	342	6-7/8	356
	19x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-3/8x19	16x2 $\frac{1}{2}$ x27	361	6-7/8	382
19"	20x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-7/8x20	8x1x28	120	6-7/8	170
	20x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-5/8x20	8x1 $\frac{1}{4}$ x28	160	6-7/8	182
	20x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-7/8x20	9x1x28	135	6-7/8	178
	20x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-5/8x20	9x1 $\frac{1}{4}$ x28	186	6-7/8	192
	20x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-5/8x20	10x1 $\frac{1}{4}$ x28	213	6-7/8	202
	20x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-3/8x20	11x1 $\frac{1}{4}$ x28	239	6-7/8	229
	20x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-3/8x20	12x1 $\frac{1}{4}$ x28	246	6-7/8	241
	20x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-1/8x20	12x1-3/4x28	266	6-7/8	260
	20x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-1/8x20	13x1-3/4x28	293	6-7/8	274
	20x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-7/8x20	14x2x28	320	6-7/8	311
	20x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-5/8x20	15x2 $\frac{1}{4}$ x28	347	6-7/8	352
	20x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-5/8x20	16x2 $\frac{1}{4}$ x28	355	6-7/8	370
	20x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-3/8x20	16x2 $\frac{1}{2}$ x28	374	6-7/8	397

*Weight does not include 2 anchor bolts @ 12#

TYPE D BEARINGS
FIXED (CONT.)

BOTTOM FLANGE WIDTH	TOP PLATE	WEB	MASONRY PLATE	P	HEIGHT (NO LEAD PLATE)	*WEIGHT
20"	21x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-7/8x21	8x1x29	124	6-7/8	178
	21x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-5/8x21	8x1 $\frac{1}{2}$ x29	166	6-7/8	190
	21x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-7/8x21	9x1x29	140	6-7/8	186
	21x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-5/8x21	9x1 $\frac{1}{2}$ x29	193	6-7/8	200
	21x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-5/8x21	10x1 $\frac{1}{2}$ x29	220	6-7/8	210
	21x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-3/8x21	11x1 $\frac{1}{2}$ x29	248	6-7/8	238
	21x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-3/8x21	12x1 $\frac{1}{2}$ x29	255	6-7/8	251
	21x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-1/8x21	12x1-3/4x29	276	6-7/8	271
	21x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-1/8x21	13x1-3/4x29	303	6-7/8	285
	21x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-7/8x21	14x2x29	331	6-7/8	323
	21x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-5/8x21	15x2 $\frac{1}{2}$ x29	360	6-7/8	366
	21x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-5/8x21	16x2 $\frac{1}{2}$ x29	368	6-7/8	384
	21x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-3/8x21	16x2 $\frac{1}{2}$ x29	388	6-7/8	413
21"	22x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-7/8x22	9x1x30	145	6-7/8	194
	22x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-5/8x22	9x1 $\frac{1}{2}$ x30	200	6-7/8	208
	22x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-5/8x22	10x1 $\frac{1}{2}$ x30	228	6-7/8	219
	22x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-3/8x22	11x1 $\frac{1}{2}$ x30	257	6-7/8	248
	22x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-3/8x22	12x1 $\frac{1}{2}$ x30	264	6-7/8	261
	22x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-1/8x22	12x1-3/4x30	285	6-7/8	281
	22x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-1/8x22	13x1-3/4x30	314	6-7/8	296
	22x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-7/8x22	14x2x30	343	6-7/8	336
	22x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-5/8x22	15x2 $\frac{1}{2}$ x30	372	6-7/8	380
	22x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-5/8x22	16x2 $\frac{1}{2}$ x30	381	6-7/8	399
	22x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-3/8x22	16x2 $\frac{1}{2}$ x30	401	6-7/8	428
	22x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-3/8x22	17x2 $\frac{1}{2}$ x30	431	6-7/8	449
22"	23x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-7/8x23	9x1x31	150	6-7/8	202
	23x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-5/8x23	9x1 $\frac{1}{2}$ x31	207	6-7/8	216
	23x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-5/8x23	10x1 $\frac{1}{2}$ x31	236	6-7/8	227
	23x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-3/8x23	11x1 $\frac{1}{2}$ x31	265	6-7/8	257
	23x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-3/8x23	12x1 $\frac{1}{2}$ x31	273	6-7/8	271
	23x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-1/8x23	12x1-3/4x31	295	6-7/8	292
	23x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-1/8x23	13x1-3/4x31	325	6-7/8	307
	23x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-7/8x23	14x2x31	355	6-7/8	348
	23x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-5/8x23	15x2 $\frac{1}{2}$ x31	385	6-7/8	394
	23x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-5/8x23	16x2 $\frac{1}{2}$ x31	393	6-7/8	413
	23x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-3/8x23	16x2 $\frac{1}{2}$ x31	415	6-7/8	443
	23x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-3/8x23	17x2 $\frac{1}{2}$ x31	445	6-7/8	465
23"	24x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-7/8x24	10x1x32	172	6-7/8	219
	24x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-5/8x24	10x1 $\frac{1}{2}$ x32	243	6-7/8	236
	24x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-3/8x24	11x1 $\frac{1}{2}$ x32	274	6-7/8	267
	24x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-3/8x24	12x1 $\frac{1}{2}$ x32	282	6-7/8	281
	24x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-1/8x24	12x1-3/4x32	304	-7/8	302

*Weight does not include 2 anchor bolts @ 12#

TYPE D BEARINGS
(FIXED CONT.)

BOTTOM FLANGE WIDTH	TOP PLATE	WEB	MASONRY PLATE	P	HEIGHT (NO LEAD PLATE)	*WEIGHT
23"	24x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-1/8x24	13x1-3/4x32	335	6-7/8	318
	24x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-7/8x24	14x2x32	366	6-7/8	361
	24x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-5/8x24	15x2 $\frac{1}{4}$ x32	397	6-7/8	407
	24x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-5/8x24	16x2 $\frac{1}{4}$ x32	406	6-7/8	428
	24x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-3/8x24	16x2 $\frac{1}{2}$ x32	428	6-7/8	459
	24x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-3/8x24	17x2 $\frac{1}{2}$ x32	459	6-7/8	481
	24x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-5/8x24	18x2-3/4x32	491	7-3/8	550
24"	25x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-7/8x25	10x1x33	178	6-7/8	227
	25x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-5/8x25	10x1 $\frac{1}{4}$ x33	251	6-7/8	245
	25x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-3/8x25	11x1 $\frac{1}{4}$ x33	282	6-7/8	277
	25x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-3/8x25	12x1 $\frac{1}{4}$ x33	291	6-7/8	291
	25x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-1/8x25	12x1-3/4x33	314	6-7/8	313
	25x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-1/8x25	13x1-3/4x33	346	6-7/8	329
	25x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-7/8x25	14x2x33	378	6-7/8	373
	25x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-5/8x25	15x2 $\frac{1}{4}$ x33	410	6-7/8	421
	25x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-5/8x25	16x2 $\frac{1}{4}$ x33	419	6-7/8	442
	25x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-3/8x25	16x2 $\frac{1}{2}$ x33	442	6-7/8	474
	25x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-3/8x25	17x2 $\frac{1}{2}$ x33	474	6-7/8	497
	25x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-5/8x25	18x2-3/4x33	506	7-3/8	568
25"	26x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-7/8x26	10x1x34	183	6-7/8	235
	26x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-5/8x26	10x1 $\frac{1}{4}$ x34	259	6-7/8	253
	26x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-3/8x26	11x1 $\frac{1}{4}$ x34	291	6-7/8	286
	26x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-3/8x26	12x1 $\frac{1}{4}$ x34	300	6-7/8	300
	26x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-1/8x26	12x1-3/4x34	324	6-7/8	324
	26x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-1/8x26	13x1-3/4x34	356	6-7/8	340
	26x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-7/8x26	14x2x34	389	6-7/8	385
	26x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-5/8x26	15x2 $\frac{1}{4}$ x34	422	6-7/8	435
	26x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-5/8x26	16x2 $\frac{1}{4}$ x34	432	6-7/8	457
	26x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-3/8x26	16x2 $\frac{1}{2}$ x34	455	6-7/8	489
	26x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-3/8x26	17x2 $\frac{1}{2}$ x34	488	6-7/8	513
	26x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-5/8x26	18x2-3/4x34	522	7-3/8	586
26"	27x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-7/8x27	11x1x35	159	6-7/8	253
	27x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-5/8x27	11x1 $\frac{1}{4}$ x35	248	6-7/8	274
	27x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-3/8x27	11x1 $\frac{1}{2}$ x35	300	6-7/8	296
	27x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-3/8x27	12x1 $\frac{1}{2}$ x35	309	6-7/8	310
	27x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-1/8x27	12x1-3/4x35	333	6-7/8	334
	27x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x3-1/8x27	13x1-3/4x35	367	6-7/8	352
	27x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-7/8x27	14x2x35	401	6-7/8	398
	27x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-5/8x27	15x2 $\frac{1}{4}$ x35	435	6-7/8	449
	27x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-5/8x27	16x2 $\frac{1}{4}$ x35	445	6-7/8	471
	27x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-3/8x27	16x2 $\frac{1}{2}$ x35	469	6-7/8	505
	27x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-3/8x27	17x2 $\frac{1}{2}$ x35	503	6-7/8	529
	27x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-5/8x27	18x2-3/4x35	537	7-3/8	604
	27x1 $\frac{1}{4}$ x4 $\frac{1}{2}$	3x2-3/8x27	19x3x35	571	7-3/8	673

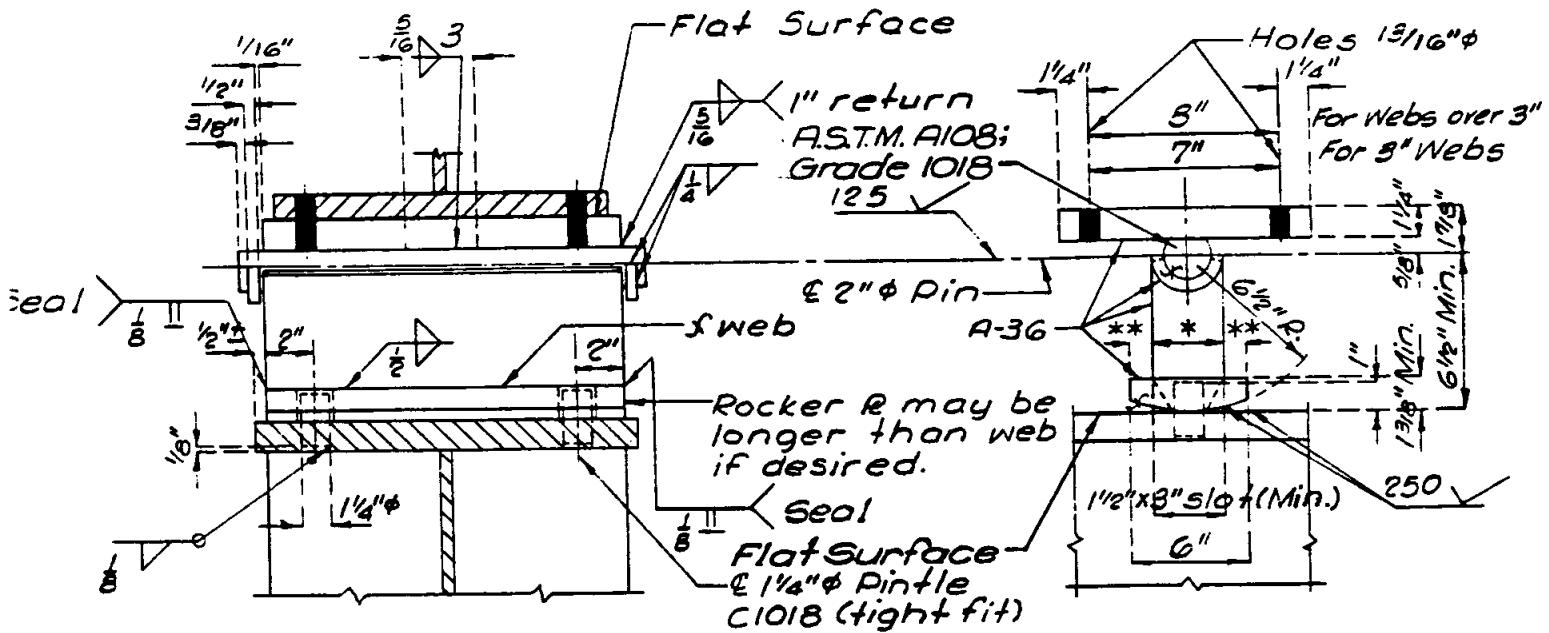
*Weight does not include 2 anchor bolts @ 12#

TYPE D BEARINGS
(FIXED CONT.)

BOTTOM FLANGE WIDTH	TOP PLATE	WEB	MASONRY PLATE	P	HEIGHT (NO LEAD PLATE)	*WEIGHT
27"	28x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	3x3-7/8x28	11x1x36	164	6-7/8	261
	28x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	3x3-5/8x28	11x1 $\frac{1}{4}$ x36	256	6-7/8	283
	28x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	3x3-3/8x28	11x1 $\frac{1}{2}$ x36	308	6-7/8	305
	28x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	3x3-3/8x28	12x1 $\frac{1}{2}$ x36	317	6-7/8	320
	28x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	3x3-1/8x28	12x1-3/4x36	343	6-7/8	345
	28x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	3x3-1/8x28	13x1-3/4x36	377	6-7/8	363
	28x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	3x2-7/8x28	14x2x36	412	6-7/8	410
	28x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	3x2-5/8x28	15x2 $\frac{1}{2}$ x36	447	6-7/8	462
	28x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	3x2-5/8x28	16x2 $\frac{1}{2}$ x36	457	6-7/8	485
	28x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	3x2-3/8x28	16x2 $\frac{1}{2}$ x36	482	6-7/8	520
	28x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	3x2-3/8x28	17x2 $\frac{1}{2}$ x36	517	6-7/8	545
	28x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	3x2-5/8x28	18x2-3/4x36	552	7-3/8	623
	28x1 $\frac{1}{2}$ x4 $\frac{1}{2}$	3x2-3/8x28	19x3x36	588	7-3/8	693

*Weight does not include 2 anchor bolts @ 12#

TYPE "D" MODIFIED BEARING



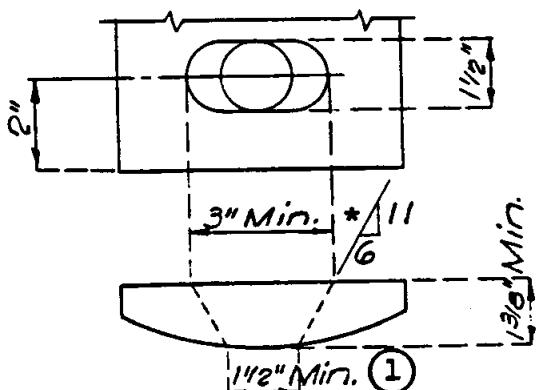
* 3" For Bridge Expansion less than 250'
4" For Bridge Expansion more than 250'

** For 3" Web use $1\frac{1}{2}$ "
For 4" Web use 1"

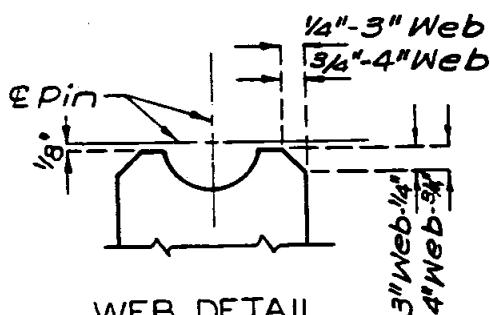
① 2" For Bridge Expansion more than 250'

ROCKER PLATE LENGTH	
MAXIMUM REACTION	ROCKER PLATE LENGTH
80.7K	12"
89.7K	13"
99.0K	14"
107.6K	15"

Note: All steel A-36



DETAIL OF BEVEL SLOT



WEB DETAIL

**TYPE "E" BEARINGS
EXPANSION**

DESIGN DATA: Steel A-36, $f_s = 20,000$ psi.
Maximum allowable Masonry Pressure = 1,000 psi.

ANCHOR BOLT SPACING: Use same anchor bolt spacing for all interior bents when difference in spacing would be 1" or less. If necessary, increase appropriate masonry plate size to accommodate larger spacing. (Use $1\frac{1}{4}$ " A.B. except for 2 Girder Design in which case use $1\frac{1}{2}$ " A.B.)

EXPANSION BEARINGS: Value of "P" controlled by Masonry Pressure.

$$\text{"e" IN MIDDLE } \frac{1}{3} \\ \text{"Pc" = } \frac{\text{Lb} - (3.53)*}{1 + 6e/b}$$

$$\text{"e" OUT OF MIDDLE } \frac{1}{3} \\ \text{"Pc" = } \frac{3'b/2 - e)L - (3.53)*}{2}$$

Value of "P" controlled by Steel Stress.

$$\text{"Ps" = } \frac{1.333 \text{ fst}^2 [L - (3**)]}{b}$$

BEVEL PLATES: Not required

*Use 4.81 for 1-3/4" holes ($1\frac{1}{4}$ " A.B.)
**Use 3.5 for 1-3/4" holes ($1\frac{1}{4}$ " A.B.)

P = Capacity of Bearing in Kips

b = Width of bottom plate

L = Length of bottom plate

e = Eccentricity ****

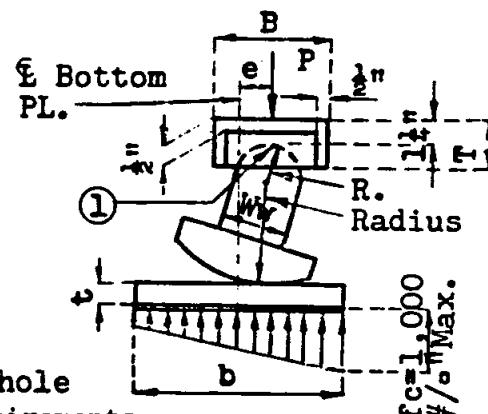
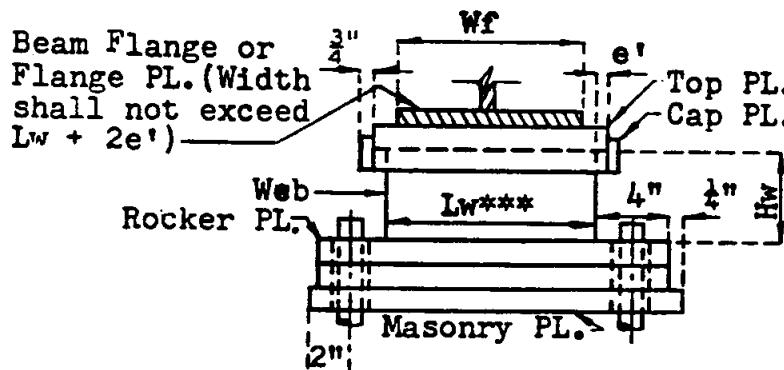
t = Bottom plate thickness

B = Width of top plate

T = Top plate thickness

Length of span or spans	60'	80'	100'	180'	260'	340'	420'
Eccentricity to use	3/4"	7/8"	1"	1 $\frac{1}{2}$ "	2"	2 $\frac{1}{2}$ "	3"

**** Design of expansion or contraction for Type "E" Bearings.
(Use $1/16$ " per 10' of span from fixed bearing + $3/8$ ".)



① See Special Provisions for lubrication requirements.

*** Length of web shall not be less than out to out dimensions of stiff plates. (Normal to web.)

e' = Lateral Expansion (Consult Structural Design Engineer)

NOTES TO DESIGNER:

1. Strive to obtain as much duplication as possible in machined bearing parts (rocker assemblies) within bridges and Projects.
2. $L_w \leq W_f + 3"$.
3. $H_w \leq 2W_w$.
4. Allowable bearing pressure on lubricant for design = 5,000 psi.
5. A vertical line from ϵ Pin shall not fall outside web at maximum eccentricity.
6. Masonry Plate thickness and Rocker plate thickness shall be in increments of $\frac{1}{8}$ ".

TYPE "E" BEARINGS
EXPANSION (CON'T)

SELECTION CRITERIA:

Proceed as if a Type "D" Expansion Bearing is required.

Select a masonry plate, rocker plate, and radius as listed in the appropriate table.

Revise the web and top plate dimensions as follows:

WEB PLATE WIDTH		TOP PLATE FOR TYPE "E"		
TYPE "D"	TYPE "E"	B	T	R
3"	4"	6"	2 $\frac{1}{4}$ "	2"
4"	5"	7"	2 $\frac{1}{2}$ "	2 $\frac{1}{2}$ "

Height and weight of Type "E" Expansion Bearings will differ from the corresponding Type "D" Expansion Bearings.

Weight of Type "E" Bearings (Expansion and Fixed) are available from a program for the Monroe 1880 calculator. Consult the Development Section.

TYPE "E" BEARINGS
FIXED

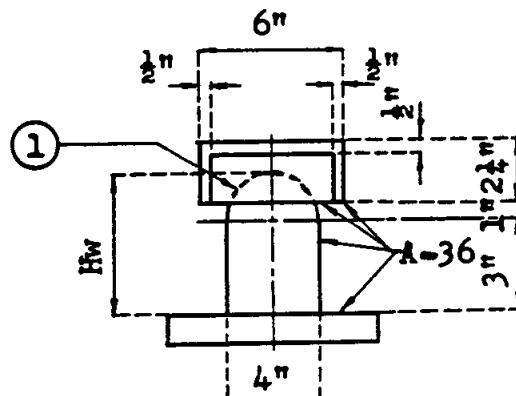
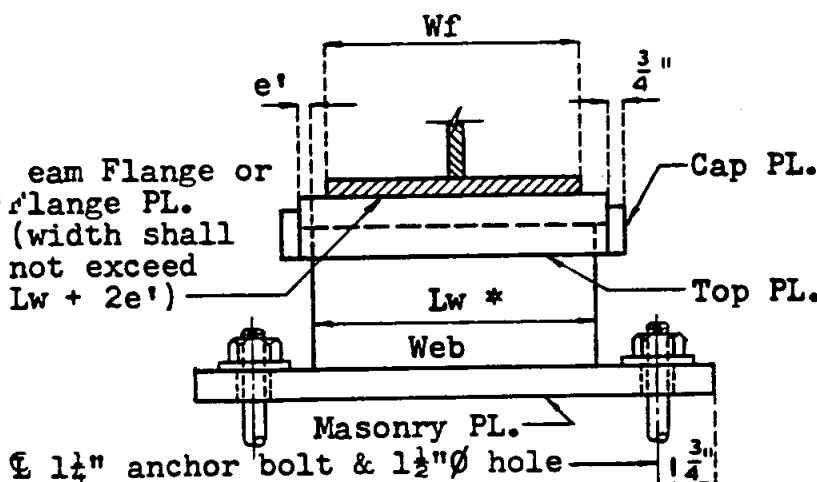
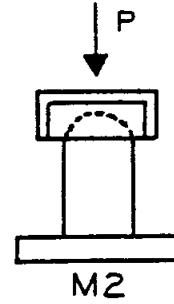
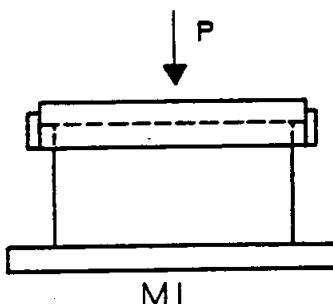
FIXED BEARINGS:

Value of "P" controlled by Masonry Pressure "Pc" = $\frac{bL-3.53}{1+3/b}$

Above formula based on an assumed eccentricity of load = $\frac{1}{2}$ ".

Value of "P" controlled by steel stress;

$$\text{MOMENT M1 } "Ps" = \frac{f_{st}^2(bL-3.53)}{36.75} \quad \text{MOMENT M2 } "Ps" = \frac{f_{st}^2(bL-3.53)}{\frac{3(b/2-1.5)^2}{2}}$$



ANCHOR BOLTS:

Spans thru 150' $1\frac{1}{4}"$ A.B.

Spans over 150' $1\frac{1}{2}"$ A.B.

All 2 Girder Designs $1\frac{1}{2}"$ A.B.

NOTES TO DESIGNER:

1. $L_w \leq W_f + 3"$

2. Masonry PL. thickness shall be in increments of $\frac{1}{4}"$.

3. Allowable bearing pressure on lubricant for design = 5,000 psi.

* Length of web shall not be less than out to out dimensions of stiffener plates. (Normal to Web).

e' = Lateral expansion (Consult Structural Design Engineer).

① See Special Provisions for lubrication requirements.

TYPE "E" BEARINGS
FIXED (CONT.)

BOTTOM FLANGE WIDTH or BEAM DEPTH	TOP PLATE	WEB	MASONRY PLATE	P	HEIGHT (NO LEAD PLATE)
8" or W21	(9+2e')x2 $\frac{1}{4}$ x6	4x5x9	8x1x17	72	7 $\frac{1}{4}$
	(9+2e')x2 $\frac{1}{4}$ x6	4x5x9	8x1 $\frac{1}{4}$ x17	96	7 $\frac{1}{2}$
	(9+2e')x2 $\frac{1}{4}$ x6	4x5x9	9x1x17	81	7 $\frac{1}{4}$
	(9+2e')x2 $\frac{1}{4}$ x6	4x5x9	9x1 $\frac{1}{4}$ x17	112	7 $\frac{1}{2}$
	(9+2e')x2 $\frac{1}{4}$ x6	4x5x9	10x1 $\frac{1}{4}$ x17	128	7 $\frac{1}{2}$
	(9+2e')x2 $\frac{1}{4}$ x6	4x5x9	11x1 $\frac{1}{2}$ x17	144	7-3/4
9" or W24	(10+2e')x2 $\frac{1}{4}$ x6	4x5x10	8x1x18	76	7 $\frac{1}{4}$
	(10+2e')x2 $\frac{1}{4}$ x6	4x5x10	8x1 $\frac{1}{4}$ x18	102	7 $\frac{1}{2}$
	(10+2e')x2 $\frac{1}{4}$ x6	4x5x10	9x1x18	86	7 $\frac{1}{4}$
	(10+2e')x2 $\frac{1}{4}$ x6	4x5x10	9x1 $\frac{1}{4}$ x18	119	7 $\frac{1}{2}$
	(10+2e')x2 $\frac{1}{4}$ x6	4x5x10	10x1 $\frac{1}{4}$ x18	136	7 $\frac{1}{2}$
	(10+2e')x2 $\frac{1}{4}$ x6	4x5x10	11x1 $\frac{1}{2}$ x18	153	7-3/4
10" or W27	(11+2e')x2 $\frac{1}{4}$ x6	4x5x11	8x1x19	81	7 $\frac{1}{4}$
	(11+2e')x2 $\frac{1}{4}$ x6	4x5x11	8x1 $\frac{1}{4}$ x19	108	7 $\frac{1}{2}$
	(11+2e')x2 $\frac{1}{4}$ x6	4x5x11	9x1x19	91	7 $\frac{1}{4}$
	(11+2e')x2 $\frac{1}{4}$ x6	4x5x11	9x1 $\frac{1}{4}$ x19	126	7 $\frac{1}{2}$
	(11+2e')x2 $\frac{1}{4}$ x6	4x5x11	10x1 $\frac{1}{4}$ x19	143	7 $\frac{1}{2}$
	(11+2e')x2 $\frac{1}{4}$ x6	4x5x11	11x1 $\frac{1}{2}$ x19	161	7-3/4
11" or W30	(12+2e')x2 $\frac{1}{4}$ x6	4x5x12	8x1x20	85	7 $\frac{1}{4}$
	(12+2e')x2 $\frac{1}{4}$ x6	4x5x12	8x1 $\frac{1}{4}$ x20	114	7 $\frac{1}{2}$
	(12+2e')x2 $\frac{1}{4}$ x6	4x5x12	9x1x20	96	7 $\frac{1}{4}$
	(12+2e')x2 $\frac{1}{4}$ x6	4x5x12	9x1 $\frac{1}{4}$ x20	132	7 $\frac{1}{2}$
	(12+2e')x2 $\frac{1}{4}$ x6	4x5x12	10x1 $\frac{1}{4}$ x20	151	7 $\frac{1}{2}$
	(12+2e')x2 $\frac{1}{4}$ x6	4x5x12	11x1 $\frac{1}{2}$ x20	170	7-3/4
12" or W33	(12+2e')x2 $\frac{1}{4}$ x6	4x5x12	12x1 $\frac{1}{2}$ x20	189	7-3/4
	(12+2e')x2 $\frac{1}{4}$ x6	4x5x12	13x1-3/4x20	208	8
	(13+2e')x2 $\frac{1}{4}$ x6	4x5x13	8x1x21	90	7 $\frac{1}{4}$
	(13+2e')x2 $\frac{1}{4}$ x6	4x5x13	8x1 $\frac{1}{4}$ x21	120	7 $\frac{1}{2}$
	(13+2e')x2 $\frac{1}{4}$ x6	4x5x13	9x1x21	101	7 $\frac{1}{4}$
	(13+2e')x2 $\frac{1}{4}$ x6	4x5x13	9x1 $\frac{1}{4}$ x21	139	7 $\frac{1}{2}$
	(13+2e')x2 $\frac{1}{4}$ x6	4x5x13	10x1 $\frac{1}{4}$ x21	159	7 $\frac{1}{2}$
	(13+2e')x2 $\frac{1}{4}$ x6	4x5x13	11x1 $\frac{1}{2}$ x21	179	7-3/4
	(13+2e')x2 $\frac{1}{4}$ x6	4x5x13	12x1 $\frac{1}{2}$ x21	199	7-3/4
	(13+2e')x2 $\frac{1}{4}$ x6	4x5x13	13x1-3/4x21	219	8
	(13+2e')x2 $\frac{1}{4}$ x6	4x5x13	14x2x21	225	8 $\frac{1}{4}$

TYPE "E" BEARINGS
FIXED (CONT.)

BOTTOM FLANGE WIDTH or BEAM DEPTH	TOP PLATE	WEB	MASONRY PLATE	P	HEIGHT (NO LEAD PLATE)
W36	(14+2e')x2 $\frac{1}{4}$ x6	4x5x14	8x1x22	94	7 $\frac{1}{4}$
	(14+2e')x2 $\frac{1}{4}$ x6	4x5x14	8x1 $\frac{1}{4}$ x22	125	7 $\frac{1}{2}$
	(14+2e')x2 $\frac{1}{4}$ x6	4x5x14	9x1x22	106	7 $\frac{1}{4}$
	(14+2e')x2 $\frac{1}{4}$ x6	4x5x14	9x1 $\frac{1}{4}$ x22	146	7 $\frac{1}{2}$
	(14+2e')x2 $\frac{1}{4}$ x6	4x5x14	10x1 $\frac{1}{4}$ x22	167	7 $\frac{1}{2}$
	(14+2e')x2 $\frac{1}{4}$ x6	4x5x14	11x1 $\frac{1}{2}$ x22	187	7-3/4
	(14+2e')x2 $\frac{1}{4}$ x6	4x5x14	12x1 $\frac{1}{2}$ x22	208	7-3/4
	(14+2e')x2 $\frac{1}{4}$ x6	4x5x14	13x1-3/4x22	230	8
	(14+2e')x2 $\frac{1}{4}$ x6	4x5x14	14x2x22	242	8 $\frac{1}{4}$
14"	(15+2e')x2 $\frac{1}{4}$ x6	4x5x15	8x1x23	98	7 $\frac{1}{4}$
	(15+2e')x2 $\frac{1}{4}$ x6	4x5x15	8x1 $\frac{1}{4}$ x23	131	7 $\frac{1}{2}$
	(15+2e')x2 $\frac{1}{4}$ x6	4x5x15	9x1x23	111	7 $\frac{1}{4}$
	(15+2e')x2 $\frac{1}{4}$ x6	4x5x15	9x1 $\frac{1}{4}$ x23	153	7 $\frac{1}{2}$
	(15+2e')x2 $\frac{1}{4}$ x6	4x5x15	10x1 $\frac{1}{4}$ x23	174	7 $\frac{1}{2}$
	(15+2e')x2 $\frac{1}{4}$ x6	4x5x15	11x1 $\frac{1}{2}$ x23	196	7-3/4
	(15+2e')x2 $\frac{1}{4}$ x6	4x5x15	12x1 $\frac{1}{2}$ x23	218	7-3/4
	(15+2e')x2 $\frac{1}{4}$ x6	4x5x15	13x1-3/4x23	240	8
	(15+2e')x2 $\frac{1}{4}$ x6	4x5x15	14x2x23	259	8 $\frac{1}{4}$
	(16+2e')x2 $\frac{1}{4}$ x6	4x5x16	8x1x24	103	7 $\frac{1}{4}$
15"	(16+2e')x2 $\frac{1}{4}$ x6	4x5x16	8x1 $\frac{1}{4}$ x24	137	7 $\frac{1}{2}$
	(16+2e')x2 $\frac{1}{4}$ x6	4x5x16	9x1x24	116	7 $\frac{1}{4}$
	(16+2e')x2 $\frac{1}{4}$ x6	4x5x16	9x1 $\frac{1}{4}$ x24	159	7 $\frac{1}{2}$
	(16+2e')x2 $\frac{1}{4}$ x6	4x5x16	10x1 $\frac{1}{4}$ x24	182	7 $\frac{1}{2}$
	(16+2e')x2 $\frac{1}{4}$ x6	4x5x16	11x1 $\frac{1}{2}$ x24	205	7-3/4
	(16+2e')x2 $\frac{1}{4}$ x6	4x5x16	12x1 $\frac{1}{2}$ x24	228	7-3/4
	(16+2e')x2 $\frac{1}{4}$ x6	4x5x16	13x1-3/4x24	251	8
	(16+2e')x2 $\frac{1}{4}$ x6	4x5x16	14x2x24	274	8 $\frac{1}{4}$
	(16+2e')x2 $\frac{1}{4}$ x6	4x5x16	15x2 $\frac{1}{4}$ x24	277	8 $\frac{1}{2}$
	(17+2e')x2 $\frac{1}{4}$ x6	4x5x17	8x1x25	107	7 $\frac{1}{4}$
16"	(17+2e')x2 $\frac{1}{4}$ x6	4x5x17	8x1 $\frac{1}{4}$ x25	143	7 $\frac{1}{2}$
	(17+2e')x2 $\frac{1}{4}$ x6	4x5x17	9x1x25	121	7 $\frac{1}{4}$
	(17+2e')x2 $\frac{1}{4}$ x6	4x5x17	9x1 $\frac{1}{4}$ x25	166	7 $\frac{1}{2}$
	(17+2e')x2 $\frac{1}{4}$ x6	4x5x17	10x1 $\frac{1}{4}$ x25	190	7 $\frac{1}{2}$
	(17+2e')x2 $\frac{1}{4}$ x6	4x5x17	11x1 $\frac{1}{2}$ x25	213	7-3/4
	(17+2e')x2 $\frac{1}{4}$ x6	4x5x17	12x1 $\frac{1}{2}$ x25	237	7-3/4
	(17+2e')x2 $\frac{1}{4}$ x6	4x5x17	13x1-3/4x25	261	8
	(17+2e')x2 $\frac{1}{4}$ x6	4x5x17	14x2x25	285	8 $\frac{1}{4}$
	(17+2e')x2 $\frac{1}{4}$ x6	4x5x17	15x2-1/4x25	294	8 $\frac{1}{2}$

TYPE "E" BEARINGS
FIXED (CONT.)

BOTTOM FLANGE WIDTH	TOP PLATE	WEB	MASONRY PLATE	P	HEIGHT (NO LEAD PLATE)
17"	(18+2e')x2 $\frac{1}{4}$ x6	4x5x18	8x1x26	111	7 $\frac{1}{4}$
	(18+2e')x2 $\frac{1}{4}$ x6	4x5x18	8x1 $\frac{1}{4}$ x26	149	7 $\frac{1}{2}$
	(18+2e')x2 $\frac{1}{4}$ x6	4x5x18	9x1x26	125	7 $\frac{1}{4}$
	(18+2e')x2 $\frac{1}{4}$ x6	4x5x18	9x1 $\frac{1}{4}$ x26	173	7 $\frac{1}{2}$
	(18+2e')x2 $\frac{1}{4}$ x6	4x5x18	10x1 $\frac{1}{4}$ x26	197	7 $\frac{1}{2}$
	(18+2e')x2 $\frac{1}{4}$ x6	4x5x18	11x1 $\frac{1}{4}$ x26	222	7-3/4
	(18+2e')x2 $\frac{1}{4}$ x6	4x5x18	12x1 $\frac{1}{4}$ x26	247	7-3/4
	(18+2e')x2 $\frac{1}{4}$ x6	4x5x18	13x1-3/4x26	272	8
	(18+2e')x2 $\frac{1}{4}$ x6	4x5x18	14x2x26	297	8 $\frac{1}{4}$
	(18+2e')x2 $\frac{1}{4}$ x6	4x5x18	15x2 $\frac{1}{4}$ x26	311	8 $\frac{1}{2}$
18"	(19+2e')x2 $\frac{1}{4}$ x6	4x5x19	8x1x27	116	7 $\frac{1}{4}$
	(19+2e')x2 $\frac{1}{4}$ x6	4x5x19	8x1 $\frac{1}{4}$ x27	155	7 $\frac{1}{2}$
	(19+2e')x2 $\frac{1}{4}$ x6	4x5x19	9x1x27	130	7 $\frac{1}{4}$
	(19+2e')x2 $\frac{1}{4}$ x6	4x5x19	9x1 $\frac{1}{4}$ x27	180	7 $\frac{1}{2}$
	(19+2e')x2 $\frac{1}{4}$ x6	4x5x19	10x1 $\frac{1}{4}$ x27	205	7 $\frac{1}{2}$
	(19+2e')x2 $\frac{1}{4}$ x6	4x5x19	11x1 $\frac{1}{4}$ x27	231	7-3/4
	(19+2e')x2 $\frac{1}{4}$ x6	4x5x19	12x1 $\frac{1}{4}$ x27	256	7-3/4
	(19+2e')x2 $\frac{1}{4}$ x6	4x5x19	13x1-3/4x27	282	8
	(19+2e')x2 $\frac{1}{4}$ x6	4x5x19	14x2x27	308	8 $\frac{1}{4}$
	(19+2e')x2 $\frac{1}{4}$ x6	4x5x19	15x2 $\frac{1}{4}$ x27	329	8 $\frac{1}{2}$
19"	(20+2e')x2 $\frac{1}{4}$ x6	4x5x20	8x1x28	120	7 $\frac{1}{4}$
	(20+2e')x2 $\frac{1}{4}$ x6	4x5x20	8x1 $\frac{1}{4}$ x28	160	7 $\frac{1}{2}$
	(20+2e')x2 $\frac{1}{4}$ x6	4x5x20	9x1x28	135	7 $\frac{1}{4}$
	(20+2e')x2 $\frac{1}{4}$ x6	4x5x20	9x1 $\frac{1}{4}$ x28	186	7 $\frac{1}{2}$
	(20+2e')x2 $\frac{1}{4}$ x6	4x5x20	10x1 $\frac{1}{4}$ x28	213	7 $\frac{1}{2}$
	(20+2e')x2 $\frac{1}{4}$ x6	4x5x20	11x1 $\frac{1}{4}$ x28	239	7-3/4
	(20+2e')x2 $\frac{1}{4}$ x6	4x5x20	12x1 $\frac{1}{4}$ x28	266	7-3/4
	(20+2e')x2 $\frac{1}{4}$ x6	4x5x20	13x1-3/4x28	293	8
	(20+2e')x2 $\frac{1}{4}$ x6	4x5x20	14x2x28	320	8 $\frac{1}{4}$
	(20+2e')x2 $\frac{1}{4}$ x6	4x5x20	15x2 $\frac{1}{4}$ x28	346	8 $\frac{1}{2}$

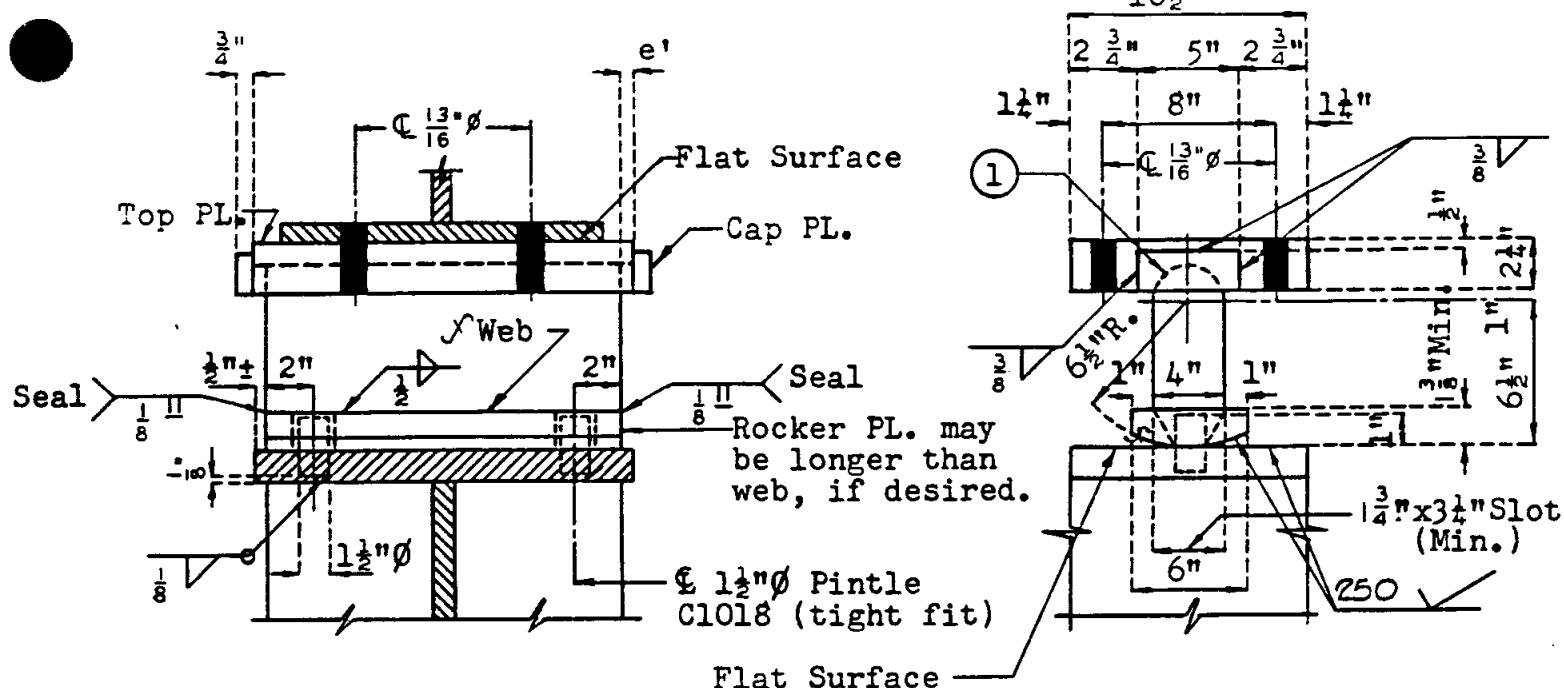
TYPE "E" BEARINGS
FIXED (CONT.)

BOTTOM FLANGE WIDTH	TOP PLATE	WEB	MASONRY PLATE	P	HEIGHT (NO LEAD PLATE)
20"	(21+2e')x2 $\frac{1}{4}$ x6	4x5x21	8x1x29	124	7 $\frac{1}{4}$
	(21+2e')x2 $\frac{1}{4}$ x6	4x5x21	8x1 $\frac{1}{4}$ x29	166	7 $\frac{1}{2}$
	(21+2e')x2 $\frac{1}{4}$ x6	4x5x21	9x1x29	140	7 $\frac{1}{4}$
	(21+2e')x2 $\frac{1}{4}$ x6	4x5x21	9x1 $\frac{1}{4}$ x29	193	7 $\frac{1}{2}$
	(21+2e')x2 $\frac{1}{4}$ x6	4x5x21	10x1 $\frac{1}{4}$ x29	220	7 $\frac{1}{2}$
	(21+2e')x2 $\frac{1}{4}$ x6	4x5x21	11x1 $\frac{1}{2}$ x29	248	7-3/4
	(21+2e')x2 $\frac{1}{4}$ x6	4x5x21	12x1 $\frac{1}{2}$ x29	276	7-3/4
	(21+2e')x2 $\frac{1}{4}$ x6	4x5x21	13x1-3/4x29	303	8
	(21+2e')x2 $\frac{1}{4}$ x6	4x5x21	14x2x29	331	8 $\frac{1}{4}$
	(21+2e')x2 $\frac{1}{4}$ x6	4x5x21	15x2 $\frac{1}{4}$ x29	360	8 $\frac{1}{2}$
	(21+2e')x2 $\frac{1}{4}$ x6	4x5x21	16x2 $\frac{1}{4}$ x29	363	8 $\frac{1}{2}$
21"	(22+2e')x2 $\frac{1}{4}$ x6	4x5x22	9x1x30	145	7 $\frac{1}{4}$
	(22+2e')x2 $\frac{1}{4}$ x6	4x5x22	9x1 $\frac{1}{4}$ x30	200	7 $\frac{1}{2}$
	(22+2e')x2 $\frac{1}{4}$ x6	4x5x22	10x1 $\frac{1}{4}$ x30	228	7 $\frac{1}{2}$
	(22+2e')x2 $\frac{1}{4}$ x6	4x5x22	11x1 $\frac{1}{2}$ x30	257	7-3/4
	(22+2e')x2 $\frac{1}{4}$ x6	4x5x22	12x1 $\frac{1}{2}$ x30	285	7-3/4
	(22+2e')x2 $\frac{1}{4}$ x6	4x5x22	13x1-3/4x30	314	8
	(22+2e')x2 $\frac{1}{4}$ x6	4x5x22	14x2x30	343	8 $\frac{1}{4}$
	(22+2e')x2 $\frac{1}{4}$ x6	4x5x22	15x2 $\frac{1}{4}$ x30	372	8 $\frac{1}{2}$
	(22+2e')x2 $\frac{1}{4}$ x6	4x5x22	16x2 $\frac{1}{4}$ x30	381	8 $\frac{1}{2}$
22"	(23+2e')x2 $\frac{1}{4}$ x6	4x5x23	9x1x31	150	7 $\frac{1}{4}$
	(23+2e')x2 $\frac{1}{4}$ x6	4x5x23	9x1 $\frac{1}{4}$ x31	207	7 $\frac{1}{2}$
	(23+2e')x2 $\frac{1}{4}$ x6	4x5x23	10x1 $\frac{1}{4}$ x31	236	7 $\frac{1}{2}$
	(23+2e')x2 $\frac{1}{4}$ x6	4x5x23	11x1 $\frac{1}{2}$ x31	265	7-3/4
	(23+2e')x2 $\frac{1}{4}$ x6	4x5x23	12x1 $\frac{1}{2}$ x31	295	7-3/4
	(23+2e')x2 $\frac{1}{4}$ x6	4x5x23	13x1-3/4x31	325	8
	(23+2e')x2 $\frac{1}{4}$ x6	4x5x23	14x2x31	355	8 $\frac{1}{4}$
	(23+2e')x2 $\frac{1}{4}$ x6	4x5x23	15x2 $\frac{1}{4}$ x31	385	8 $\frac{1}{2}$
	(23+2e')x2 $\frac{1}{4}$ x6	4x5x23	16x2 $\frac{1}{4}$ x31	398	8 $\frac{1}{2}$
23"	(24+2e')x2 $\frac{1}{4}$ x6	4x5x24	10x1x32	172	7 $\frac{1}{4}$
	(24+2e')x2 $\frac{1}{4}$ x6	4x5x24	10x1 $\frac{1}{4}$ x32	243	7 $\frac{1}{2}$
	(24+2e')x2 $\frac{1}{4}$ x6	4x5x24	11x1 $\frac{1}{2}$ x32	274	7-3/4
	(24+2e')x2 $\frac{1}{4}$ x6	4x5x24	12x1 $\frac{1}{2}$ x32	304	7-3/4
	(24+2e')x2 $\frac{1}{4}$ x6	4x5x24	13x1-3/4x32	335	8
	(24+2e')x2 $\frac{1}{4}$ x6	4x5x24	14x2x32	366	8 $\frac{1}{4}$
	(24+2e')x2 $\frac{1}{4}$ x6	4x5x24	15x2 $\frac{1}{4}$ x32	397	8 $\frac{1}{2}$
	(24+2e')x2 $\frac{1}{4}$ x6	4x5x24	16x2 $\frac{1}{4}$ x32	416	8 $\frac{1}{2}$

TYPE "E" BEARINGS
FIXED (CONT.)

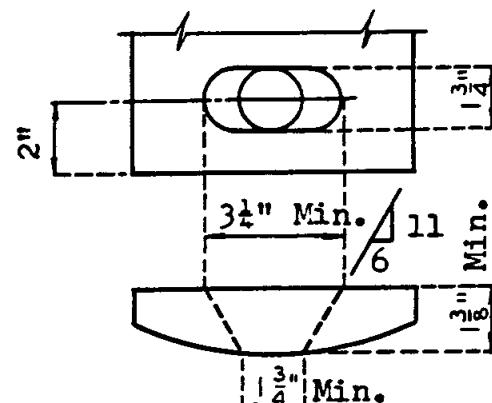
BOTTOM FLANGE WIDTH	TOP PLATE	WEB	MASONRY PLATE	P	HEIGHT (NO LEAD PLATE)
24"	(25+2e')x2 $\frac{1}{4}$ x6	4x5x25	10x1x33	178	7 $\frac{1}{4}$
	(25+2e')x2 $\frac{1}{4}$ x6	4x5x25	10x1 $\frac{1}{4}$ x33	251	7 $\frac{1}{2}$
	(25+2e')x2 $\frac{1}{4}$ x6	4x5x25	11x1 $\frac{1}{2}$ x33	282	7-3/4
	(25+2e')x2 $\frac{1}{4}$ x6	4x5x25	12x1 $\frac{1}{2}$ x33	314	7-3/4
	(25+2e')x2 $\frac{1}{4}$ x6	4x5x25	13x1-3/4x33	346	8
	(25+2e')x2 $\frac{1}{4}$ x6	4x5x25	14x2x33	378	8 $\frac{1}{4}$
	(25+2e')x2 $\frac{1}{4}$ x6	4x5x25	15x2 $\frac{1}{4}$ x33	410	8 $\frac{1}{2}$
	(25+2e')x2 $\frac{1}{4}$ x6	4x5x25	16x2 $\frac{1}{4}$ x33	433	8 $\frac{1}{2}$
25"	(26+2e')x2 $\frac{1}{4}$ x6	4x5x26	10x1x34	183	7 $\frac{1}{4}$
	(26+2e')x2 $\frac{1}{4}$ x6	4x5x26	10x1 $\frac{1}{4}$ x34	259	7 $\frac{1}{2}$
	(26+2e')x2 $\frac{1}{4}$ x6	4x5x26	11x1 $\frac{1}{2}$ x34	291	7-3/4
	(26+2e')x2 $\frac{1}{4}$ x6	4x5x26	12x1 $\frac{1}{2}$ x34	324	7-3/4
	(26+2e')x2 $\frac{1}{4}$ x6	4x5x26	13x1-3/4x34	356	8
	(26+2e')x2 $\frac{1}{4}$ x6	4x5x26	14x2x34	389	8 $\frac{1}{4}$
	(26+2e')x2 $\frac{1}{4}$ x6	4x5x26	15x2 $\frac{1}{4}$ x34	422	8 $\frac{1}{2}$
	(26+2e')x2 $\frac{1}{4}$ x6	4x5x26	16x2 $\frac{1}{4}$ x34	450	8 $\frac{1}{2}$
26"	(27+2e')x2 $\frac{1}{4}$ x6	4x5x27	11x1x35	207	7 $\frac{1}{4}$
	(27+2e')x2 $\frac{1}{4}$ x6	4x5x27	11x1 $\frac{1}{4}$ x35	300	7 $\frac{1}{2}$
	(27+2e')x2 $\frac{1}{4}$ x6	4x5x27	12x1 $\frac{1}{2}$ x35	333	7-3/4
	(27+2e')x2 $\frac{1}{4}$ x6	4x5x27	13x1-3/4x35	367	8
	(27+2e')x2 $\frac{1}{4}$ x6	4x5x27	14x2x35	401	8 $\frac{1}{4}$
	(27+2e')x2 $\frac{1}{4}$ x6	4x5x27	15x2 $\frac{1}{4}$ x35	435	8 $\frac{1}{2}$
	(27+2e')x2 $\frac{1}{4}$ x6	4x5x27	16x2 $\frac{1}{4}$ x35	467	8 $\frac{1}{2}$
	(28+2e')x2 $\frac{1}{4}$ x6	4x5x28	11x1x36	213	7 $\frac{1}{4}$
27"	(28+2e')x2 $\frac{1}{4}$ x6	4x5x28	11x1 $\frac{1}{4}$ x36	308	7 $\frac{1}{2}$
	(28+2e')x2 $\frac{1}{4}$ x6	4x5x28	12x1 $\frac{1}{2}$ x36	343	7-3/4
	(28+2e')x2 $\frac{1}{4}$ x6	4x5x28	13x1-3/4x36	377	8
	(28+2e')x2 $\frac{1}{4}$ x6	4x5x28	14x2x36	412	8 $\frac{1}{4}$
	(28+2e')x2 $\frac{1}{4}$ x6	4x5x28	15x2 $\frac{1}{4}$ x36	447	8 $\frac{1}{2}$
	(28+2e')x2 $\frac{1}{4}$ x6	4x5x28	16x2 $\frac{1}{4}$ x36	482	8 $\frac{1}{2}$

TYPE "E" MODIFIED BEARING



- (1) See Special Provisions for lubrication requirements.

ROCKER PLATE LENGTH	
Maximum Reaction	Rocker PL. Length
76.2 ^k	12"
85.2 ^k	13"
94.2 ^k	14"
103.2 ^k	15"



DETAIL OF BEVEL SLOT

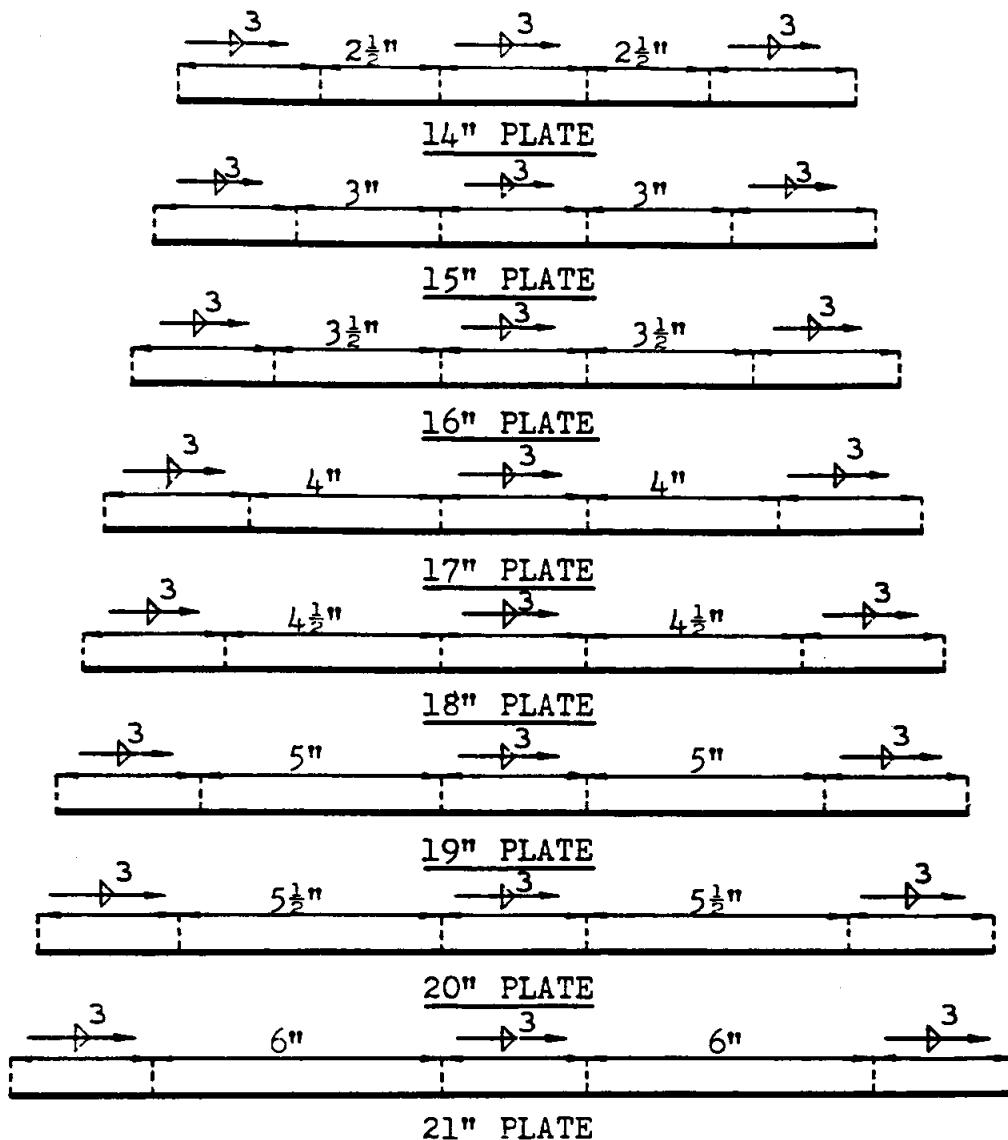
NOTE: All steel to be A-36.

TOP PLATE WELDING DETAILS

TYPE "D" & "E" BEARINGS
(Top Brg. Plate to Flange)

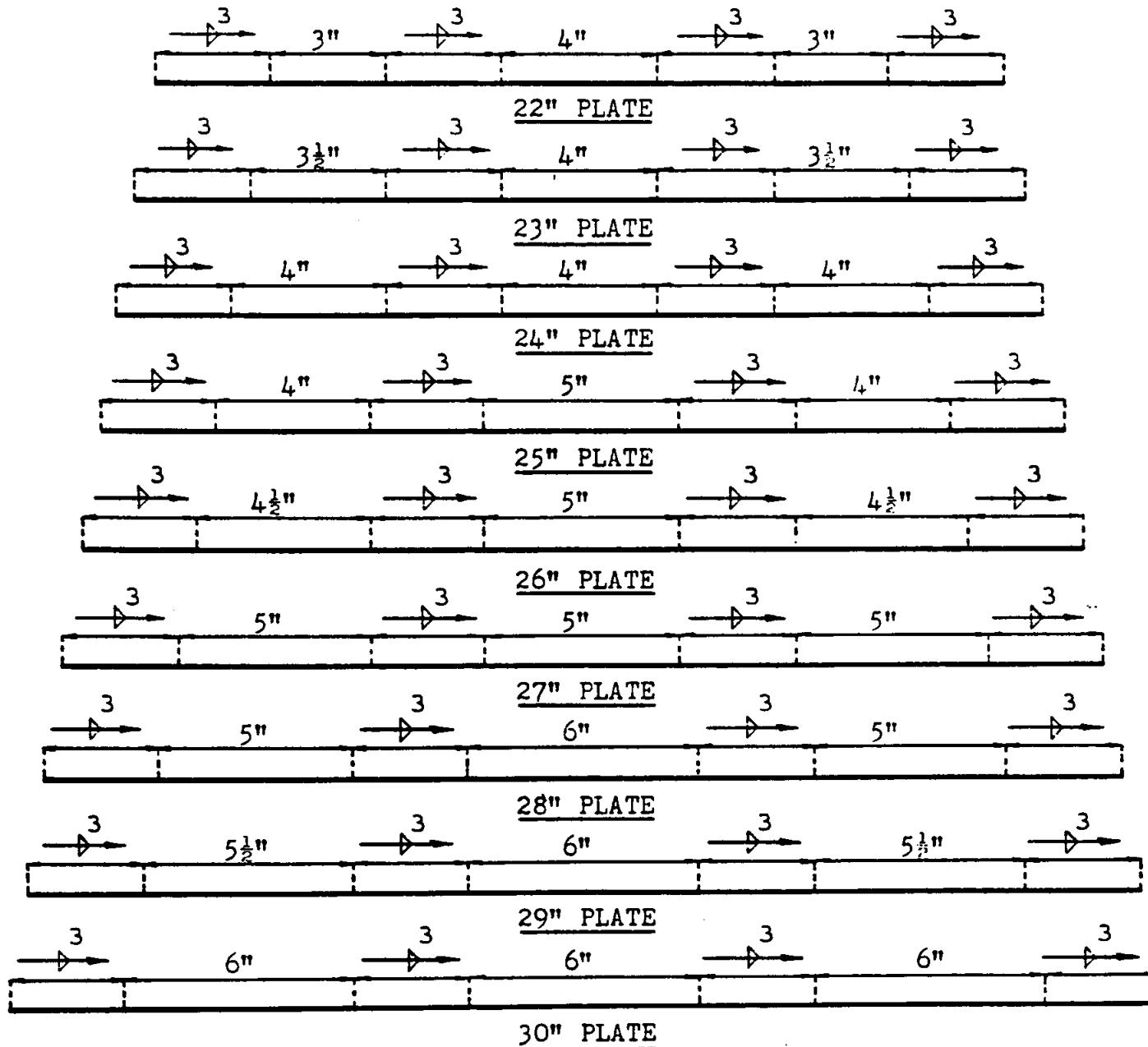
Top bearing plates *13" or less in length shall be welded to the bottom flange plate with a 3" long weld at each corner, transverse to flange.

Top bearing plates *larger than 13" in length shall be welded to the bottom flange plate with a series of 3" long welds as shown below.



* Top plate length or flange width, whichever is shorter, will control welding dimensions.

TOP PLATE WELDING DETAILS
 TYPE "D" & "E" BEARINGS
 (TOP BRG. PLATE TO FLANGE CON'T.)



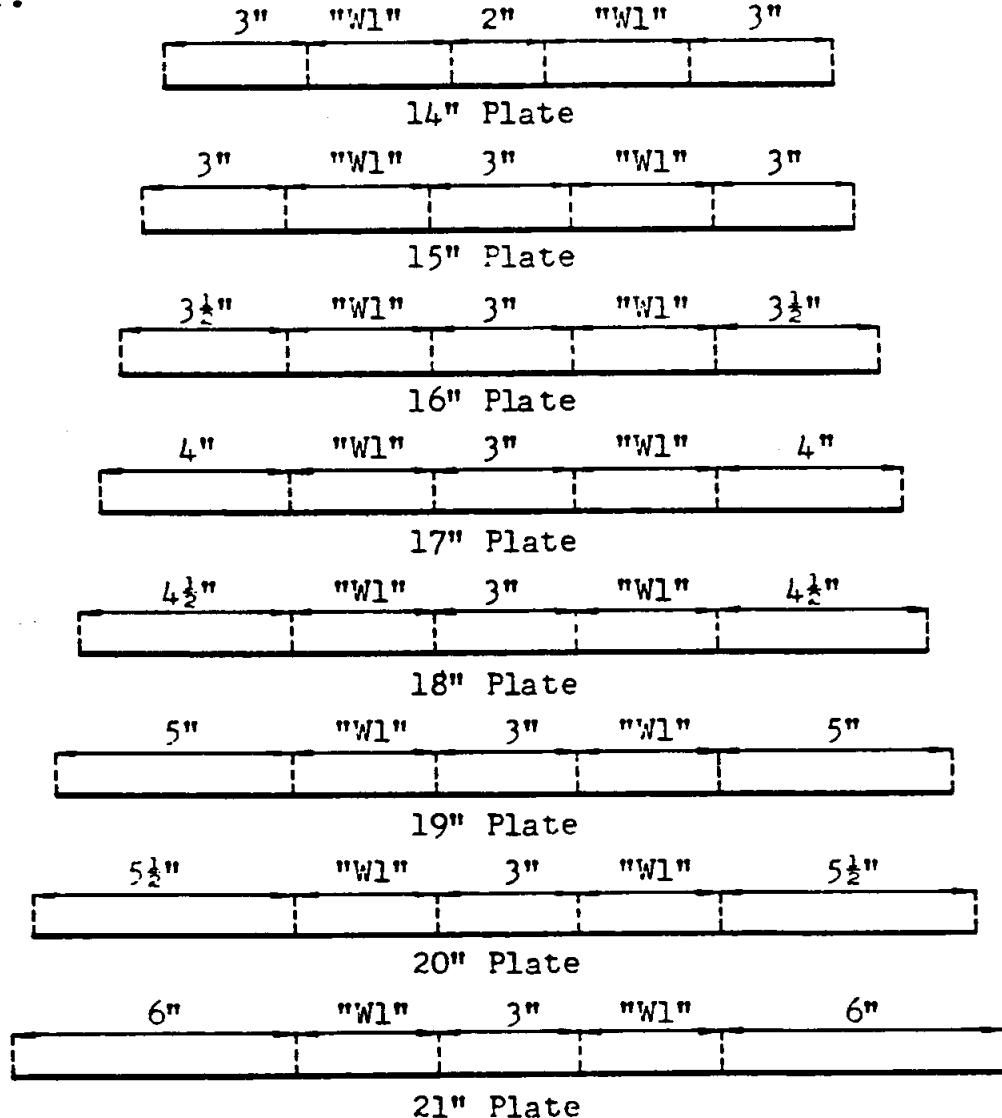
TOP PLATE WELDING DETAILS

TYPE "D" BEARINGS
(Top Brg. Plate to Pin)

Top bearing plates 13" or less in length shall be welded to the pin with a $5/16 \times 3"$ long weld centered on the pin in its longitudinal direction.

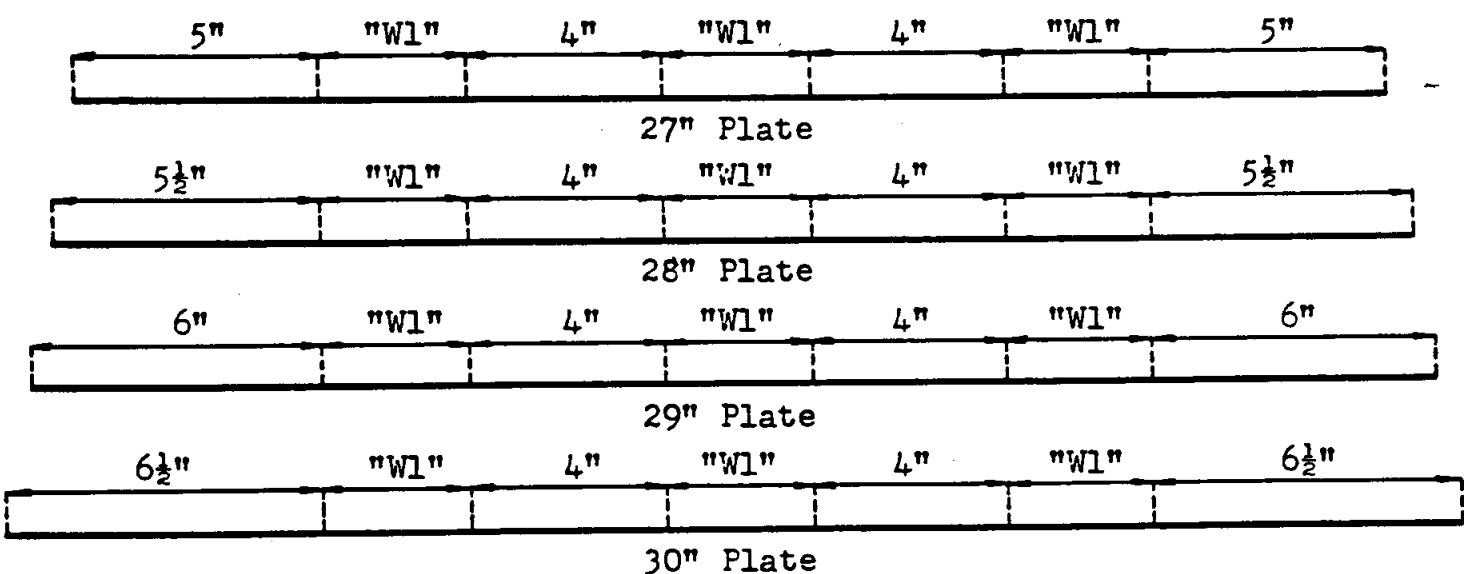
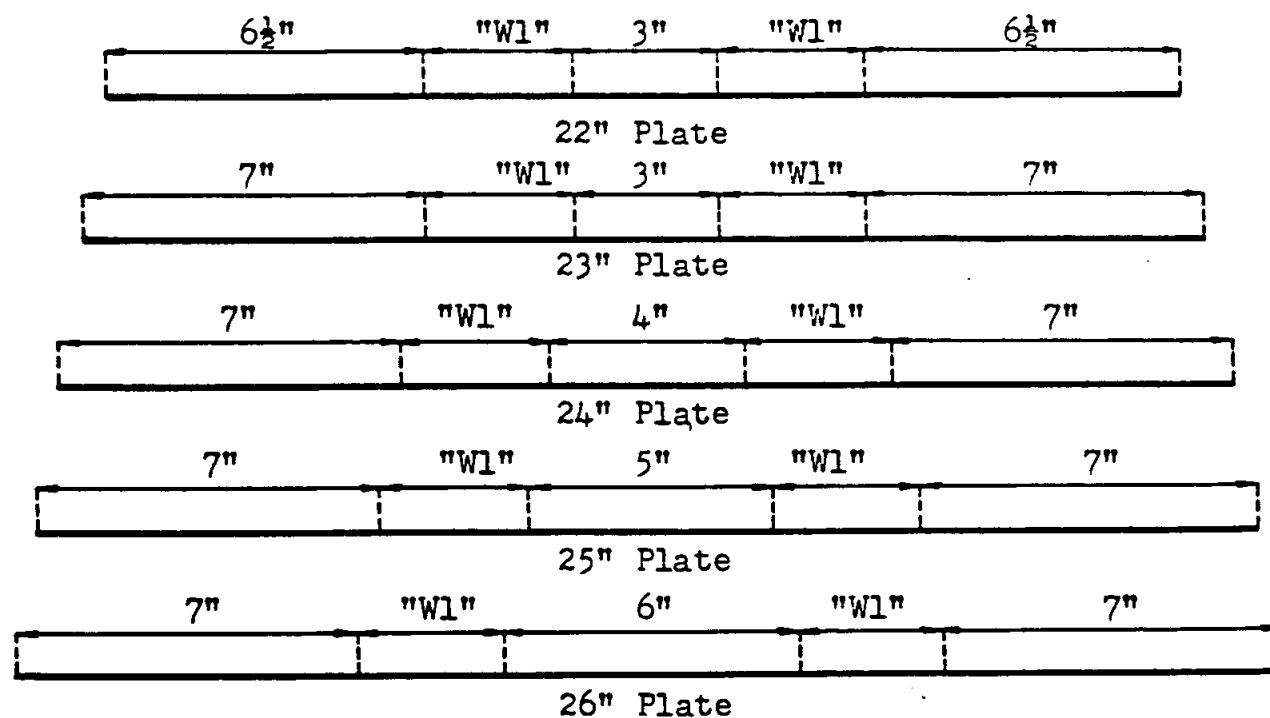
Top bearing plates larger than 13" in length shall be welded to the pin with a series of $5/16 \times 3"$ long welds ("W1").

There shall also be a $5/16$ weld with a 1" return at each corner.



"W1" = $5/16 \times 3"$ Weld Both Sides.

TOP PLATE WELDING DETAILS
 TYPE "D" BEARINGS
 (TOP BRG. PLATE TO PIN CON'T)



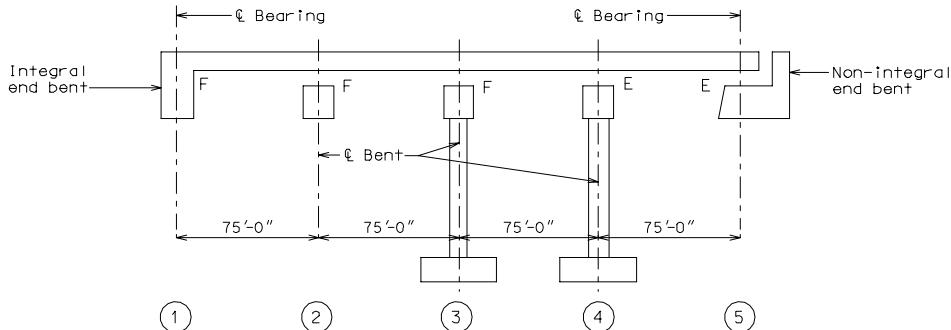
"W1" = 5/16 x 3" Weld Both Sides.

STANDARD FIXED BEARING PAD DESIGN

Elastomeric Bearing Pads

The standard fixed bearing pad is to be used on all flexible bents (such as pile cap bents) and at all fixed bents (such as bent no. 3 of a four span continuous structure) whether this bent is flexible or rigid (such as an open bent).

EXAMPLE:



End Bent 1 : Integral construction –
use standard plain fixed bearings.

Int. Bent 2 : Flexible bent (pile cap) –
use standard laminated fixed bearings.

Int. Bent 3 : Rigid bent - fixed (no movement) –
use standard laminated fixed bearings.

Int. Bent 4 : Rigid bent - expansion –
use standard laminated expansion bearings.

End Bent 5 : Rigid bent - expansion –
use standard laminated expansion bearings.

Note: Pot bearings are used on long bridges with sharp curvature requiring a large lateral rotation and displacement. Limited applications recommended due to high cost. Before using this type of bearings, consult the Structural Project Manager.

Elastomeric Bearing Pads
STANDARD FIXED BEARING PAD DESIGN (CONT.)

Standard bearing pads for steel and P/S I-Girders are to be used if possible. Use design and figures provided in this section. Bearing pads for box girders, slabs, and special structures shall be designed in accordance with this section.

Bearings for structures shall be designed according to AASHTO 1996 and interims 1997 and 1998. The design should follow "Method A" (AASHTO Article 14.6.6). Except for compressive stress requirements for plain pads at integral end bents as defined below.

For Plain Elastomer Pad, (AASHTO Article 14.6.6.3.2)

$$\sigma_{TL} \leq 0.55 \text{ GS and } \sigma_{TL} \leq 0.80 \text{ ksi}$$

Plain elastomer pad shall be used in integral concrete end bent diaphragms. When this is the case...

$$\sigma_{TL} \leq 1.00 \text{ GS and } \sigma_{TL} \leq 0.80 \text{ ksi}$$

For laminated pad, (AASHTO Article 14.6.6.3.2)

$$\sigma_{TL} \leq 1.00 \text{ GS and } \sigma_{TL} \leq 1.00 \text{ ksi}$$

ROTATIONAL REQUIREMENT

Rotations shall be taken as the maximum possible change in slope between the top and bottom surfaces of the bearing caused by the initial lack of parallelism between the bottom of girder flange and top of bearing and the girder end rotation due to imposed loads and movements. The following equation must be satisfied to ensure that uplift does not occur under any combination of loads and corresponding rotations:

$$\sigma_{TL} \geq 0.50 \text{ GS' (L/T)}^2 \theta \text{ m,x (AASHTO Article 14.6.6.3.5-1)}$$

Plain elastomeric bearing pads contained within integral concrete diaphragm are not subject to this rotation requirement.

Elastomeric Bearing Pads

STANDARD FIXED BEARING PAD DESIGN (CONT.)ROTATIONAL REQUIREMENT (CONT.)

TABLE OF $\theta_{m,x}$ (RADIAN) (*)				
		Maximum Span Length (***)	End Bent	Interior Bent
P/S 1-GIRDER	Type 2	46'-0"	0.0045	0.0010
	Type 3	57'-0"	0.0050	0.0010
	Type 4	66'-0"	0.0052	0.0010
	Type 6	89'-0"	0.0059	0.0010
	Type 7	110'-0"	0.0051	0.0008
	42" Web	90'-0"	0.0081	0.0020
	48" Web	100'-0"	0.0080	0.0018
PLATE GIRDERS	54" Web	110'-0"	0.0078	0.0018
	60" Web	125'-0"	0.0085	0.0019
	66" Web	140'-0"	0.0093	0.0019
	72" Web	150'-0"	0.0093	0.0019

* All of the $\theta_{m,x}$ values are calculated for rotations caused by dead loads and live loads only. Additional rotation due to girder camber must be added (in radians) to the values displayed in the table for bearing pad design. A straight line approximation from ℓ bearing to quarter or tenth point is an acceptable method of calculating the camber rotation.

*** If the span length exceeds the length shown in the table, the rotations must be recalculated by the designer.

REFERENCES

1996 AASHTO Specifications and 1997 & 1998 Interim - Section 14.

AASHTO CRITERIA - Article 14.6.6.3.6

To ensure stability, the total thickness of elastomer (T) shall not exceed L/3 or W/3
Length (L) - Parallel to the direction of translation.

Width (W) - Perpendicular to the direction of translation.

SYMBOL DEFINITIONS

t = Thickness of plain bearing or individual internal layer of elastomer in a laminated bearing. (preferred min. for plain bearing = 1/2") (1/4" for P/S double tee girders).

tt & tb = Thickness of top or bottom layer laminate with one side not heat bonded to plate (standard = 1/4").

T = Total effective elastomer thickness (summation of t's and tt & tb's).
 $\geq 2(\text{total temperature movement}) = 2 \Delta$

$$S = \text{Shape Factor} \quad S = \frac{LW}{2t(L+W)} \quad \text{OR} \quad t = \frac{LW}{2(L+W)S}$$

For laminated bearings, use the thickest individual layer of the bearing for compression stress check. For rotation, check both t & tt-tb. (AASHTO Article 14.6.6.3.2 and AASHTO Article 14.6.6.3.5)

G = Shear Modulus (PSI) (AASHTO Article 14.3) for design use:

$$\begin{aligned} G &= 120 \text{ PSI } 60 \text{ Durometer } (**) \\ G &= 160 \text{ PSI } 70 \text{ Durometer} \end{aligned}$$

above G values are for shear, compression, rotation or duration loads.

$\theta_{m,x}$ = Maximum rotation about transverse axis due to initial lack of parallelism plus dead load and live load.

(**) use G = 155 for plain elastomeric pads surrounded by an integral concrete diaphragm.

Elastomeric Bearing Pads

STANDARD FIXED BEARING PAD DESIGN (CONT.)SYMBOL DEFINITIONS (CONT.)

P = Average compressive stress in a layer (psi)

P = 0.55 GS and shall not exceed 800 psi; for plain pads (AASHTO Article 14.6.6.3.2)

P = 1.00 GS and shall not exceed 1000 psi; for plain pads contained within an integral concrete diaphragm.

P = 1.00 GS and shall not exceed 1000 psi; for laminated pads (AASHTO Article 14.6.6.3.2)

DL = Service load dead load (pounds or kips)

DL_{min} = DL1 + barrier curb

DL_{max} = DL1 + barrier curb + future wearing surface

LL = service load live load (no impact) (pounds or kips)

At the intermediate bents with 2 bearing pads per girder line, use 1/2 of the live load reaction for each pad.

MoDOT DESIGN REQUIREMENTS

$$\text{Min. DL} = .2(LW) \quad \text{or} \quad \frac{DL}{LW} > 200 \text{ Psi}$$

$$\text{Max. DL} = .5(LW) \quad \text{or} \quad \frac{DL}{LW} < 500 \text{ Psi}$$

$$\text{Max. (DL+LL)} = P(LW) \quad \text{or} \quad \frac{(DL+LL)}{LW} < P < 800 \text{ Psi for plain pads.} \\ 1000 \text{ Psi for laminated pads.}$$

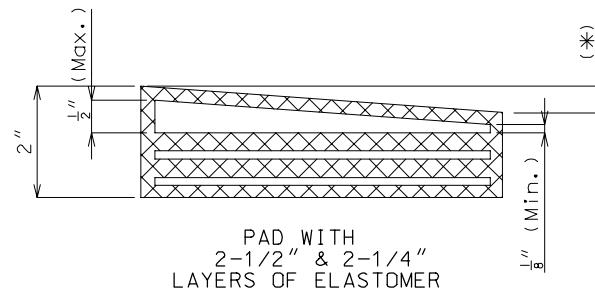
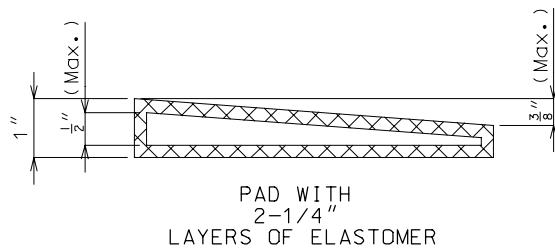
Hardness: use 60 Durometer hardness for all bearings, except 70 Durometer pads are used for PTFE expansion bearings.

BEARING TAPER

Fixed plain pads 1/2" thick are used only at integral end bents when the required taper due to girder slope is less than 1/8".

Laminated bearing taper is provided by tapering the top shim to match the slope of the girder to the nearest 1/8" total difference in thickness. Thickness of shims shall be a minimum of 1/8" and a maximum of 1/2". For excessive girder slopes it may be necessary to taper the top two shims.

Tapered layers of elastomer are not allowed.

EXAMPLES:

(*) 3/8" (Max.) for 1 tapered shim
3/4" (Max.) for 2 tapered shims

STANDARD FIXED BEARING PAD DESIGN (CONT.)

Elastomeric Bearing Pads

PAD DEFLECTION (ELASTOMERIC EXPANSION BEARING)

For expansion bearing design, it is necessary to determine the total temperature movement, Δ .

$$\Delta = (\text{thermal coefficients}) (\text{temperature range}) (\text{expansion length}) (\phi) = \text{total temperature movement}$$

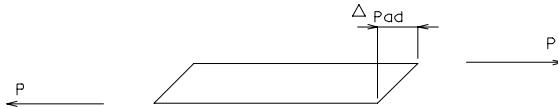
$$\Delta (\text{steel}) = (.0000065) (140^\circ) (\text{expansion length}) (\phi)$$

$$\Delta (\text{concrete}) = (.000006) (120^\circ) (\text{expansion length}) (\phi)$$

$\phi = 1.00$ @ int. bent and semi-deep abut.

$\phi = 1.25$ @ end bent (additional safety factor due to earth pressure)

For the substructure design it is necessary to determine the bearing pad deflection due to shear forces such as longitudinal wind, longitudinal forces from live load, and the temperature.



The following equation may be used to compute the pad deflection of an expansion pad.

$$\Delta_{\text{Pad}} = \frac{P \times T}{L \times W \times G}$$

This equation can be used to find shear resistance, P , given a pad deflection, where:

- P = Shear Force
- T = Pad Thickness (elastomer only)
- L = Length of Pad
- W = Width of Pad
- G = Shear Modulus

For distribution of the longitudinal temperature forces and the longitudinal wind forces, the following values of the shear modulus, G, should be used:

60 durometer

G Min. = 150 psi

G Max. = 300 psi

G values above are for temporary loads.

Note: The shear modulus varies with the durometer, temperature and the load duration.

**STANDARD ELASTOMERIC BEARING PAD DETAILS
FOR P/S GIRDERS**

Elastomeric Bearing Pads

FIXED BEARINGS - All integral end bents

Thickness - use 1/2" plain pads for I-Girders
use 1/4" plain pads for Double-Tee girders

Hardness - use 60 hardness

Length and width - see table 3 for I-Girders
see Sec. 3.56 for Double-Tee girders

FIXED BEARINGS - integral intermediate bents

Thickness - use $t = 1/2"$ $tt = 1/4"$ $tb = 1/4"$
use laminated pad with 2 layers of 1/4" elastomer
 $"C"$ = total bearing height = 5/8"

Hardness - use 60 hardness

Length and width - see table 2

EXPANSION BEARINGS

THICKNESS - LAMINATED PADS (*)						
Δ (in.)	t (in.)	$tt+tb$ (in.) (ea.)	T (in.) (**)	Layers t Elast.	Layers $tt+tb$ Elast.	C (in.)
1/2	1/2	1/4	1	1	2	1-1/4
3/4	1/2	1/4	1-1/2	2	2	1-7/8
1	1/2	1/4	2	3	2	2-1/2
1-1/4	1/2	1/4	2-1/2	4	2	3-1/8
1-1/2	1/2	1/4	3	5	2	3-3/4
1-3/4	1/2	1/4	3-1/2	6	2	4-3/8
2	1/2	1/4	4	7	2	5
2-1/4	1/2	1/4	4-1/2	8	2	5-5/8
2-1/2	1/2	1/4	5	9	2	6-1/4

Δ = Total temperature movement

t = Thickness of middle layers of elastomer

$tt+tb$ = Thickness of top and bottom layers of elastomer

T = Total effective thickness of elastomer (sum of t and $tt+tb$)

C = Total thickness including steel shims

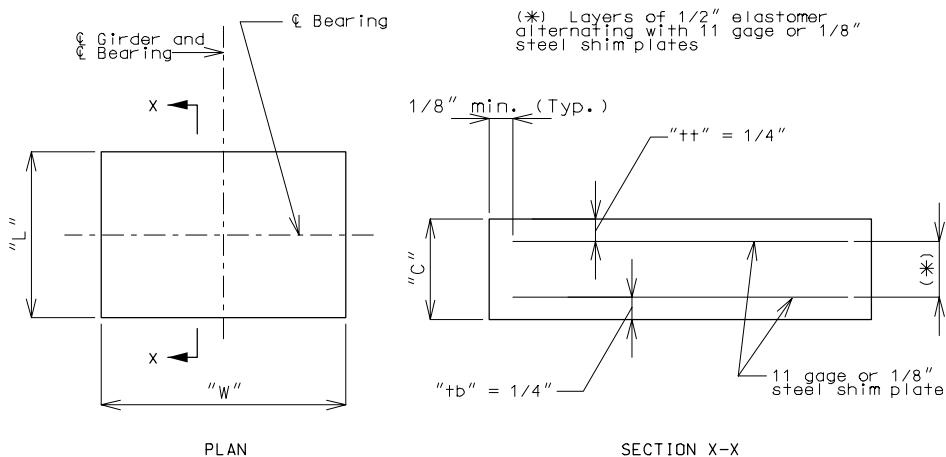
Hardness = 60 required

(*) Use 1/8" steel shim plates between layers of elastomer

(**) Not less than: $T_{min} = 2\Delta$ (AASHTO Article 14.6.6.3.4)
 $C_{max} = 6-1/4"$ FOR P/S
FOR C GREATER THAN 6-1/4" USE PTFE

**STANDARD ELASTOMERIC BEARING PAD DETAILS
FOR P/S GIRDERS (CONT.)**

Elastomeric Bearing Pads



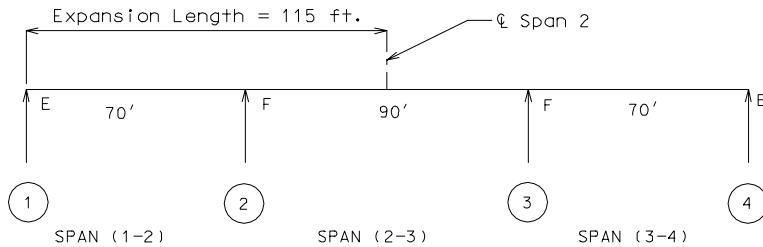
DETAILS OF LAMINATED ELASTOMERIC BEARINGS FOR P/S STRUCTURES

**LAMINATED ELASTOMERIC BEARINGS
FOR P/S GIRDERS**

Elastomeric Bearing Pads

DESIGN EXAMPLE

Note: Use the standard bearings if possible. Bearings shall be designed only for special cases.



EXPANSION BEARINGS AT BENTS #1 & #4

Type 6 P/S I-Girder, Bottom Flange = 24"

SERVICE LOAD REACTIONS:

$$DL \min = 60.00 \text{ kips (DL1 + barrier curb)}$$

$$DL \max = 67.69 \text{ kips (DL1 + barrier curb + future wearing surface)}$$

$$LL = 61.96 \text{ kips (impact not included)}$$

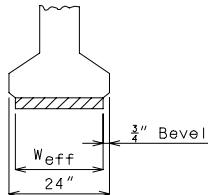
$$\Delta = (.000006) (120^\circ) (115 \times 12) (1.25) = 1.242"$$

$$\text{Min. } T = 2 \Delta = 2 \times 1.242" = 2.484" \quad \text{say } 2\frac{1}{2}"$$

$$W_{eff} = 24 - 2(3/4) = 22 \frac{1}{2}"$$

$$\text{Try } W = 16" \quad 16/3 > 2\frac{1}{2}$$

$$\text{Try } L = 11" \quad 11/3 > 2\frac{1}{2}$$



$$S = \frac{L \times W}{2t(L+W)} \quad S = \frac{11 \times 16}{2(1/2)(11+16)} = 6.5185$$

Check thickest layer only for compressive stress

$$S = \frac{11 \times 16}{2(1/4)(11+16)} = 13.0370$$

for exterior layer

$$P_{max} = GS = 6.5185(120) = 782 \text{ psi} < 1000 \text{ psi}$$

use $P = 782 \text{ psi}$

CHECK MIN. DL (should not include future wearing surface)
 $DL_{min}/LW = 60.00/11(16) = .3409 \text{ ksi} > .200 \text{ ksi} \quad -OK-$

CHECK MAX. DL

$$DL_{max} = 67.69/11(16) = .3846 < .500 \text{ ksi} \quad -OK-$$

**LAMINATED ELASTOMERIC BEARINGS
FOR P/S GIRDERS (CONT.)**

Elastomeric Bearing Pads

DESIGN EXAMPLE (CONT.)

Check max. DL + LL

$$(67.69 + 61.96) / 11(16) = .7366 < .782 \quad -\text{OK}-$$

Check Rotation

$$\sigma_{TL} \geq 0.5 GS(L/T)^2 \theta_m x$$

$\theta_m x$ (for type 6 P/S I-Girder at end bent) = 0.0059

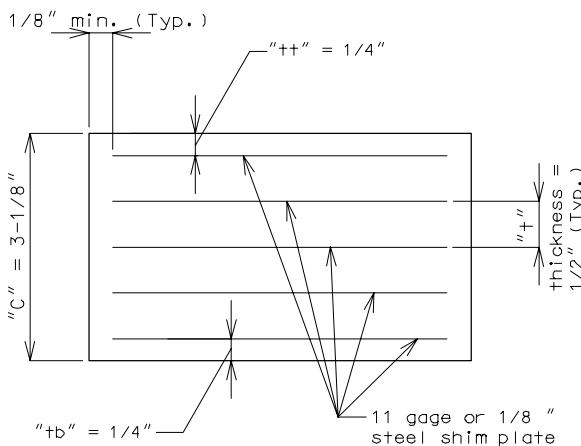
$$\sigma_{TL} \geq 0.5(0.120)(13.070)(11/2.5)^2(0.0059)$$

$$\sigma_{TL} \geq 0.0893 \text{ ksi}$$

$$0.7366 \geq 0.0893 \text{ ksi} \quad -\text{OK}-$$

$$\text{Number of Interior Layers} = \frac{T-tt+tb}{t} = \frac{2.5-0.25-0.25}{0.5} = 4$$

$$\text{Total thickness } C = 2(.25) + 4(.5) + (5 \times 1/8) = 3-1/8"$$



SECTION THRU BEARING

**STANDARD ELASTOMERIC BEARING PAD TABLES
FOR P/S I-GIRDERS**

Elastomeric Bearing Pads

Table 1

Laminated Expansion Bearings									
Bottom Flange Width	DL + LL Max kips	DL Max kips	DL Min kips	L in ①	W in ①	Shape Factor ② for "tt+tb"	Shape Factor ③ for "+"	P max ksi ④	
17	66.7	54.0	21.6	9	12	10.29	5.14	0.617	
17	98.0	70.0	28.0	10	14	11.67	5.83	0.700	
17	131.6	85.3	34.1	11	15.5	12.87	6.43	0.772	
17	151.0	93.0	37.2	12	15.5	13.53	6.76	0.812	
17	171.0	100.8	40.3	13	15.5	14.14	7.07	0.848	
17	191.5	108.5	43.4	14	15.5	14.71	7.36	0.883	
18	66.7	54.0	21.6	9	12	10.29	5.14	0.617	
18	98.0	70.0	28.0	10	14	11.67	5.83	0.700	
18	137.7	88.0	35.2	11	16	13.04	6.52	0.782	
18	165.1	99.0	39.6	12	16.5	13.89	6.95	0.834	
18	187.2	107.3	42.9	13	16.5	14.54	7.27	0.873	
18	209.9	115.5	46.2	14	16.5	15.15	7.57	0.909	
19	74.7	58.5	23.4	9	13	10.64	5.32	0.638	
19	98.0	70.0	28.0	10	14	11.67	5.83	0.700	
19	137.7	88.0	35.2	11	16	13.04	6.52	0.782	
19	179.4	105.0	42.0	12	17.5	14.24	7.12	0.854	
19	203.6	113.8	45.5	13	17.5	14.92	7.46	0.895	
19	228.7	122.5	49.0	14	17.5	15.56	7.78	0.933	
24	186.6	108.0	43.2	12	18	14.40	7.20	0.864	
24	245.8	130.0	52.0	13	20	15.76	7.88	0.945	
24	308.0	154.0	61.6	14	22	17.11	8.56	1.000	
24	337.5	168.8	67.5	15	22.5	18.00	9.00	1.000	
24	360.0	180.0	72.0	16	22.5	18.70	9.35	1.000	
24	382.5	191.3	76.5	17	22.5	19.37	9.68	1.000	
24	405.0	202.5	81.0	18	22.5	20.00	10.00	1.000	

Note: For structure with expansion bearing or non-integral bents

① Check minimum "L" $\geq 3T$ and minimum "W" $\geq 3T$

② Based on "tt+tb" = 1/4"

③ Based on "+" = 1/2"

④ Use 60 hardness for shape factor > 5.0, G = 0.120 ksi

**STANDARD ELASTOMERIC BEARING PAD TABLES
FOR P/S I-GIRDERS (CONT.)**

Elastomeric Bearing Pads

Table 2

Laminated Fixed Bearings							
Bottom Flange Width	DL + LL Max kips	DL Max kips	DL Min kips	L in ①	W in ①	Shape Factor ② for "tt+tb"	P max ksi ③
17	124.0	62.0	24.8	8	15.5	10.55	1.000
17	139.5	69.8	27.9	9	15.5	11.39	1.000
17	155.0	77.5	31.0	10	15.5	12.16	1.000
17	170.5	85.3	34.1	11	15.5	12.87	1.000
17	186.0	93.0	37.2	12	15.5	13.53	1.000
17	201.5	100.8	40.3	13	15.5	14.14	1.000
17	217.0	108.5	43.4	14	15.5	14.71	1.000
18	132.0	66.0	26.4	8	16.5	10.78	1.000
18	148.5	74.3	29.7	9	16.5	11.65	1.000
18	165.0	82.5	33.0	10	16.5	12.45	1.000
18	181.5	90.8	36.3	11	16.5	13.20	1.000
18	198.0	99.0	39.6	12	16.5	13.89	1.000
18	214.5	107.3	42.9	13	16.5	14.54	1.000
18	231.0	115.5	46.2	14	16.5	15.15	1.000
19	140.0	70.0	28.0	8	17.5	10.98	1.000
19	157.5	78.8	31.5	9	17.5	11.89	1.000
19	175.0	87.5	35.0	10	17.5	12.73	1.000
19	192.5	96.3	38.5	11	17.5	13.51	1.000
19	210.0	105.0	42.0	12	17.5	14.24	1.000
19	227.5	113.8	45.5	13	17.5	14.92	1.000
19	245.0	122.5	49.0	14	17.5	15.56	1.000
24	180.0	90.0	36.0	8	22.5	11.80	1.000
24	202.5	101.3	40.5	9	22.5	12.86	1.000
24	225.0	112.5	45.0	10	22.5	13.85	1.000
24	247.5	123.8	49.5	11	22.5	14.78	1.000
24	270.0	135.0	54.0	12	22.5	15.65	1.000
24	292.5	146.3	58.5	13	22.5	16.48	1.000
24	315.0	157.5	63.0	14	22.5	17.26	1.000
24	337.5	168.8	67.5	15	22.5	18.00	1.000

Note: For integral intermediate bents

① Check minimum "L" $\geq 3T$ and minimum "W" $\geq 3T$

② Based on "tt+tb" = 1/4"

③ Use 60 hardness for shape factor > 5.0, G = 0.120 ksi

All the above bearings consist of 2 layers of 1/4" elastomer separated by a 1/8" shim.

For fixed bearings requiring more than 2 layers of 1/4" elastomer and 1 shim plate, use shape factor requirements from table 1.

**STANDARD ELASTOMERIC BEARING PAD TABLES
FOR P/S I-GIRDERS (CONT.)**

Elastomeric Bearing Pads

Table 3

Plain Fixed Bearings							
Bottom Flange Width	DL + LL Max kips	DL Max kips	DL Min kips	L in	W in	Shape Factor ① for "+"	P max ksi ②
17	86.1	54.0	21.6	9	12	5.14	0.797
17	100.8	63.0	25.2	9	14	5.48	0.800
17	111.6	69.8	27.9	9	15.5	5.69	0.800
17	112.0	70.0	28.0	10	14	5.83	0.800
17	124.0	77.5	31.0	10	15.5	6.08	0.800
17	136.4	85.3	34.1	11	15.5	6.43	0.800
17	148.8	93.0	37.2	12	15.5	6.76	0.800
17	161.2	100.8	40.3	13	15.5	7.07	0.800
17	173.6	108.5	43.4	14	15.5	7.36	0.800
18	86.1	54.0	21.6	9	12	5.14	0.797
18	100.8	63.0	25.2	9	14	5.48	0.800
18	118.8	74.3	29.7	9	16.5	5.82	0.800
18	112.0	70.0	28.0	10	14	5.83	0.800
18	132.0	82.5	33.0	10	16.5	6.23	0.800
18	140.8	88.0	35.2	11	16	6.52	0.800
18	145.2	90.8	36.3	11	16.5	6.60	0.800
18	158.4	99.0	39.6	12	16.5	6.95	0.800
18	171.6	107.3	42.9	13	16.5	7.27	0.800
18	184.8	115.5	46.2	14	16.5	7.57	0.800
19	93.6	58.5	23.4	9	13	5.32	0.800
19	108.0	67.5	27.0	9	15	5.63	0.800
19	126.0	78.8	31.5	9	17.5	5.94	0.800
19	112.0	70.0	28.0	10	14	5.83	0.800
19	128.0	80.0	32.0	10	16	6.15	0.800
19	140.0	87.5	35.0	10	17.5	6.36	0.800
19	154.0	96.3	38.5	11	17.5	6.75	0.800
19	168.0	105.0	42.0	12	17.5	7.12	0.800
19	182.0	113.8	45.5	13	17.5	7.46	0.800
19	196.0	122.5	49.0	14	17.5	7.78	0.800
24	172.8	108.0	43.2	12	18	7.20	0.800
24	192.0	120.0	48.0	12	20	7.50	0.800
24	216.0	135.0	54.0	12	22.5	7.83	0.800
24	208.0	130.0	52.0	13	20	7.88	0.800
24	234.0	146.3	58.5	13	22.5	8.24	0.800
24	252.0	157.5	63.0	14	22.5	8.63	0.800
24	270.0	168.8	67.5	15	22.5	9.00	0.800
24	288.0	180.0	72.0	16	22.5	9.35	0.800
24	306.0	191.3	76.5	17	22.5	9.68	0.800
24	324.0	202.5	81.0	18	22.5	10.00	0.800

Note: For integral end bents, use laminated bearing when taper over 1/8" is required.

① Based on "+" = 1/2"

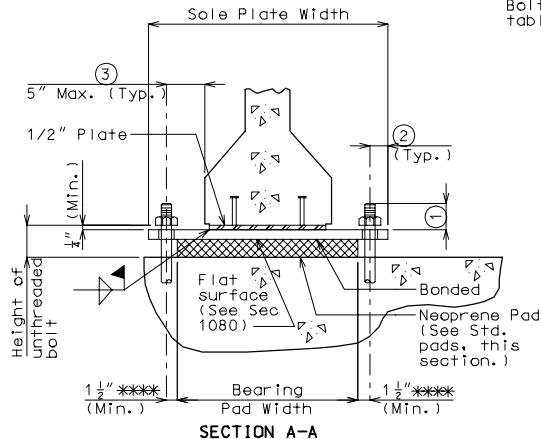
② Use 60 hardness for shape factor > 4.0. G = 0.155 ksi

Elastomeric Bearing Pads

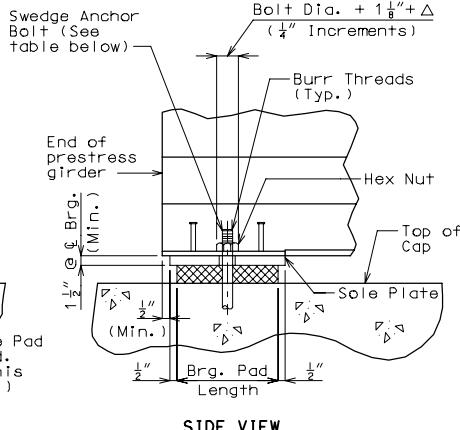
STANDARD ELASTOMERIC BEARING PAD TABLES
FOR P/S I-GIRDERS (CONT.)

Bearing details for prestressed structures
(expansion bearing)

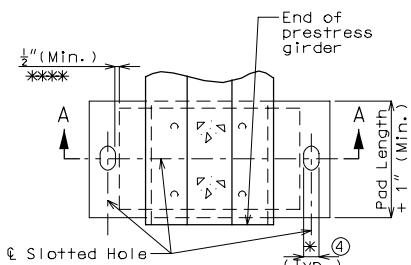
Note: The location of anchor bolts in relation to the slotted holes in the sole plate shall correspond with the temperature at the time of erection. At 60°F the slotted holes should center on the anchor bolts.



SECTION A-A



SIDE VIEW



PART PLAN VIEW

All anchor bolts shall be ASTM A709 Grade 50W Steel.

* Slot width may be increased on wide roadways to accommodate lateral expansion. See Structural Project Manager.

** For $\Delta > 2\frac{1}{2}"$, use PTFE bearings.

*** Seismic Performance Category B, C & D

Design anchor bolts for earthquake restraint. (See Sec. 6.1) Use shear blocks to limit to four anchor bolts.

**** Designer should verify that minimum dimensions are met or neoprene will melt and flow into hole during manufacturing of bearing.

Note: Bevel sole plate to match the slope of girder to the nearest 1/8" total difference in thickness across the plate. Minimum thickness shall be 1-1/2" at centerline bearing and 1" at the edge of bearing.
(By design)

	BOLT DIAMETER		
	1 1/2"	2"	2 1/2"
(1)	2 1/4"	2 1/2"	3"
(2)	2 1/4"(Min.)	3"(Min.)	3 3/4"(Min.)
(3) ****	2"(Min.)	2 5/8"(Min.)	2 5/8"(Min.)
(4)	1 5/8"	2 1/8"	2 5/8"

Chart based on level bearing pad and 1-1/2" sole plate at Ⓛ bearing

BOLT DIAM.	MAX. DEAD LOAD REACTION SEISMIC PERFORMANCE CATEGORY A (***)			
	TOTAL TEMPERATURE MOVEMENT, Δ (***)	1 1/2"	2"	2 1/2"
1 1/2"	70 kips	60 kips	47 kips	39 kips
2"	167 kips	143 kips	112 kips	92 kips
2 1/2"	326 kips	281 kips	220 kips	180 kips

Seismic Performance Category A

Note: When Service Load Design is used the allowable anchor bolt bending stress ($0.55 F_y$) is permitted to increase by 50%. Use shear blocks if necessary to limit to two anchor bolts. The above chart is based on a transverse force of $0.2(DL)$ and a longitudinal force of zero.

**STANDARD ELASTOMERIC BEARING PAD DETAILS
FOR STEEL GIRDERS**

Elastomeric Bearing Pads

Fixed Bearings - Laminated pad (*)

Thickness - Use $t = 1/2"$ and $tt\&tb = 1/4"$

Try a total elastomer thickness equal to a value and check rotation requirements.

Try to minimize total elastomer thickness

$$C = T + [1/8" \times (\# \text{layers} - 1)]$$

Where #layers = $(Tx2) + 1$

Length and Width - Use length and width shown in tables 1 and 2
Table 1 will produce smallest beam cap

Hardness - Use 60 hardness

Expansion Bearings - Laminated pad (*)

Length and Width - Use length and width shown in tables 1 and 2
Table 1 will produce smallest beam cap

Thickness - Laminated Pads (*)						
Δ (in.)	t (in.)	$tt\&tb$ (in.) (eq.)	T (in.) (**)	Layers t Elast.	Layers $tt\&tb$ Elast.	C (in.)
1/2	1/2	1/4	1	1	2	1-1/4
3/4	1/2	1/4	1-1/2	2	2	1-7/8
1	1/2	1/4	2	3	2	2-1/2
1-1/4	1/2	1/4	2-1/2	4	2	3-1/8
1-1/2	1/2	1/4	3	5	2	3-3/4
1-3/4	1/2	1/4	3-1/2	6	2	4-3/8
2	1/2	1/4	4	7	2	5
2-1/4	1/2	1/4	4-1/2	8	2	5-5/8
2-1/2	1/2	1/4	5	9	2	6-1/4

Δ = Total temperature movement

t = Thickness of middle layers of elastomer

$tt\&tb$ = Thickness of top and bottom layers of elastomer

T = Total effective thickness of elastomer (sum of t and $tt\&tb$)

C = Total thickness including steel shims

Cmax = 6-1/4" for steel girders (for C greater than 6-1/4" use PTFE for steel girders)

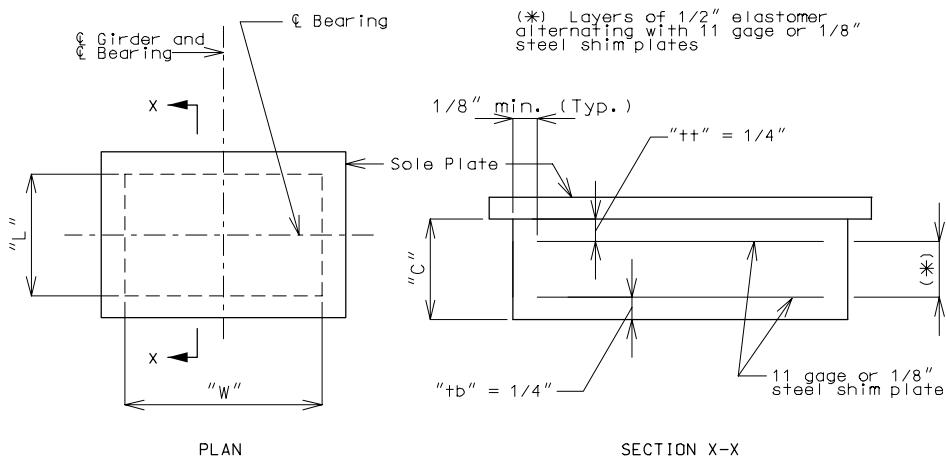
Hardness = 60 required

(*) Use 1/8" steel shim plates between layers of elastomer

(**) Not greater than: Tmax or less than Tmin for pad size shown in table 1 or 2.

**STANDARD ELASTOMERIC BEARING PAD DETAILS
FOR STEEL GIRDERS (CONT.)**

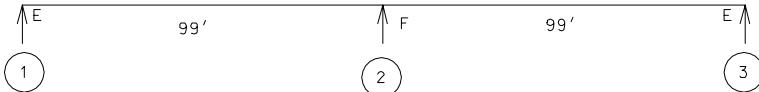
Elastomeric Bearing Pads



DETAILS OF LAMINATED ELASTOMERIC BEARINGS FOR STEEL STRUCTURES

STANDARD ELASTOMERIC BEARING PAD DESIGN EXAMPLE
FOR STEEL GIRDERSDESIGN EXAMPLE

Structure (99'-99') Continuous Composite Plate Girder - 48" Web

Fixed Bearing at Bent #2

Given: Bottom flange width = 15"

Service Loads: DLmin = 155.0 kips (DL1 + Barrier Curb)

DLmax = 170.4 kips (DL1 + Barrier Curb + FWS)

LL = 165.3 kips (impact not included)

DLmax + LL = 335.7 kips

From Table 1 (use first)

For DL + LL = 335.7: try L = 15 and W = 24

DL + LL = 360.0 > 335.7 -OK-

DLmax = 170.4 < 180.0 -OK-

DLmin = 155.0 kips > 72.0 kips

Bmin = 17 > 15 -NG-

From Table 2

For DL + LL = 335.7: try L = 24 and W = 15

Bmin = 9 < 15 -OK-

Try T = 2.0"

Check Rotation

$$\sigma_{TL} \geq 0.5 GS (L/T)^2 Bm, x$$

$$S = 18.46 \text{ (use shape factor for exterior layer)}$$

$$Bm, x = 0.0018 (48" \text{ Web interior bent})$$

$$\sigma_{TL} \geq 0.5(0.120)(18.46)(24/2)^2 0.0018$$

$$\sigma_{TL} \geq 0.287 \text{ ksi}$$

$$\frac{335.7}{24(15)} = 0.9325 \text{ ksi} \geq 0.287 \text{ ksi -OK-}$$

Use L = 24", W = 15", T = 2.0"

#Layer of elastomer = (2" x 2) + 1 = 5

$$C = 2.0 + [1/8 \times (5-1)] = 2-1/2"$$

Expansion Bearings at Bents #1 and #3

Given: Bottom flange width = 12"

Service Loads: DLmax = 39.0 kips

DLmin = 32.0 kips

LL = 58.2 kips

DLmax + LL = 97.2 kips

$$\Delta = (6.5 \times 10^{-6})(140)(99)(12)(1.25) = 1.35" = 1-1/2"$$

From Thickness Table, Bridge Manual Section 3.31-2.5-1
for $\Delta = 1.50"$, T = 3", C = 3-3/4"

Elastomeric Bearing Pads

STANDARD ELASTOMERIC BEARING PAD DESIGN EXAMPLE
FOR STEEL STRUCTURES (CONT.)

From Table 1 for steel girders, Bridge Manual Section 3.31-2.7-1

For $DL + LL = 97.2$: try $L = 10$ and $W = 14$

$B_{min} = 9 < 12$ " -OK-

$DL_{max} = 70.0 > 39.0$ -OK-

$DL_{min} = 28.0 < 32.0$ -OK-

$T_{max} = 3$ " < 5" -OK-

Check Rotation

$$\sigma_{TL} \geq 0.5 GS (L/T)^2 \theta_m, x$$

$$S = 11.67$$

$$\theta_m, x = 0.0080 \text{ (48" Web interior bent)}$$

$$\sigma_{TL} \geq 0.5(0.120)(11.67)(10/3)^2 0.0080$$

$$\sigma_{TL} \geq 0.0622 \text{ ksi}$$

$$\frac{97.2}{10(14)} = 0.694 \text{ ksi} \geq 0.0622 \text{ ksi -OK-}$$

Sole Plate Designs

Bent #2 - fixed bearing

Use 1-1/2" min. thickness at centerline on fixed bearing.

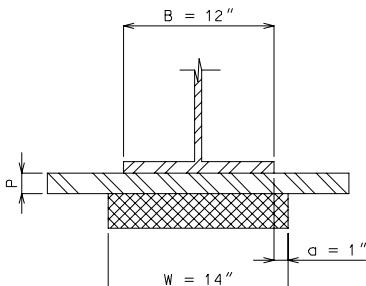
Bents #1 and #3 - expansion bearing

$$a = (W-B)/2 = (14-12)/2 = 1"$$

$$R = (DL+LL)(a/W) = 97.2(1/14) \\ = 6.94 \text{ kips}$$

$$Ma = R \times a/2 = 6.94(1/2) \\ = 3.47 \text{ in-k}$$

$$\text{Since: } f_s = Mc/I \\ c = P/2 \\ I = L \times P^3/12$$



for A36 steel
 $f_s = 20 \text{ ksi}$

$$\text{Then } P = \sqrt{\frac{Ma \times 12}{2 \times L \times f_s}} =$$

$$P = \sqrt{\frac{3.47 \times 12}{2 \times 10 \times 20}} = .3227 < 1.5$$

Use $P = 1-1/2"$ min.

STANDARD ELASTOMERIC BEARING PAD TABLES FOR STEEL GIRDERS

TABLE 1

Elastomeric Bearing Pads

L in	W in	Bmin	Tmax	t in	tt-tb in	Δ max	DL + LL max	DL max	DL min	Shape Factor for "t"	Shape Factor for "tt-tb"	Pmax ksi
9	12	9	3.0	0.5	0.25	1.50	66.7	54.0	21.6	5.14	10.29	0.617
10	14	9	3.0	0.5	0.25	1.50	98.0	70.0	28.0	5.83	11.67	0.700
11	16	9	3.5	0.5	0.25	1.75	137.7	88.0	35.2	6.52	13.04	0.782
12	18	11	4.0	0.5	0.25	2.00	186.6	108.0	43.2	7.20	14.40	0.864
13	20	13	4.0	0.5	0.25	2.00	245.8	130.0	52.0	7.88	15.76	0.945
14	22	15	4.5	0.5	0.25	2.25	308.0	154.0	61.6	8.56	17.11	1.000
15	24	17	5.0	0.5	0.25	2.50	360.0	180.0	72.0	9.23	18.46	1.000
16	26	19	5.0	0.5	0.25	2.50	416.0	208.0	83.2	9.90	19.81	1.000
17	28	21	5.0	0.5	0.25	2.50	476.0	238.0	95.2	10.58	21.16	1.000
18	30	23	5.0	0.5	0.25	2.50	540.0	270.0	108.0	11.25	22.50	1.000
20	34	27	5.0	0.5	0.25	2.50	680.0	340.0	136.0	12.59	25.19	1.000

T = Total effective elastomer thickness (sum of "t"'s and "tt-tb"'s)

Δ = Total temperature movement

B = Bottom flange width

Use 60 Hardness, G = 0.120 ksi

Bmin = W-2(3.5), minimum = 9"

Tmax = The minimum of L/3 rounded to the lowest 1/2" and
W/3 rounded to the lowest 1/2".
When Tmax > 5.0", use PTFE bearings

STANDARD ELASTOMERIC BEARING PAD TABLES FOR STEEL GIRDERS (CONT.)

TABLE 2

W in	L in	Bmin	Tmax	+ in	tt+tb in	Δ max	DL + LL max	DL max	DL min	Shape Factor for "+"	Shape Factor for "tt+tb"	Pmax ksi
9	12	9.0	3.0	0.5	0.25	1.50	66.7	54.0	21.6	5.14	10.29	0.617
10	14	10.0	3.0	0.5	0.25	1.50	98.0	70.0	28.0	5.83	11.67	0.700
11	16	11.0	3.0	0.5	0.25	1.75	137.7	88.0	35.2	6.52	13.04	0.782
12	18	12.0	4.0	0.5	0.25	2.00	186.6	108.0	43.2	7.20	14.40	0.864
13	20	13.0	4.0	0.5	0.25	2.00	245.8	130.0	52.0	7.88	15.76	0.945
14	22	14.0	4.5	0.5	0.25	2.25	308.0	154.0	61.6	8.56	17.11	1.000
15	24	15.0	5.0	0.5	0.25	2.50	360.0	180.0	72.0	9.23	18.46	1.000
16	26	16.0	5.0	0.5	0.25	2.50	416.0	208.0	83.2	9.90	19.81	1.000
17	28	17.0	5.0	0.5	0.25	2.50	476.0	238.0	95.2	10.58	21.16	1.000
18	30	18.0	5.0	0.5	0.25	2.50	540.0	270.0	108.0	11.25	22.50	1.000
20	34	13	5.0	0.5	0.25	2.50	680.0	340.0	136.0	12.59	25.19	1.000

T = Total effective elastomer thickness (sum of "+"s and "tt+tb"s)

Δ = Total temperature movement

B = Bottom flange width

Use 60 Hardness, G = 0.120 ksi

Bmin = W-2(3.5), minimum = 9"

Tmax = The minimum of L/3 rounded to the lowest 1/2" and
W/3 rounded to the lowest 1/2".
When Tmax > 5.0", use PTFE bearings

Bridge Manual

Bearings - Section 3.31

Page: 2.7-3

Elastomeric Bearing Pads

STANDARD ELASTOMERIC BEARING PAD TABLES FOR STEEL GIRDERS (CONT.)

(Integral end bents)

(PLAIN FIXED BEARINGS)

"W" (Width) (in)	"L" (Length) (in)	"T" (Thk.) (in)	DL+LL max (Kips)	DL max (Kips)	DL min (Kips)	"S" (Shape Factor)	Pmax kip
10	10	0.5	77.5	50.0	20.0	5.0	0.775
10	12	0.5	96.0	60.0	24.0	5.5	0.800
10	14	0.5	112.0	70.0	28.0	5.8	0.800
11	10	0.5	88.0	55.0	22.0	5.2	0.800
11	12	0.5	105.6	66.0	26.4	5.7	0.800
11	14	0.5	123.2	77.0	30.8	6.2	0.800
12	12	0.5	115.2	72.0	28.8	6.0	0.800
12	14	0.5	134.4	84.0	33.6	6.5	0.800
12	16	0.5	153.6	96.0	38.4	6.9	0.800
13	12	0.5	124.8	78.0	31.2	6.2	0.800
13	14	0.5	145.6	91.0	36.4	6.7	0.800
13	16	0.5	166.4	104.0	41.6	7.2	0.800
14	12	0.5	134.4	84.0	33.6	6.5	0.800
14	14	0.5	156.8	98.0	39.2	7.0	0.800
14	16	0.5	179.2	112.0	44.8	7.5	0.800
15	14	0.5	168.0	105.0	42.0	7.2	0.800
15	16	0.5	192.0	120.0	48.0	7.7	0.800
15	18	0.5	216.0	135.0	54.0	8.2	0.800
16	14	0.5	179.2	112.0	44.8	7.5	0.800
16	16	0.5	204.8	128.0	51.2	8.0	0.800
16	18	0.5	230.4	144.0	57.6	8.5	0.800
17	14	0.5	190.4	119.0	47.6	7.7	0.800
17	16	0.5	217.6	136.0	54.4	8.2	0.800
17	18	0.5	244.8	153.0	61.2	8.7	0.800
18	16	0.5	230.4	144.0	57.6	8.5	0.800
18	18	0.5	259.2	162.0	64.8	9.0	0.800
18	20	0.5	288.0	180.0	72.0	9.5	0.800
19	16	0.5	243.2	152.0	60.8	8.7	0.800
19	18	0.5	273.6	171.0	68.4	9.2	0.800
19	20	0.5	304.0	190.0	76.0	9.7	0.800
20	18	0.5	288.0	180.0	72.0	9.5	0.800
20	20	0.5	320.0	200.0	80.0	10.0	0.800
20	22	0.5	352.0	220.0	88.0	10.5	0.800

Do not use sole plate.

Impact not included in live load.

Use laminated bearings consisting of two 0.25" layers of elastomer and one beveled plate when taper greater than 1/8" of the bearing is required.

Bearing pad width shall extend to within 1" from the edge of the bottom flange and not extend beyond the edge of the bottom flange.

Use 60 hardness.

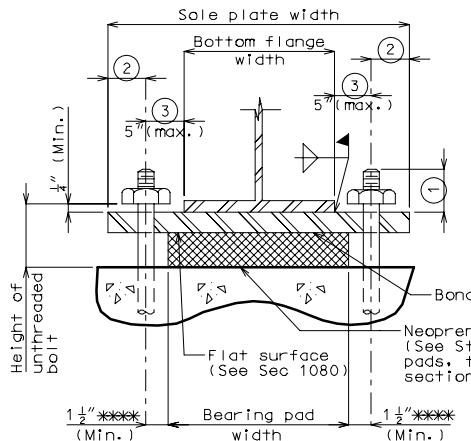
Use girder chairs instead of widening beam.

Elastomeric Bearing Pads

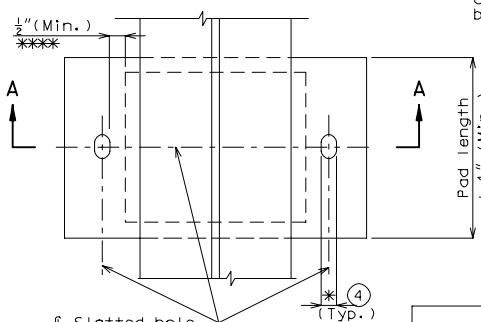
ELASTOMERIC BEARING DETAILS FOR STEEL STRUCTURES

(Expansion bearing)

Note: The location of anchor bolts in relation to the slotted holes in the sole plate shall correspond with the temperature at the time of erection. At 60°F the slotted holes should center on the anchor bolts.



SECTION A-A



PART PLAN VIEW

All anchor bolts shall be ASTM A709 grade 50W steel.

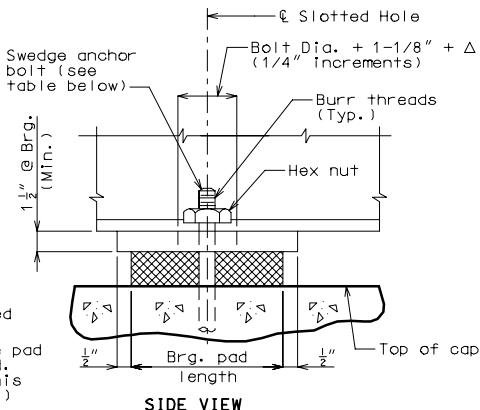
* Slot width may be increased on wide roadways to accommodate lateral expansion. See Structural Project Manager.

** For $\Delta > 2\frac{1}{2}"$, use PTFE bearings.

***** Seismic Performance Category B, C & D**

Design anchor bolts for earthquake restraint. (See Sec. 6.1) Use shear blocks to limit to four anchor bolts.

**** Designer should verify that minimum dimensions are met or neoprene will melt and flow into hole during manufacturing of bearing.



SIDE VIEW

Note: Bevel sole plate to match the slope of girder to the nearest 1/8" total difference in thickness across the plate. Minimum thickness shall be 1-1/2" at centerline bearing and 1" at the edge of bearing. (by design)

Bolt Diameter		
1 1/2"	2"	2 1/2"
2 1/4"	2 1/2"	3"
2 1/2"(Min.)	3"(Min.)	3 3/4"(Min.)
3"(Min.)	2 3/8"(Min.)	2 5/8"(Min.)
4 1/2"	2 1/8"	2 5/8"

Chart based on level bearing pad and 1-1/2" sole plate at 4 Slotted Holes

BOLT DIAM.	MAX. DEAD LOAD REACTION SEISMIC PERFORMANCE CATEGORY A (***)			
	1 1/4"	1 1/2"	2"	2 1/2"
1 1/2"	70 Kips	60 Kips	47 Kips	39 Kips
2"	167 Kips	143 Kips	112 Kips	92 Kips
2 1/2"	326 Kips	281 Kips	220 Kips	180 Kips

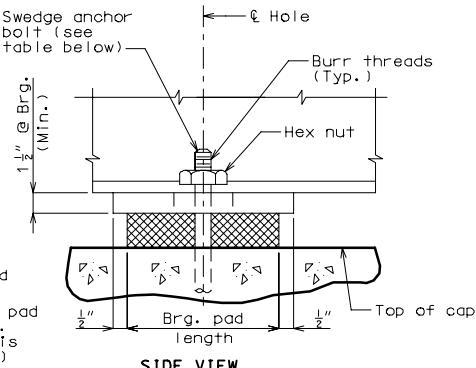
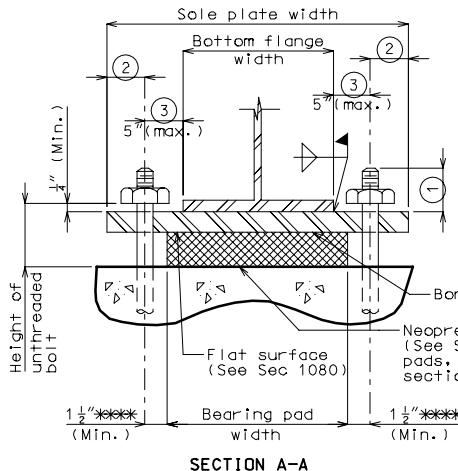
Seismic Performance Category A

Note: When service load design is used the allowable anchor bolt bending stress (0.55 Fy) is permitted to increase by 50 percent. Use shear blocks if necessary to limit to two anchor bolts. The above chart is based on a transverse force of 0.2(DL) and a longitudinal force of zero.

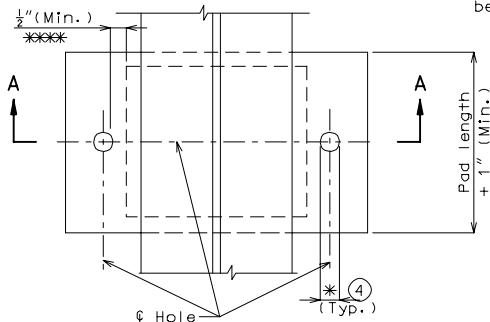
Elastomeric Bearing Pads

ELASTOMERIC BEARING DETAILS FOR STEEL STRUCTURES

(Fixed bearing)



Note: Bevel sole plate to match the slope of girder to the nearest $\frac{1}{8}$ " total difference in thickness across the plate. Minimum thickness shall be $1\frac{1}{2}$ " at centerline bearing and $1\frac{1}{4}$ " at the edge of bearing. (by design)



Bolt Diameter		
1 $\frac{1}{2}$ "	2"	2 $\frac{1}{2}$ "
2 $\frac{3}{4}$ "	2 $\frac{1}{2}$ "	3"
2 $\frac{1}{2}$ " (Min.)	3" (Min.)	3 $\frac{3}{4}$ " (Min.)
(3) ***	2 $\frac{3}{8}$ " (Min.)	2 $\frac{5}{8}$ " (Min.)
(4)	1 $\frac{5}{8}$ "	2 $\frac{1}{8}$ "
		2 $\frac{5}{8}$ "

Chart based on level bearing pad and $1\frac{1}{2}$ " sole plate at $\frac{1}{8}$ " bearing

Horizontal seismic force per bearing (***) Seismic Performance Category A (***)				
Bolt Diam.	Bearing Pad Height			
	1 $\frac{1}{4}$ "	1 $\frac{1}{8}$ "	2 $\frac{1}{2}$ "	3 $\frac{1}{8}$ "
1 $\frac{1}{2}$ "	27 kips	20 kips	16 kips	14 kips
2"	64 kips	49 kips	39 kips	33 kips
2 $\frac{1}{2}$ "	126 kips	96 kips	77 kips	65 kips

Seismic Performance Category A

Note: When service load design is used the allowable anchor bolt bending stress ($0.55 F_y$) is permitted to increase by 50 percent. Use shear blocks if necessary to limit to two anchor bolts.

All anchor bolts shall be ASTM A709 grade 50W steel.

* Slot width may be increased on wide roadways to accommodate lateral expansion. See Structural Project Manager.

*** Seismic Performance Category B,C & D**

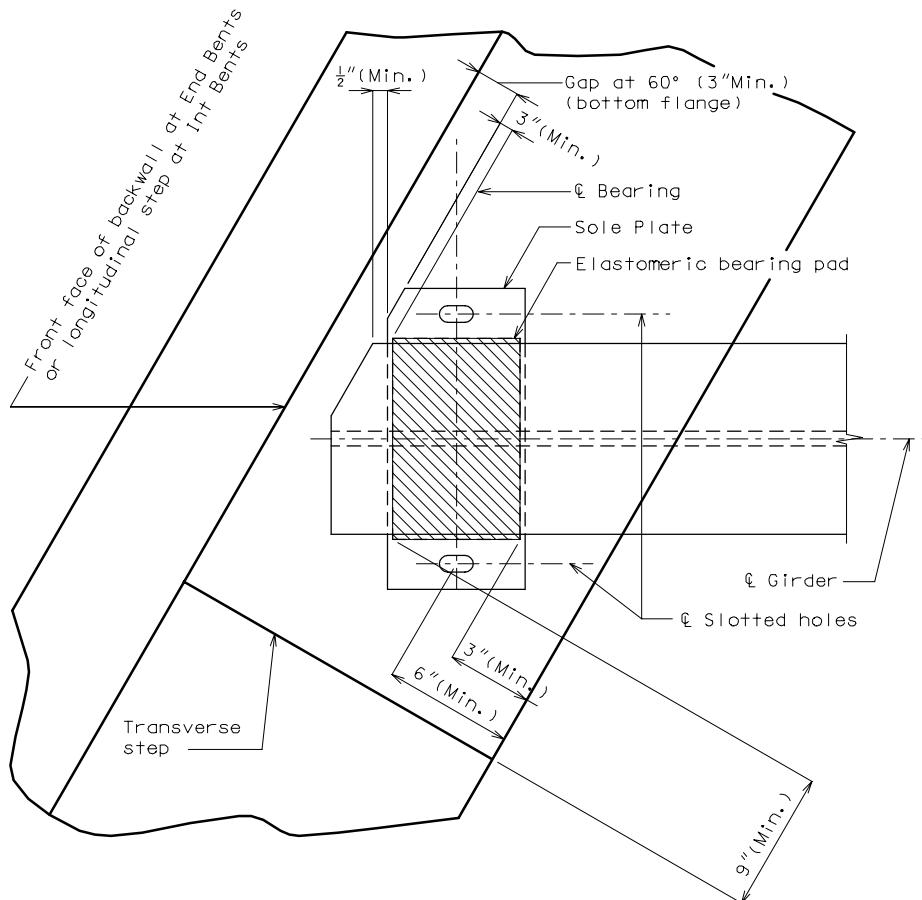
Design anchor bolts for earthquake restraint. (See Sec. 6.1) Use shear blocks to limit to four anchor bolts.

*** Designer should verify that minimum dimensions are met or neoprene will melt and flow into hole during manufacturing of bearing.

*** Horizontal seismic force per bearing = $\sqrt{[(0.20)(girder (DL) reaction)]^2 + [(0.20)(\frac{\text{segment weight}}{\text{no. of girder}})]^2}$ where segment weight is the weight of the superstructure between expansion joints when there is one fixed bent. If more than one fixed bent per segment exists, divide out segment weight appropriately.

SOLE PLATE CLIPPING DETAILS

(For steel structures)

**SECTION THRU BEARING**

Minimum edge distance shall be maintained on all holes in sole plate.

Slotted holes shown are for expansion bearings.

Round holes shall be used for fixed bearings.

SLIDING BEARING DESIGN

PTFE (Polytetrafluoroethylene) Bearings

SLIDING BEARING

PTFE sliding bearing shall consist of a lower unit and an upper unit as follows:

The lower unit shall be PTFE bonded to a 1/8" stainless steel plate then to a neoprene pad (See Design Layout).

The upper unit shall be a 1/8" highly polished stainless steel plate bonded to a steel sole plate.

DESIGN DATA:

Lower Unit - Ref. 1996 AASHTO and 1997 & 1998 Interims Section 14 and Mo. Std. Spec. 1038

Use standard bearings. Bearings shall be designed only for special cases. See Structural Project Manager.

Neoprene Elastomeric Pad -

Maximum (DL + LL) Compressive Stress = $P_{max.} = SG$
but not greater than
1000 psi max.

Maximum (DL) Compressive Stress = 500 psi
Minimum (DL) Compressive Stress = 200 psi

1. Use $G = 160 \text{ psi}$ (70 hardness)

Maximum Width (W) = Flange Width + 6" (inches)
 Minimum Width = Flange Width

Then: $(L) = \frac{DL + LL}{P_{max.}(W)}$ (inches)
 2. Rotations shall be taken as the maximum possible difference in slope between the top and bottom surfaces of the bearing caused by the initial lack of parallelism and the girder end rotation due to imposed loads and movements. The following equation must be satisfied to ensure that uplift does not occur under any combination of loads and corresponding rotations:

$\sigma_{TL} \geq 0.5 \text{ GS } (L/T)^2 \text{ } \theta m_x$ (AASHTO Article 14.6.6.3.5-1)

T = Pad thickness (elastomer only)

θ_m, x = Maximum rotation due to initial lack of parallelism and the girder end rotation due to dead loads and live loads. Designer should check the rotation requirement of the bearing for a specific girder, bearing size and bent type to verify elastomer thickness in the bearing tables are adequate.

(Refer to page 2.1-3 of this section for table of B_m, x)
Note: Table does not include rotations due to initial lack of parallelism and camber.

For neoprene elastomeric pad design use laminated fixed bearing criteria.

$$S = \frac{LW}{2 + (L + W)}$$

- + = The thickness of each individual layer of elastomer. Standard thickness for all layers is 1/2" for the neoprene pads. Use 1/8" steel plate between layers of the elastomer.

SLIDING BEARING DESIGN (CONT.)

3. Use PTFE thickness of 1/16" (-0 + 1/16") (AASHTO Article 14.6.2.3.1) length and width same as pad.

Note: Bond PTFE to the 1/8" stainless steel plate which will in turn be vulcanized to the neoprene pad.

UPPER UNIT

1. Stainless Steel Plate (1/8" thick)

Plate Length = pad length + Δ + 1-1/2" (1/2" increments)

Where Δ = Total temperature movement
(Steel) = (.0000065)(140)(expansion length) (Φ)

Φ = 1.00 @ Int. Bent and Semi-Deep Abut.

Φ = 1.25 @ End Bent (Additional safety factor due to earth pressure)

Plate width = Pad width + 1"

2. Sole Plate (*) Thickness = 1-1/2" minimum @ & Brg.
(1" absolute minimum at edge)

Sole Plate Length = Stainless steel plate length + 1".

Sole Plate Width = Beam flange width + 8-1/2" minimum or
flange width + 17-1/2" maximum or
Pad width + 11-1/2".

(*) Use A-36 steel.

Note: 70 Durometer hardness is to be used for sliding bearings.

PTFE (Polytetrafluoroethylene) Bearings

SLIDING BEARING TABLES

Neoprene Elastomer Pads
Sliding Bearings:

Table 1

Bearing Pad		Type "N" Neoprene Elastomeric		Bottom flange width in.	LENGTH X WIDTH			S Shape Factor	Pmax ksi
Length in.	Width in.	Thickness in. ①	No. of Shim Plates ②		DL+LL max. kips	DL max. kips	DL min. kips		
9	12	1.125	1	9	88.9	54.0	21.6	5.14	0.823
10	14	1.125	1	9	130.7	70.0	28.0	5.83	0.933
11	16	1.125	1	10	176.0	88.0	35.2	6.52	1.000
12	18	1.125	1	12	216.0	108.0	43.2	7.20	1.000
13	20	1.750	2	14	260.0	130.0	52.0	7.88	1.000
14	22	1.750	2	16	308.0	154.0	61.6	8.56	1.000
15	24	1.750	2	18	360.0	180.0	72.0	9.23	1.000
16	26	1.750	2	20	416.0	208.0	83.2	9.90	1.000
17	28	1.750	2	22	476.0	238.0	95.2	10.58	1.000
18	30	1.750	2	24	540.0	270.0	108.0	11.25	1.000
19	32	2.375	3	26	608.0	304.0	121.6	11.92	1.000
20	34	2.375	3	28	680.0	340.0	136.0	12.59	1.000
21	36	2.375	3	30	756.0	378.0	151.2	13.26	1.000

Neoprene Elastomer Pads
Sliding Bearings:

Table 2

Bearing Pad		Type "N" Neoprene Elastomeric		Bottom flange width in.	LENGTH X WIDTH			S Shape Factor	Pmax ksi
Width in.	Length in.	Thickness in. ①	No. of Shim Plates ②		DL+LL max. kips	DL max. kips	DL min. kips		
9	12	1.125	1	9	88.9	54.0	21.6	5.14	0.823
10	14	1.125	1	9	130.7	70.0	28.0	5.83	0.933
11	16	1.125	1	9	176.0	88.0	35.2	6.52	1.000
12	18	1.125	1	9	216.0	108.0	43.2	7.20	1.000
13	20	1.750	2	9	260.0	130.0	52.0	7.88	1.000
14	22	1.750	2	9	308.0	154.0	61.6	8.56	1.000
15	24	1.750	2	9	360.0	180.0	72.0	9.23	1.000
16	26	1.750	2	10	416.0	208.0	83.2	9.90	1.000
17	28	1.750	2	11	476.0	238.0	95.2	10.58	1.000
18	30	1.750	2	12	540.0	270.0	108.0	11.25	1.000
19	32	2.375	3	13	608.0	304.0	121.6	11.92	1.000
20	34	2.375	3	14	680.0	340.0	136.0	12.59	1.000
21	36	2.375	3	15	756.0	378.0	151.2	13.26	1.000

① The pad thickness includes thickness of shim plates.

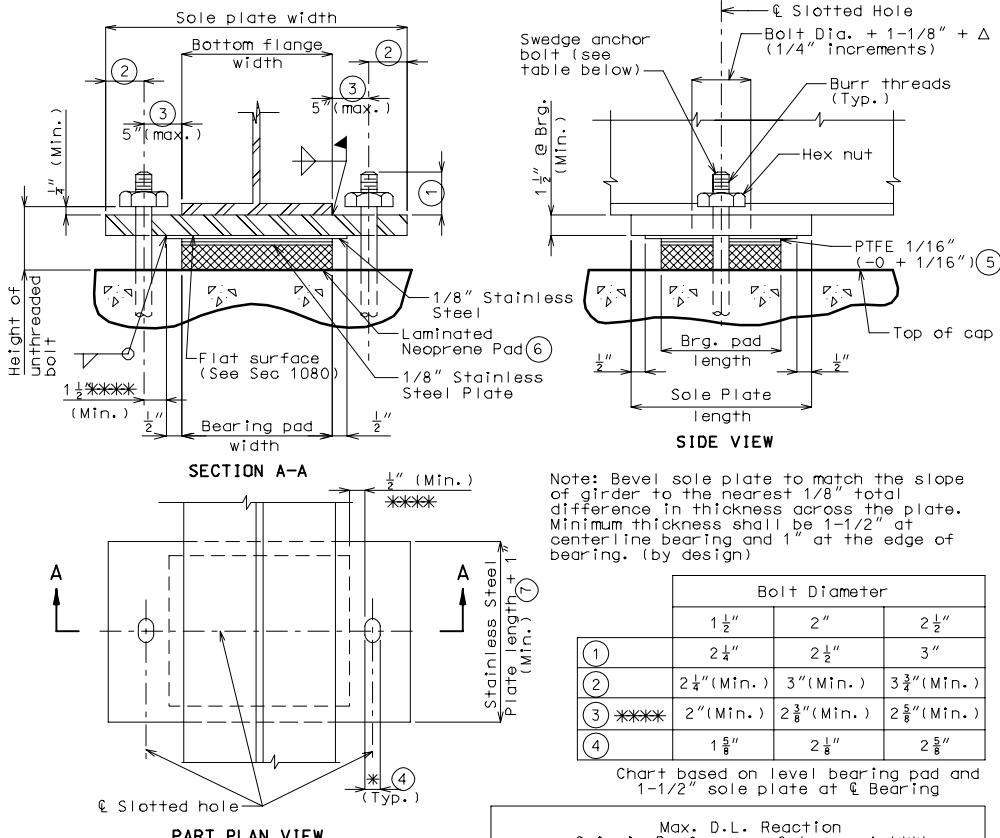
② Locate the 1/8" shim plates between the equal layer layers of 1/2" elastomer.

③ The rotation requirements must be checked for PTFE bearings at end bents for these bearing sizes.

SLIDING BEARING DETAILS

PTFE (Polytetrafluoroethylene) Bearings

Note: The location of anchor bolts in relation to the slotted holes in the sole plate shall correspond with the temperature at the time of erection. At 60°F the slotted holes should center on the anchor bolts.



Note: Bevel sole plate to match the slope of girder to the nearest 1/8" total difference in thickness across the plate. Minimum thickness shall be 1-1/2" at centerline bearing and 1" at the edge of bearing. (by design)

Chart based on level bearing pad and 1-1/2" sole plate at 1/2" Bearing				
Max. D.L. Reaction Seismic Performance Category A (**)				
Bolt Diam.	Bearing Pad Height			
	1 1/8"	1 3/4"	2 3/8"	3"
1 1/2"	125 kips	97 kips	79 kips	67 kips
2"	296 kips	230 kips	188 kips	159 kips
2 1/2"	578 kips	449 kips	368 kips	311 kips

Seismic Performance Category A					
Note: When service load design is used the allowable anchor bolt bending stress (0.55 FY) is permitted to increase by 50 percent. Use shear blocks if necessary to limit to two anchor bolts.					

** Seismic Performance Category B,C & D

Design anchor bolts for earthquake restraint. (See example Sec. 1.2)
Use shear blocks to limit to four anchor bolts.

All anchor bolts shall be ASTM A709 grade 50W steel.

- (5) Bond PTFE to the 1/8" stainless steel plate then bond to the neoprene pad.
- (6) Bond to the brg. seat with approved approved epoxy adhesive.
- (7) For Stainless Steel Plate length, see page 3.1-2.

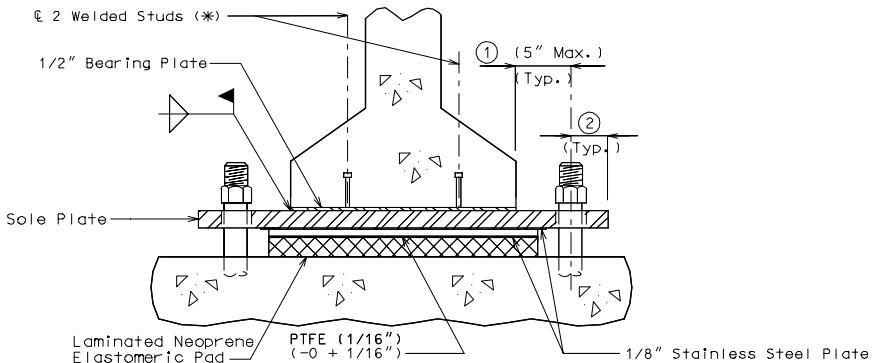
* Slot width may be increased on wide roadways to accommodate lateral expansion. See Structural Project Manager.

**** Designer should verify that minimum dimensions are met or neoprene will melt and flow into the hole during manufacturing of bearing.

PTFE (Polytetrafluoroethylene) Bearings

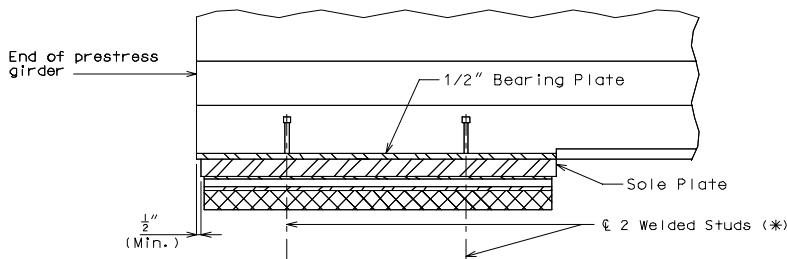
SLIDING PLATE DETAILS (CONT.)

Details of the sole plate connection to the prestress girder

**SECTION THRU GIRDER**

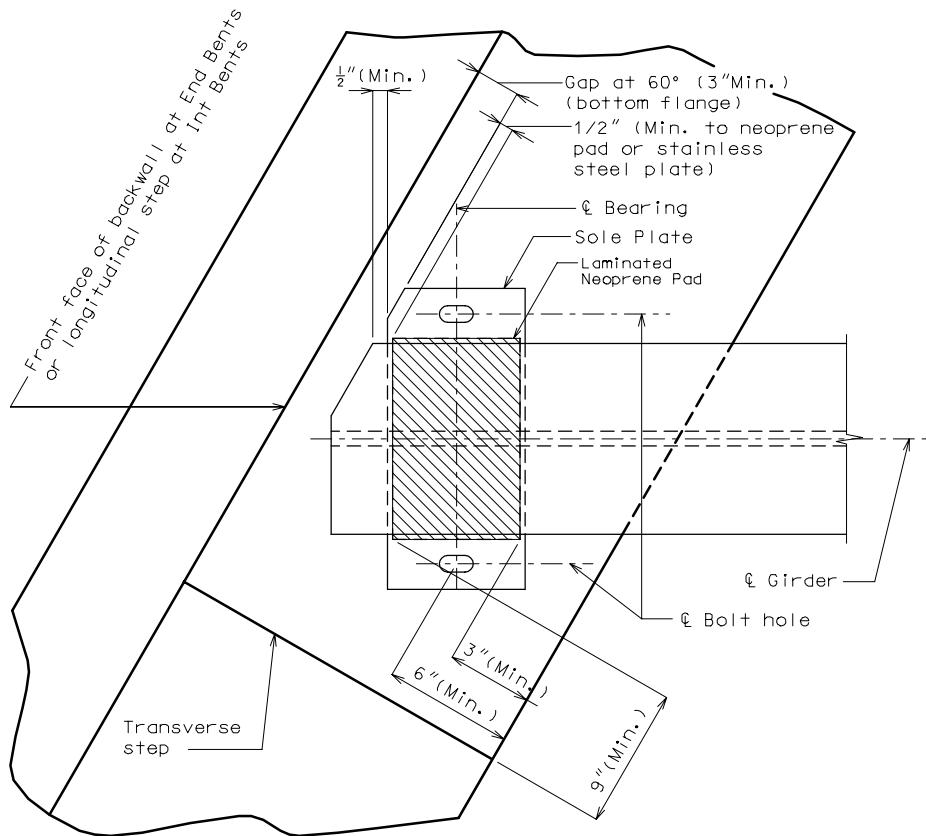
- (1) 2" Min. for a $1\frac{1}{2}$ " Ø anchor bolt
 $2\frac{1}{8}$ " Min. for a 2" Ø anchor bolt
 $2\frac{5}{8}$ " Min. for a $2\frac{1}{2}$ " Ø anchor bolt

- (2) $2\frac{1}{4}$ " Min. for a $1\frac{1}{2}$ " Ø anchor bolt
3" Min. for a 2" Ø anchor bolt
 $3\frac{1}{4}$ " Min. for a $2\frac{1}{2}$ " Ø anchor bolt

**SECTION AT END OF GIRDER**

(*) See Section 3.55 - 1.14.2 for details of 1/2" bearing plate.

Note:
For PTFE bearing details and notes not shown, see preceding pages.

SLIDING BEARING CLIPPING DETAILS**SECTION THRU BEARING**

Minimum edge distance shall be maintained on all holes in sole plate.

Slotted holes shown are for PTFE expansion bearings.

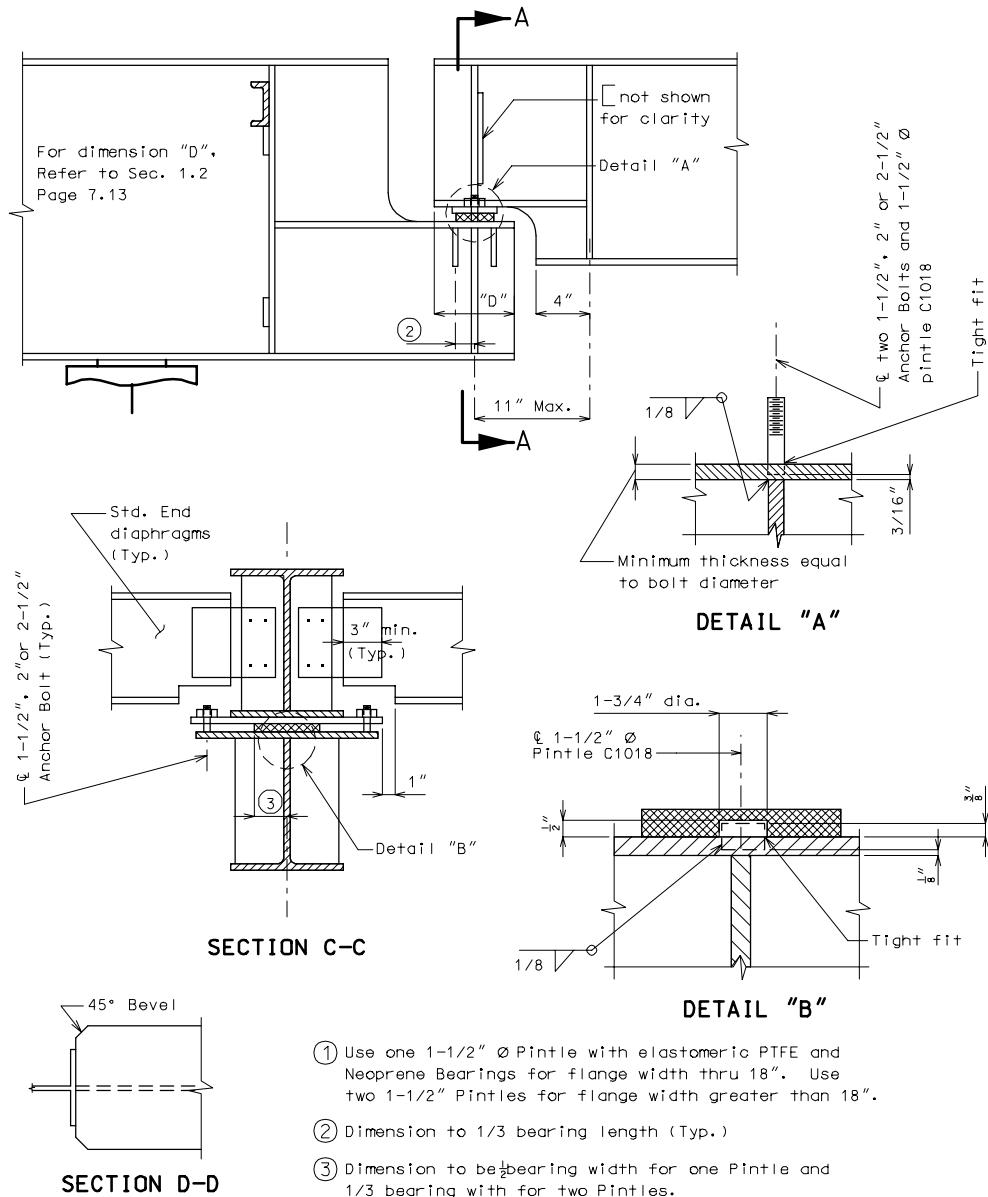
Round holes shall be used for PTFE fixed bearings.

PTFE (Polytetrafluoroethylene) Bearings

HINGED CONNECTION DETAILS

Neoprene and PTFE Bearings

Note: For details of Hinged Connection not shown, See Manual Section 3.30.



BEARING EDGE DISTANCE

Steel or Prestress Girders

Beam Ledges

Beam Ledges are discussed in (AASHTO Article 8.16.6.8.7 (1992)), (AASHTO Article 5.13.2.5 (1994)) See PCA publication "Notes on ACI 318-89" section 17.

Heavy loads placed near the edge of a concrete surface can produce spalling. Two precautions should be taken to avoid the problem. Additional reinforcement should be placed under the load and around the corner. The bearing area of the load should not project beyond the straight portion of the stirrups, nor beyond the interior face of a transverse anchor bar (if one is provided). See Figure 3.31.4.1-1. The recommended distance to a step, or the end of the bent cap in the transverse direction is 9 inches.

Bearing Clearance

When beams are placed end to end at an intermediate bent, the clearance is governed by the bent up strands, diaphragm reinforcement, skew, and any vertical or horizontal curvature in the profile grade. A 9 inch minimum between bearing pads for prestress is a general rule. For simply supported steel or constant depth girders the recommended minimum clearance is 2 inches between bearing pads. See Dimension "C". Also consider transverse girder offsets when using prestress girders on horizontally curved alignments.

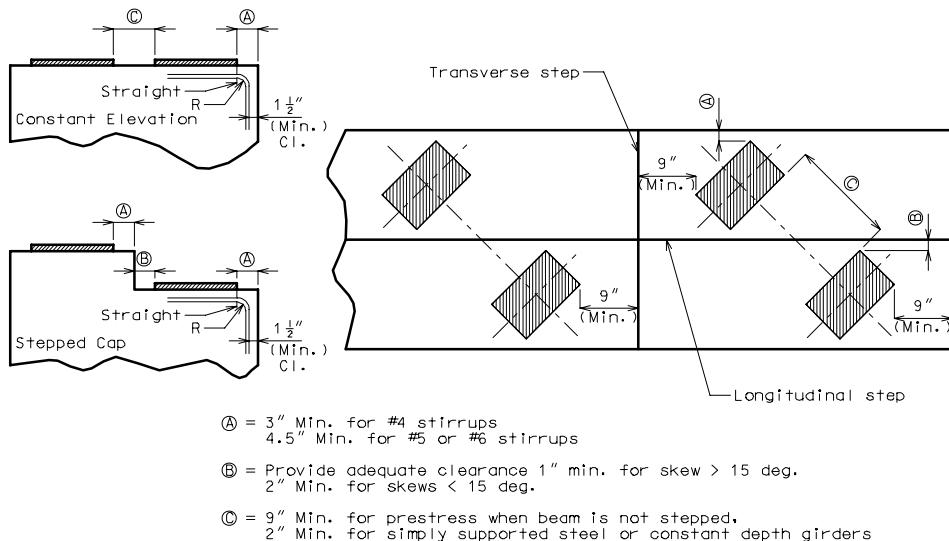
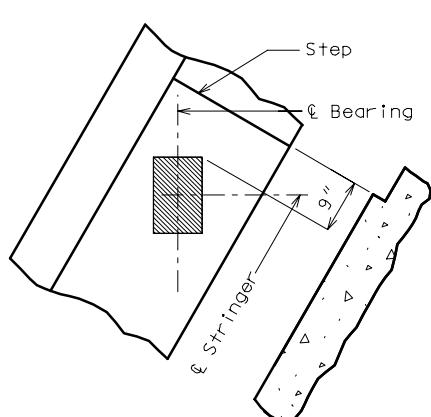


Figure 3.31.4.1-1
Bearing Clearance

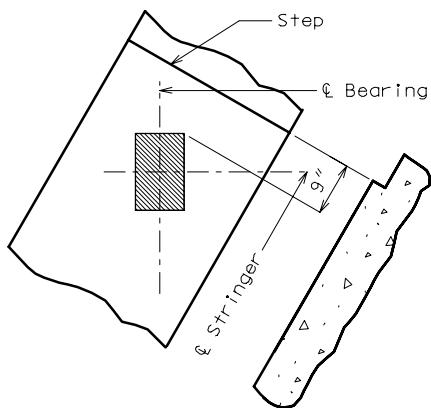
SUBSTRUCTURE BEAM STEPS AND PADS

DEFERENCE IN BEARING ELEV.	METHOD OF OBTAINING ELEVATION
1/8" or less	Retain in vertical dimension but use no fill plates Use the lower 1/8 " for bent height.
1/4" thru 1/2"	Increase thickness of top plate of bearing or haunch.
5/8" thru 1" and up *	Monolithic bearing pad or step beam.

(*) Use same method of obtaining elevation throughout a structure where practical.
Do not mix monolithic bearing pads and steps.

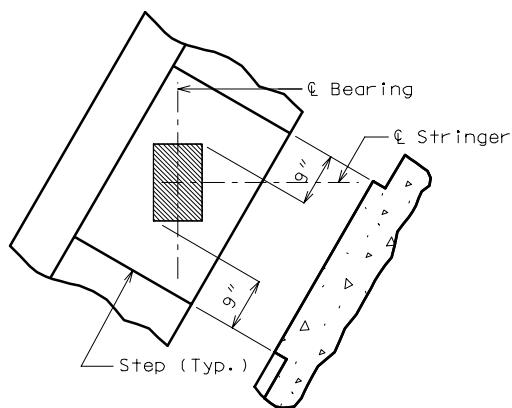


END BENT

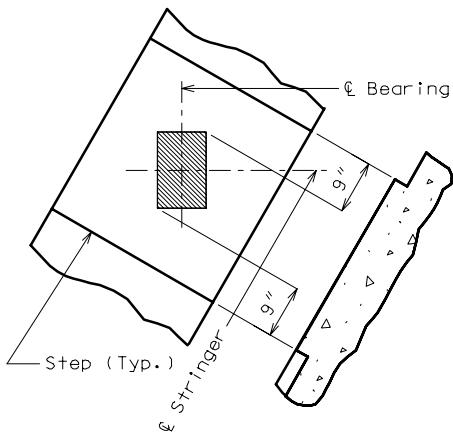


INT. BENT

STEP BEAM



END BENT

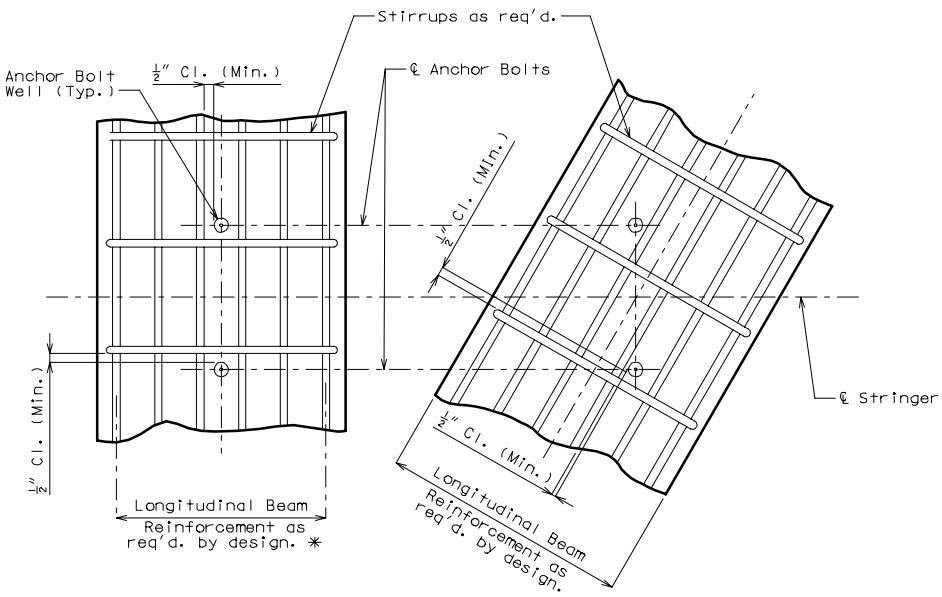


INT. BENT

MONOLITHIC BEARING PADS

ANCHOR BOLTS

Clearance for reinforcement:



SQUARE

SKEWED

PART PLAN OF BEAM TOPS
(INT. BENTS SHOWN)

(*). Use even number of bars in beam tops for square bridges when possible.

Note: Details shown above are for information only. Place the following note on the plans, preferably with "General Notes".

"All reinforcing bars in the tops of substructure beams or caps shall be spaced to clear anchor bolt wells for bearings by at least 1/2".

Note: See sheet no. 4.4-1 this section for size of anchor bolt wells.

ANCHOR BOLT TABLES

ANCHOR BOLT DETAILS:

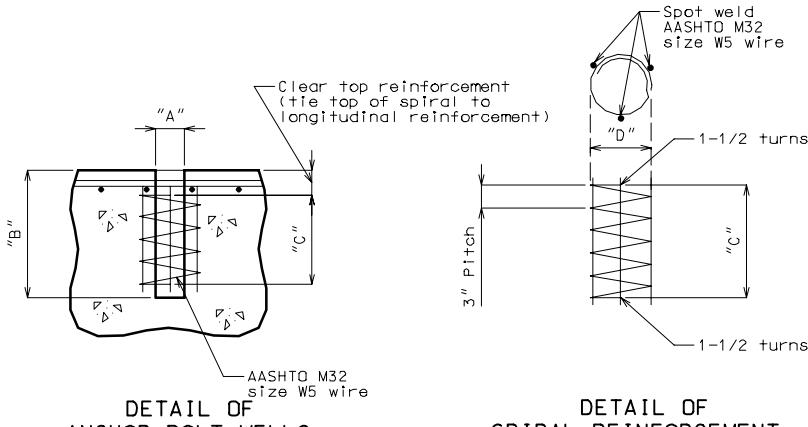
DETAIL OF
ANCHOR BOLT WELLSDETAIL OF
SPIRAL REINFORCEMENT

TABLE OF ANCHOR BOLT WELLS

Anchor Bolt Diameter	"A" Well Diameter	"B" Well Depth	"C" Spiral Depth	"D" Spiral Diameter	Spiral Bar Length	Bolt Extension into Concrete
1"	3"	12"	9"	8-1/8"	15'-1"	9"
1-1/4"	4"	15"	12"	9-1/8"	19'-9"	12"
1-1/2"	4"	18"	15"	9-1/8"	23'-0"	15"
2"	4"	21"	18"	9-1/8"	26'-1"	18"
2-1/2"	4"	28"	25"	9-1/8"	33'-2"	25"

Omit spiral on 21" WF if anchor bolt spacing is less than 6"

TABLE OF BOLT WEIGHTS

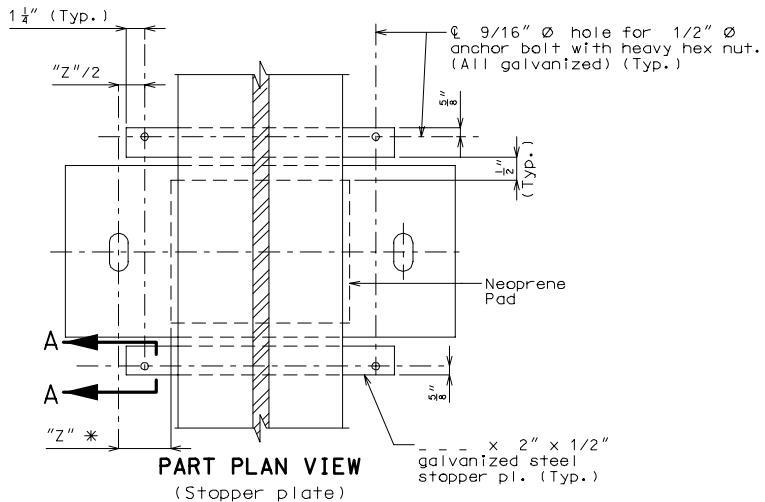
Description	(#/in.)	1"	1-1/4"	1-1/2"	2"	2-1/2"
Unthreaded	(#/in.)	----	----	.5	.89	1.39
Threaded	(#/in.)	----	----	.425	.755	1.20"
Nut	(lbs.)	----	----	1.31	2.99	5.64
Weight used for entire bearing (#/ft.)		2.673	4.175	----	----	----

Anchor bolt sizes were based on 10% dead load reactions as per zone 2 earthquake loads. Check the anchor bolts for any centrifugal forces.

Epoxy coat anchor bolt wells at bents with expansion devices.

Miscellaneous Bearing Details(PTFE) BEARING STOPPER PLATE DETAILS

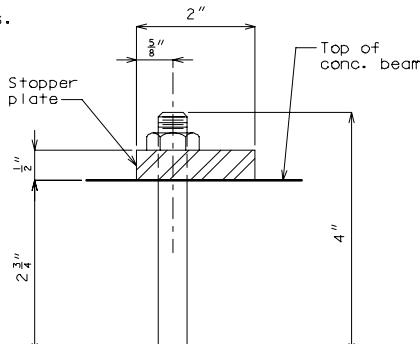
Expansion bearings with two stopper plates
to prevent creep at expansion bearing



* Add strap when dimension "Z" is 3" or greater
see page 4.5-2

Note to Detailer:

Make sure top of
bolt for stopper plates
clears bearing plate
for structures on grades.

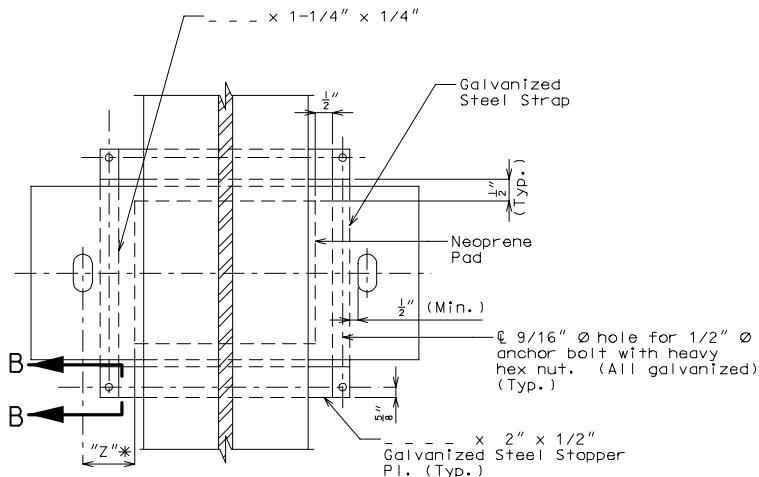


SECTION A-A

See general notes section for notes pertaining to PTFE bearings.

Miscellaneous Bearing Details(PTFE) BEARING STOPPER PLATE DETAILS (CONT.)

Bearings with stopper plates and steel straps
to prevent creep at expansion bearings.

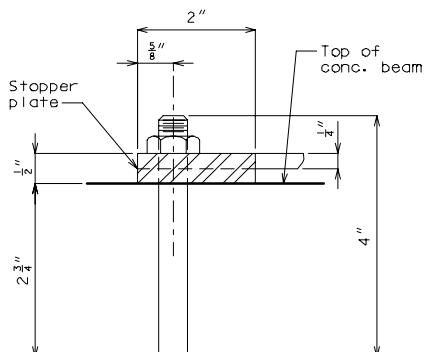


PART PLAN VIEW
(Stopper Plate and Strap)

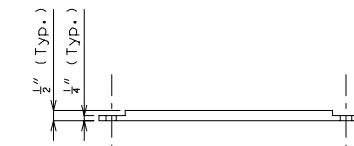
* Add strap when dimension "Z" is 3" or greater.

Note to detailer:

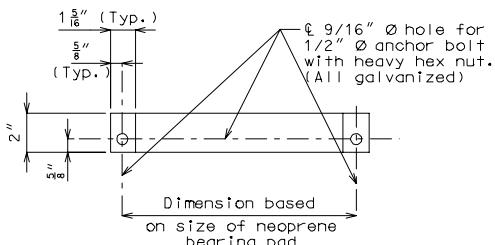
Make sure top of bolt for
stopper plates clears bearing
plate for structures on grades.



SECTION B-B

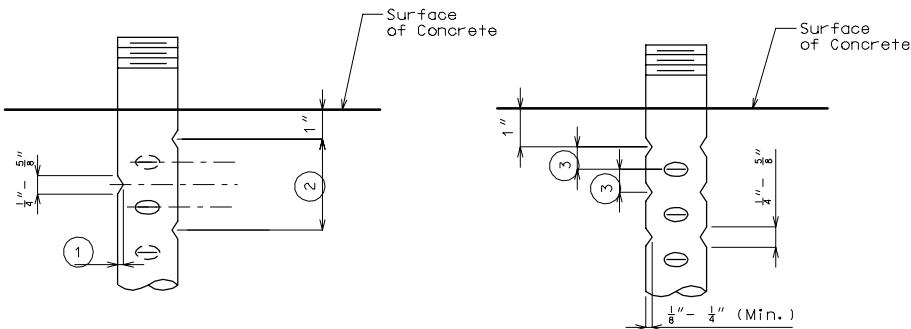


ELEVATION OF GALVANIZED STEEL STOPPER PLATE



PLAN OF GALVANIZED STEEL STOPPER PLATE

See general notes section for notes pertaining to PTFE bearings.

SWEDGE ANCHOR BOLT DETAILSMISCELLANEOUS BEARING DETAILS

DETAIL "A"

DETAIL "B"

(Optional Detail for 1-3/8" \varnothing thru 2-1/2" \varnothing Anchor Bolts)SWEDGE ANCHOR BOLT DETAILS

- (1) 1/8" — 3/4" \varnothing thru 1-1/4" \varnothing Anchor Bolts
1/8" to 1/4" — 1-3/8" \varnothing thru 2-1/2" \varnothing Anchor Bolts
- (2) 2-1/2" to 3-1/2"
- (3) 5/8" to 7/8"

Above detail shall be placed on the bearing sheet of all structures using swedge anchor bolts.